

# COOPERATIVE RESEARCH CENTRE FOR THE ANTARCTIC AND SOUTHERN OCEAN ENVIRONMENT (ANTARCTIC CRC)

Aurora Australis Marine Science Cruises AU9501, AU9604 and AU9601 - Oceanographic Field Measurements and Analysis, Inter-cruise Comparisons and Data Quality Notes

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#### Part 1

# Aurora Australis Marine Science Cruise AU9501 - Oceanographic Field Measurements and Analysis

#### **ABSTRACT**

Oceanographic measurements were conducted along WOCE Southern Ocean meridional section SR3 between Tasmania and Antarctica, and around the boundary of a square-plan test volume south of the Antarctic Divergence, from July to September 1995. A total of 208 CTD vertical profile stations were taken, 64 of those to near bottom, and the remaining 144 to a depth of 500 m. Over 2300 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients, dissolved organic and inorganic carbon, iodate/iodide, primary productivity, and biological parameters, using both a 24 and 12 bottle rosette sampler. Near surface current data were collected using a ship mounted ADCP. Measurement and data processing techniques are summarised, and a summary of the data is presented in graphical and tabular form.

#### 1.1 INTRODUCTION

Marine science cruise AU9501, the fourth oceanographic cruise of the Cooperative Research Centre for the Antarctic and Southern Ocean Environment (Antarctic CRC), was conducted aboard the Australian Antarctic Division vessel RSV Aurora Australis from July to September 1995. The first major constituent of the cruise was the collection of oceanographic data relevant to the Australian Southern Ocean WOCE Hydrographic Program, along WOCE section SR3 (Figure 1.1a). The primary scientific objectives of this program are summarised in Rosenberg et al. (1995a). This was the sixth occupation of section SR3, and the first during a southern winter. Previous occupations of SR3 by the Aurora Australis were in the spring of 1991 (Rintoul and Bullister, submitted), in the autumn of 1993 (Rosenberg et al., 1995a), and in the summers of 1993/94 and 1994/95 (Rosenberg et al., 1995b and 1996). The northern half of the SR3 section was occupied by the SCRIPPS ship R.V. Melville in the autumn of 1995 (principal investigators R.Watts, S. Rintoul, J. Richman, B. Petit, D. Luther, J. Filloux, J. Church, A. Chave).

The second major constituent of the cruise was the dual oceanographic and sea ice experiments FORMEX (Formation Experiment: water mass formation near the Antarctic Continental slope) and HIHO-HIHO (Harmonious Ice and Hydrographic Observations - Halide In, Heat Out: sea ice formation processes; Worby et al., 1996). The primary objectives of FORMEX are:

- 1. to obtain quantitative estimates of the rate of formation of Antarctic surface waters in the ice pack during winter;
- 2. to obtain quantitative estimates of the transfer of heat between the ocean and atmosphere and the role of advection of surface and circumpolar deep water on these transfers;
- 3. to investigate processes and mechanisms involved in the mixing of Polar Zone waters with "Complex Zone" waters near the Antarctic shelf.

FORMEX CTD measurements were collected to a depth of 500 m every 5 nautical miles around the perimeter of a closed 60x60 nautical mile area within the pack ice (Figure 1.1b). The closed volume was sampled clockwise 3 times over a 21 day period, with 48 CTD/ADCP profile stations sampled on each of the 3 completed circuits.

This report describes the collection of oceanographic data from the SR3 transect and FORMEX, and summarises the chemical analysis and data processing methods employed. All information required for use of the data set is presented in tabular and graphical form.

#### 1.2 CRUISE ITINERARY

The cruise commenced with a north to south traverse of section SR3, with a typical station spacing of 30 nautical miles. Station spacing between 49.5°S and 52°S was decreased to less than 20 nautical miles (Table 1.2) to include CTD casts over current meter and inverted echo sounder moorings (Table 1.4), thereby increasing meridional resolution in the vicinity of the Subantarctic Front. The mooring array had been deployed in the autumn of 1995 by the R.V. Melville (principal investigators R.Watts, S. Rintoul, J. Richman, B. Petit, D. Luther, J. Filloux, J. Church, A. Chave). South of ~55°S, periods of very calm conditions were encountered, with winds close to zero and the ocean surface glassy. ADCP measurements from this period will be useful for an examination of ADCP data in the absence of noise created by rolling and pitching of the ship. CTD data from this period will allow closer examination of CTD data quality in the absence of pressure reversals caused by a heaving vessel. The section was interrupted at ~65.1°S, due to thick sea ice and rising northerly winds.

The first lap around the FORMEX area was commenced 3 days after the interruption of the SR3 transect, and took 4 days to complete. The ship then travelled south as far as ~65.5°S, with further progress prevented by sea ice conditions. The SR3 section was recommenced at the southernmost latitude, and 3 stations were completed from south to north (Table 1.2). Note that the southermost station was over the continental slope, in a water depth of 1761 m.

Back at the FORMEX site, 2 test casts were taken inside the FORMEX area, both to trial a protective cover against cold air for the CTD sensors, and to investigate sensor performance on CTD serial 1193. FORMEX lap 2 then commenced, 6 days after the completion of lap 1, and taking 4.5 days to complete. Lap 3 commenced 1.5 days after the completion of lap 2, and took 3.5 days to complete. The time before and after each FORMEX lap was dedicated to sea ice experiments.

The ship then returned to the SR3 section, and CTD measurements at stations 44, 43 and 42 were repeated, owing to conductivity sensor malfunction during the earlier occupation. Before returning to Hobart, a further 4 stations were completed over inverted echo sounder moorings along the SR3 transect in the vicinity of the Subantarctic Front (Table 1.4). No measurements could be taken at the remaining 3 inverted echo sounder locations (mooring numbers I3, I5 and I7) due to rough weather conditions encountered on the northward leg.

#### **Table 1.1:** Summary of cruise itinerary.

Expedition Designation
Cruise AU9501 (cruise acronym ABSTAIN), encompassing WOCE section SR3, and FORMEX

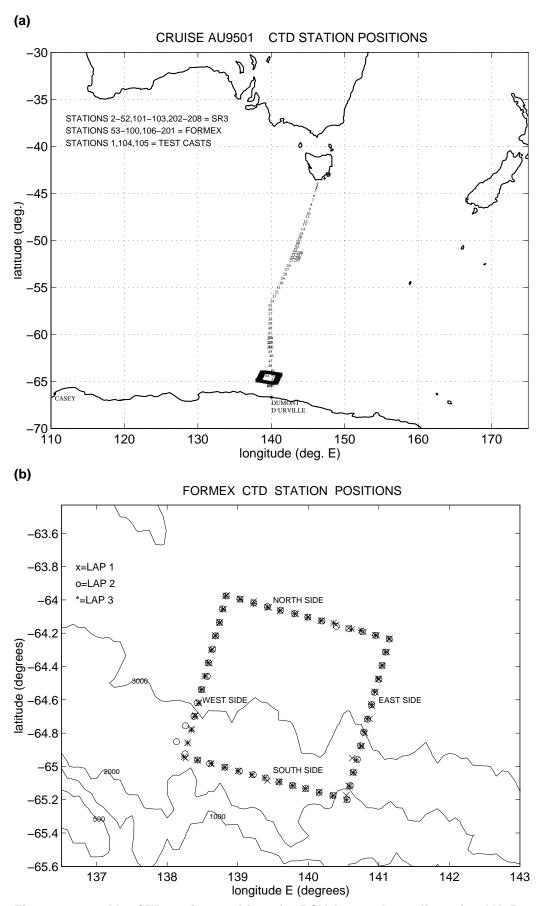
Chief Scientists
Nathan Bindoff, Antarctic CRC
Ian Allison, Antarctic Division

Ship RSV Aurora Australis

Ports of Call

-

Cruise Dates
July 17 to September 2 1995



<u>Figure 1.1a and b:</u> CTD station positions for RSV Aurora Australis cruise AU9501 along WOCE transect SR3, and around FORMEX area.

#### 1.3 CRUISE SUMMARY

#### 1.3.1 CTD casts and water samples

In the course of the cruise, 61 CTD casts were completed along the SR3 section (Figure 1.1a), with most casts reaching to within 17 m of the sea floor (Table 1.2); 144 CTD casts to a depth of 500 m were completed on the 3 FORMEX laps; and 3 additional full depth test casts were completed at various locations. Over 2300 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients (orthophosphate, nitrate plus nitrite, and reactive silicate), dissolved organic and inorganic carbon, iodate/iodide, primary productivity, and biological parameters, using a 24 bottle rosette sampler for the SR3 section, and a 12 bottle system (with 6 bottles mounted) for FORMEX. Table 1.3 provides a summary of samples drawn at each station. Principal investigators for the various water sampling programmes are listed in Table 1.5a. For all stations, the different samples were drawn in a fixed sequence (see Rosenberg et al., 1996, for more details, including descriptions of methods for drawing samples).

#### 1.3.2 Principal investigators

The principal investigators for the CTD and water sample measurements are listed in Table 1.5a. Cruise participants are listed in Table 1.5b.

Table 1.2 (following 6 pages): Summary of station information for RSV Aurora Australis cruise AU9501. The information shown includes time, date, position and ocean depth for the start of the cast, at the bottom of the cast, and for the end of the cast. The maximum pressure reached for each cast, and the altimeter reading at the bottom of each SR3 cast (i.e. elevation above the sea bed) are also included. Missing ocean depth values are due to noise from the ship's bow thrusters interfering with the echo sounder. For casts which do not reach to within 100 m of the bed (i.e. the altimeter range), or for which the altimeter was not functioning, there is no altimeter value. For station names, TEST is a test cast, and Fx.y is cast number y on FORMEX lap x (Figure 1.1b). Note that all times are UTC (i.e. GMT). CTD unit 7 (serial no. 1103) was used for stations 30 to 44, and 104 to 105.

station			STAF	RT	maxP		BO1	TOM				EN	ID .	
number	time	date	latitude	longitude depth(m)	(dbar)	time	latitude	longitude	depth(m	n) altimeter	time	latitude	longitude	depth(m)
				- J	()			<u> </u>		,				
1 TEST	2227 1	7-JUL-95	44:22.85S	146:10.75E 2387	2306	2345	44:22.665	146:11.34E	2392	58.4	0046	44:22.50S	146:11.50E	2393
2 SR3	0315 1	8-JUL-95	43:59.86S	146:19.20E 240	174	0330	43:59.885	146:19.62E	-	14.0	0358	43:59.978	146:20.32E	210
3 SR3	0538 1	8-JUL-95	44:07.38S	146:13.72E 1076	1106	0612	44:07.598	146:14.85E	-	16.0	0658	44:07.598	146:15.67E	-
4 SR3	1000 1	8-JUL-95	44:22.72S	146:10.59E 2407	2348	1103	44:22.658	146:10.77E	-	15.6	1224	44:22.628	146:10.90E	-
5 SR3	1610 1	8-JUL-95	44:43.18S	146:02.80E 3225	3230	1736	44:43.248	146:03.31E	3225	17.6	1916	44:43.30S	146:03.67E	3123
6 SR3				145:51.22E 2866	2890	0155	45:12.728	3 145:51.11E	-	18.0	0317	45:12.66S	145:52.36E	2764
7 SR3	1729 1	9-JUL-95	45:41.88S	145:39.45E 2017	2056	1838	45:41.888	145:38.57E	2068	17.6	2005	45:41.66S	145:37.75E	2068
8 SR3	0027 2	0-JUL-95	46:10.36S	145:27.57E 2744	2748	0148	46:10.188	145:27.58E	2740	18.1	0311	46:09.89S	145:27.63E	2764
9 SR3	0710 2	0-JUL-95	46:39.14S	145:15.03E 3348	3392	0835	46:38.938	145:14.68E	-	16.8	1019	46:38.40S	145:14.63E	3368
10 SR3	1413 2	0-JUL-95	47:08.72S	145:03.10E 3593	3910	1545	47:08.288	145:04.02E	-	15.1	1721	47:07.67S	145:04.28E	-
11 SR3				144:54.33E 4300	4344			144:55.48E		17.9	2336	47:26.85S	144:56.04E	4068
12 SR3	0318 2	1-JUL-95	47:59.90S	144:40.57E 4064	4144	0458	47:59.088	144:40.79E	-	5.0	0633	47:58.53S	144:40.99E	-
13 SR3	0852 2	1-JUL-95	48:19.03S	144:31.56E 4003	4170	1040	48:18.358	144:31.13E	-	15.0	1242	48:18.12S	144:31.58E	3936
14 SR3				144:18.95E 4177	4134			3 144:19.15E		16.5	1850	48:44.91S	144:19.14E	4045
15 SR3				144:05.63E 4218	4254	2341	49:15.288	144:05.86E	4350	11.1	0133	49:14.49S	144:06.13E	-
16 SR3				143:56.13E 3686	3836			3 143:57.07E		-			143:57.97E	-
17 SR3				143:48.21E 3788	3864			143:49.92E		16.0			143:50.73E	-
18 SR3				143:40.72E 3711	3818			3 143:41.91E		17.3			143:42.88E	
19 SR3				143:33.66E 3583	3656			143:35.08E		16.7			143:36.13E	3573
20 SR3				143:26.96E 3655	3556			3 143:27.26E		19.9			143:27.22E	-
21 SR3				143:17.77E 3808	3880			3 143:17.62E		19.8			143:17.39E	-
22 SR3				143:07.69E 3706	3876			3 143:08.06E		15.0			143:08.68E	-
23 SR3				142:59.21E 3778	3788	-		3 143:00.10E		17.0			143:00.77E	
24 SR3				142:50.80E 3757	3674			142:52.80E		17.4			142:53.60E	3722
25 SR3				142:42.01E 3512	3514			142:44.15E		19.5			142:45.42E	-
26 SR3				142:22.85E 3348	3470			142:23.97E		12.0			142:24.57E	-
27 SR3				142:08.25E 3133	3134			142:08.16E		15.0			142:07.92E	
28 SR3				141:51.81E 2508	2508			141:52.23E		13.0			141:52.65E	2661
29 SR3				141:35.63E 2662	2656			141:35.57E		15.6			141:35.70E	-
30 SR3				141:19.42E 2815	2844			141:19.86E		12.0			141:19.75E	-
31 SR3				141:00.79E 3348	3300			141:00.34E		15.2			141:00.74E	3328
32 SR3				140:43.48E 3993	4140			140:43.15E		15.0			140:43.08E	-
33 SR3				140:23.88E 3583	3638			140:24.37E		15.5			140:25.04E	-
34 SR3				140:06.09E 3890	4162			140:06.07E		15.0			140:05.98E	-
35 SR3				139:50.88E 4075	4180			139:51.85E		14.3			139:52.18E	415/
36 SR3	0024 2	7-JUL-95	57:22.25S	139:51.04E 4075	4058	0212	57:22.17S	3 139:49.72E	-	11.4	0404	57:22.58S	139:48.79E	-

station			STAF	PΤ	maxP		BC	OTTC	)M				F	ND	
Number	time	date	latitude	longitude depth(m)	(dbar)	time	latitude		ongitude d	denth(m	) altimeter	time	latitude		depth(m)
- ramoon		dato	idilidae	rongitudo dopun(m)	(dbdi)		latitado	<u> </u>	origitado c	aoptii(iii	, ammotor	timo	latitudo	iongitado	aopti (iii)
37 SR3	0650.2	7-JUI -95	57:51 42S	139:51.42E 4095	4182	0831	57:51 31	1S 13	39:51.89E	_	15.0	1000	57:51 39	S 139:52.72E	= _
38 SR3				139:51.08E 3993	4044			-	39:51.57E	_	12.8			S 139:51.62E	
39 SR3	_			139:50.49E 3942	4046				39:50.71E	-	15.9	0215	58:51.72	S 139:50.53E	-
40 SR3				139:50.89E 4218	4220				39:51.23E	-	15.8			S 139:51.76E	
41 SR3				139:50.94E 4587	4540	1632	59:50.24	4S 13	39:51.31E	-	13.8	1829	59:49.57	S 139:52.13E	E 4587
42 SR3	2320 2	28-JUL-95	60:21.27S	139:50.24E 4443	4506	0128	60:21.54	4S 13	39:49.95E	4443	9.9	0328	60:21.87	S 139:49.61E	<u>-</u>
43 SR3	0611 2	9-JUL-95	60:51.27S	139:50.17E 4402	4466	0747	60:51.80	OS 13	39:49.52E	-	11.3	0928	60:52.30	S 139:49.72E	<u>-</u>
44 SR3	1431 2	29-JUL-95	61:21.06S	139:51.01E 4351	4410	1649	61:22.09	9 <mark>S</mark> 13	39:50.41E	4351	13.6	1847	61:22.39	S 139:50.64E	4351
45 SR3	2326 2	29-JUL-95	61:50.05S	139:51.60E 4300	3348	0125	61:49.87	7S 13	39:54.95E	4300	-	0255	61:50.58	S 139:57.90E	<b>∃</b> -
46 SR3	0622 3	80-JUL-95	62:15.68S	140:00.46E 4054	4082	0758	62:15.84	4S 14	40:01.21E	4054	16.4	0936	62:16.32	S 140:02.14E	<b>∃</b> -
47 SR3				139:53.68E 3235	3262	1601	62:50.56	6S 13	39:54.91E	3275	13.5	1728	62:51.63	S 139:55.29E	3255
48 SR3				139:50.37E 3819	3830				39:49.53E		25.5			S 139:47.19E	
49 SR3				140:07.79E 3716	3746				40:11.10E		16.0			S 140:14.37E	
50 SR3				140:20.49E 3481	3476				40:20.04E	3471	13.7			S 140:19.64E	
51 SR3				140:20.35E 3327	3274	-			40:18.40E	-	16.2			S 140:16.84E	
52 SR3				140:19.45E 2583	2582				40:18.91E	-	14.9			S 140:18.24E	
53 F1.1				140:37.39E 2701	496	_			40:36.97E	_	-			S 140:36.63E	_
54 F1.2				140:37.98E 2598	496				40:37.62E		-	_		S 140:37.09E	
55 F1.3				140:34.41E 2471	500				40:34.00E		-			S 140:33.66E	
56 F1.4				140:32.34E 2217	496				40:31.93E	2232	-			S 140:31.67E	
57 F1.5				140:21.43E 2383	496				40:21.26E	-	-			S 140:20.98E	
58 F1.6				140:09.12E 2569	496				40:08.93E	-	-			S 140:08.75E	
59 F1.7				139:57.79E 2746	498				39:57.66E	-	-			S 139:57.50E	
60 F1.8				139:47.20E 2538	496				39:47.10E	2544	-			S 139:46.83E	
61 F1.9				139:34.91E 2537	496				39:34.86E	-	-			S 139:34.83E	
62 F1.10				139:25.27E 2688	498				39:25.16E		-			S 139:25.13E	
63 F1.11				139:12.11E 2911	496				39:12.06E		-			S 139:12.03E	
64 F1.12				139:00.64E 2595	496	_			39:00.56E		-			S 139:00.52E	
65 F1.13				138:48.70E 2314	498				38:48.65E	2314	-			S 138:48.67E	
66 F1.14				138:37.25E 2524	496	_			38:37.16E	-	-			S 138:37.09E	-
67 F1.15				138:26.05E 2205	498				38:25.99E	_	-			S 138:25.92E	-
68 F1.16				138:15.69E 2498	498				38:15.69E		-			S 138:15.60E	
69 F1.17				138:17.32E 2630	498	_		-	38:17.57E		-			S 138:17.68E	
70 F1.18				138:20.80E 2858	498				38:21.00E		-			S 138:21.08E	
71 F1.19				138:23.81E 2858	496	1651	64:41.52	2S 13	38:23.88E	2867	-	1708	64:41.41	S 138:24.18E	2867
72 F1.20	1805	6-AUG-95	64:37.03S	138:26.85E 2853	496	1820	64:36.98	3S 13	38:26.97E	2843	-	1838	64:36.89	S 138:27.03E	2843

station			STAF	RT	maxP		BO	ттом					EN	ID	
number	time	date	latitude	longitude depth(m)	(dbar)	time	latitude		itude	depth(n	n) altimeter	time	latitude	longitude	depth(m)
		5.5.1.5		Total Samuel and and and	(5)						.,	-			
73 F1.21	1925	6-AUG-95	64:32.33S	138:30.00E 3086	498	1940	64:32.25	S 138:3	0.00E	3096	_	1959	64:32.22S	138:30.05E	3096
74 F1.22	2107	6-AUG-95	64:27.42S	138:33.24E 3188	498	2123	64:27.42	S 138:3	3.27E	3183	-	2139	64:27.35S	138:33.25E	3183
75 F1.23	2235	6-AUG-95	64:22.86S	138:36.08E 3287	496	2252	64:22.85	S 138:3	6.13E	3287	-	2306	64:22.83S	138:36.24E	3287
76 F1.24				138:38.57E 3392	496	0015	64:17.82	S 138:3	8.79E	3402	-			138:38.98E	
77 F1.25				138:40.75E 3480	500	0132	64:12.83	S 138:4	0.83E	3480	-			138:41.23E	
78 F1.26	0322	7-AUG-95	64:08.17S	138:44.91E 3564	498	0337	64:08.13	S 138:4	5.25E	3564	-	0358	64:08.04S	138:45.64E	3571
79 F1.27	0446	7-AUG-95	64:03.24S	138:48.02E 3677	498	0458	64:03.20	S 138:4	8.31E	-	-	0516	64:03.21S	138:48.61E	-
80 F1.28	0553	7-AUG-95	63:58.39S	138:50.63E 3706	500	0610	63:58.50	S 138:5	1.34E	-	-	0627	63:58.34S	138:52.12E	3737
81 F1.29	0715	7-AUG-95	63:59.61S	139:02.32E 3699	498	0727	63:59.59	S 139:0	2.66E	3700	-	0746	63:59.52S	139:03.19E	3700
82 F1.30	0847	7-AUG-95	64:00.56S	139:13.69E 3618	496	0900	64:00.48	S 139:1	3.91E	3620	-	0915	64:00.54S	139:14.46E	3621
83 F1.31	1027	7-AUG-95	64:02.70S	139:26.35E 3629	498	1038	64:02.67	S 139:2	6.59E	3629	-	1057	64:02.74S	139:26.97E	-
84 F1.32	1147	7-AUG-95	64:03.85S	139:36.33E 3614	498	1158	64:03.76	S 139:3	6.71E	-	-	1209	64:03.67S	139:37.09E	3604
85 F1.33	1306	7-AUG-95	64:05.16S	139:49.29E 3631	498	1319	64:05.06	S 139:4	19.57E	-	-	1335	64:04.90S	139:49.94E	3635
86 F1.34	1431	7-AUG-95	64:06.24S	139:59.92E 3655	498	1445	64:06.07	S 140:0	0.27E	-	-	1503	64:05.97S	140:00.56E	-
87 F1.35				140:11.71E 3610	500	1552	64:07.24	S 140:1	2.03E	-	-	1611	64:07.13S	140:12.49E	-
88 F1.36				140:23.59E 3612	496	1659	64:08.89	S 140:2	23.77E	-	-			140:24.00E	
89 F1.37	_			140:34.32E 3610	496		64:10.21				-			140:34.20E	
90 F1.38				140:46.92E 3594	496		64:11.59	_			-			140:46.75E	
91 F1.39				140:58.08E 3597	498		64:12.82				-			140:58.41E	
92 F1.40				141:09.21E 3623	498		64:13.87				-			141:09.47E	
93 F1.41				141:06.73E 3550	498		64:18.78				-			141:06.75E	
94 F1.42				141:03.08E 3467	498		64:23.74				-			141:03.51E	
95 F1.43				141:00.15E 3365	496		64:28.43	-	-		-			141:00.56E	
96 F1.44				140:57.15E 3264	508		64:33.28		_		-			140:57.55E	
97 F1.45				140:54.08E 3100	498		64:38.20				-			140:54.19E	
98 F1.46				140:52.30E 2881	496		64:42.83				-	_		140:52.17E	
99 F1.47				140:48.28E 2699	498		64:48.00				-			140:47.96E	
100 F1.48				140:45.46E 2602	498	_	64:52.59	-		_	-			140:45.07E	
101 SR3				139:44.93E 1761	1736		65:30.63				10.7			139:45.07E	
102 SR3				139:47.82E 2074	2072		65:27.66		-		11.6	_		139:47.62E	
103 SR3				139:56.58E 2551	2538		65:21.80		-		12.8			139:56.31E	
104 TEST				3 139:16.75E 3583	3582		64:21.39				16.7			139:13.36E	
105 TEST				3 138:31.57E 2701	2706		64:40.68				11.1			138:29.10E	
106 F2.19				3 138:22.80E 2767	500		64:41.91			2780	-			138:22.18E	
107 F2.20				138:25.50E 2865	496		64:37.08			-	-			138:25.01E	
108 F2.21	2217	14-AUG-95	64:32.288	138:29.28E 3043	498	2230	64:32.23	S 138:2	9.10E	3037	-	2244	64:32.20S	138:28.95E	: 3036

station			STAR		maxP		BO	TTO	M				EN	ID	
number	time	date	latitude	longitude depth(m)	(dbar)	time	latitude			depth(m	) altimeter	time	latitude	longitude	depth(m)
					(55)					P (	,				
109 F2.22	2346 1	4-AUG-95	64:27.59S	138:34.14E 3225	498	2357	64:27.60	S 138	3:34.00E	3225	_	0019	64:27.59S	138:33.54E	3225
110 F2.23				138:35.08E 3276	498		64:22.67				_			138:34.21E	
111 F2.24				138:38.63E 3419	498		64:17.62				-			138:37.54E	
112 F2.25				138:41.11E 3471	498		64:12.91			-	-			138:40.31E	
113 F2.26	0830 1	5-AUG-95	64:08.07S	138:44.31E 3583	498	0843	64:08.04	S 138	3:44.04E	-	-	0903	64:07.96S	138:43.53E	3573
114 F2.27				138:47.02E 3686	498		64:03.22			-	-			138:46.49E	
115 F2.28	1			138:50.14E 3716	498		63:58.54			-	-			138:49.50E	
116 F2.29	1328 1	5-AUG-95	63:59.70S	139:01.86E 3706	498	1338	63:59.70	S 139	9:01.62E	3696	-			139:01.36E	
117 F2.30	1458 1	5-AUG-95	64:01.04S	139:13.75E 3634	498	1510	64:01.07	S 139	9:13.54E	3634	-	1528	64:01.04S	139:13.17E	3634
118 F2.31	1626 1	5-AUG-95	64:02.41S	139:25.20E 3604	498	1638	64:02.43	S 139	9:24.99E	3604	-	1652	64:02.44S	139:24.70E	3604
119 F2.32	1739 1	5-AUG-95	64:03.69S	139:36.59E 3609	498	1754	64:03.60	S 139	9:36.21E	3635	-	1809	64:03.57S	139:35.86E	3635
120 F2.33	1924 1	5-AUG-95	64:04.91S	139:48.41E 3634	498	1939	64:04.86	S 139	9:48.09E	3639	-	2002	64:04.77S	139:47.47E	3634
121 F2.34	2106 1	5-AUG-95	64:06.19S	139:59.58E 3634	498	2122	64:06.10	S 139	9:59.20E	3654	-	2136	64:06.01S	139:58.77E	3654
122 F2.35	2236 1	5-AUG-95	64:07.57S	140:11.61E 3645	498	2249	64:07.50	S 140	):11.22E	3634	-	2303	64:07.47S	140:10.84E	3634
123 F2.36	0006 1	6-AUG-95	64:09.56S	140:23.98E 3614	498	0020	64:09.49	S 140	):23.39E	3614	-	0033	64:09.42S	140:23.01E	3634
124 F2.37	0127 1	6-AUG-95	64:10.30S	140:34.55E 3593	504	0140	64:10.26	S 140	0:34.16E	3634	-	0156	64:10.29S	140:33.84E	3634
125 F2.38	0257 1	6-AUG-95	64:11.44S	140:46.03E 3645	500	0310	64:11.47	S 140	):45.61E	-	-	0328	64:11.52S	140:45.10E	3604
126 F2.39				140:57.40E 3604	498		64:12.73		-		-			140:56.59E	
127 F2.40	1			141:08.89E 3604	498		64:14.13			3604	-			141:08.18E	
128 F2.41	1			141:05.85E 3553	498		64:18.85			-	-			141:05.50E	
129 F2.42				141:02.69E 3450	498		64:23.64				-			141:02.33E	
130 F2.43	1			141:00.02E 3389	498		64:28.58			3368	-			140:59.83E	
131 F2.44	1			140:56.42E 3276	498		64:33.27			-	-			140:56.08E	
132 F2.45				140:53.68E 3092	498	_	64:37.70				-			140:53.06E	
133 F2.46				140:50.58E 2856	498		64:42.99				-			140:49.86E	
134 F2.47	1			140:47.04E 2725	498		64:47.69			-	-			140:46.58E	-
135 F2.48	1			140:44.37E 2600	498		64:52.47				-			140:43.98E	
136 F2.1	1			140:41.82E 2518	498		64:57.28		-		-	_		140:40.50E	
137 F2.2				140:38.31E 2559	500		65:02.08				-			140:38.18E	
138 F2.3				140:35.71E 2406	498	-	65:06.94	-			-			140:35.56E	
139 F2.4				140:33.18E 2252	500	_	65:11.94				-	_		140:33.15E	-
140 F2.5				140:20.97E 2395	498		65:10.41				-			140:20.92E	
141 F2.6	1			140:09.27E 2559	498		65:09.34				-			140:09.32E	
142 F2.7				139:57.91E 2744	498		65:07.98				-			139:58.02E	
143 F2.8				139:46.59E 2514	498		65:06.88				-			139:46.81E	
144 F2.9	2220 1	7-AUG-95	65:05.61S	139:34.99E 2511	498	2234	65:05.61	S 139	9:35.08E	2526	-	2249	65:05.56S	139:35.34E	2531

station			STAR		maxP		BC	OTTO	OM				EN	ID	
number	time	date	latitude	longitude depth(m)	(dbar)	time	latitude			depth(m	n) altimeter	time	latitude	longitude	depth(m)
				<u> </u>	()				3	1 - \	,				
145 F2.10	0505 1	8-AUG-95	65:04.17S	139:24.01E 3010	498	0517	65:04.14	IS 13	39:24.13E	-	_	0538	65:04.10S	139:24.33E	3030
146 F2.11	0802 1	8-AUG-95	65:03.01S	139:13.23E 2907	498	0814	65:02.98	3S 13	39:13.32E	2917	-	0832	65:02.95S	139:13.38E	2917
147 F2.12	1033 1	8-AUG-95	65:01.70S	139:01.50E 2617	498	1045	65:01.69	S 13	39:01.57E	2627	-	1058	65:01.65S	139:01.64E	2627
148 F2.13	1432 1	8-AUG-95	65:00.33S	138:49.09E 2319	500	1446	65:00.31	IS 13	38:49.12E	2315	-	1508	65:00.27S	138:49.23E	2313
149 F2.14	1959 1	8-AUG-95	64:58.96S	138:36.09E 2445	498	2012	64:58.94	IS 13	38:36.14E	2440	-			138:36.12E	
150 F2.15	2127 1	8-AUG-95	64:57.67S	138:25.90E 2215	496	2141	64:57.63	3S 13	38:25.88E	2230	-	2154	64:57.63S	138:25.91E	2230
151 F2.16	2254 1	8-AUG-95	64:55.47S	138:15.13E 2588	498	2307	64:55.52	2S 13	38:15.13E	2593	-	2318	64:55.40S	138:15.18E	2598
152 F2.17	0054 1	9-AUG-95	64:51.06S	138:07.90E 3034	498	0106	64:51.03	3S 13	38:07.93E	3034	-	0124	64:50.99S	138:07.99E	3028
153 F2.18	0429 1	9-AUG-95	64:45.37S	138:15.57E 3163	498	0439	64:45.37	'S 13	38:15.67E	-	-	0453	64:45.33S	138:15.70E	3173
154 F3.18	1501 2	0-AUG-95	64:46.93S	138:20.56E 2877	500	1512	64:46.96	SS 13	38:20.45E	2908	-	1526	64:46.99S	138:20.19E	2918
155 F3.19	1652 2	0-AUG-95	64:41.94S	138:23.50E 2810	498	1705	64:41.98	3S 13	38:23.25E	2805	-	1723	64:42.02S	138:22.93E	2805
156 F3.20	1850 2	0-AUG-95	64:37.18S	138:26.85E 2851	498	1907	64:37.21	IS 13	38:26.52E	2856	-	1923	64:37.24S	138:26.20E	2851
157 F3.21	2024 2	0-AUG-95	64:32.38S	138:28.80E 3023	498	2039	64:32.41	IS 13	38:28.43E	3028	-	2055	64:32.50S	138:28.00E	3033
158 F3.22	2201 2	0-AUG-95	64:27.46S	138:31.82E 3174	498	2215	64:27.48	3S 13	38:31.52E	3174	-	2229	64:27.52S	138:31.06E	3174
159 F3.23	2352 2	0-AUG-95	64:22.65S	138:34.54E 3297	498	0006	64:22.69	9S 13	38:34.00E	3317	-	0025	64:22.74S	138:33.16E	3327
160 F3.24				138:37.29E 3389	498				38:36.75E		-			138:36.14E	
161 F3.25				138:41.14E 3460	498			_	38:40.58E		-			138:39.84E	
162 F3.26	-			138:44.28E 3573	498				38:43.86E		-			138:42.99E	
163 F3.27				138:47.13E 3686	498				38:46.71E		-			138:46.03E	
164 F3.28				138:49.66E 3696	498				38:49.24E	3696	-			138:48.69E	
165 F3.29				139:01.84E 3696	498				39:01.39E	-	-			139:00.64E	
166 F3.30				139:13.29E 3604	498				39:12.67E		-			139:12.21E	
167 F3.31				139:25.30E 3614	498			_	39:24.56E		-			139:24.17E	
168 F3.32				139:35.83E 3634	502	_		_	39:35.43E		-			139:35.27E	
169 F3.33				139:48.28E 3634	498			_	39:47.80E		-			139:47.16E	
170 F3.34				139:59.51E 3645	498				39:59.04E		-			139:58.43E	
171 F3.35				140:10.68E 3604	498				40:09.96E		-			140:09.20E	
172 F3.36				140:21.48E 3634	500			_	40:21.21E		-			140:20.45E	
173 F3.37				140:36.97E 3634	498				40:36.00E		-			140:34.58E	
174 F3.38				140:44.86E 3604	498			_	40:44.11E		-	-		140:42.87E	
175 F3.39				140:56.98E 3604	498		-	_	40:56.53E		-			140:55.72E	
176 F3.40				141:08.70E 3604	498				41:08.26E		-			141:07.60E	
177 F3.41				141:05.60E 3563	504			_	41:05.35E		-			141:04.87E	
178 F3.42				141:02.71E 3471	496				41:02.50E		-			141:02.27E	
179 F3.43				140:59.28E 3348	498				40:59.02E		-			140:58.74E	
180 F3.44	1030 2	2-AUG-95	64:33.06S	140:56.27E 3286	498	1044	64:32.98	3S 14	40:55.99E	3276	-	1057	64:32.84S	140:55.83E	3276

station			STAR	T	maxP		BO.	TTOM				EN	ID	
number	time	date	latitude	longitude depth(m)	(dbar)	time	latitude	longitude	depth(m	) altimeter	time	latitude	longitude	depth(m)
181 F3.45	1210 2	2-AUG-95	64:37.66S	140:53.70E 3102	498	1222	64:37.618	3 140:53.56E	3102	-	1237	64:37.53S	140:53.31E	3092
182 F3.46	1348 2	2-AUG-95	64:42.79S	140:50.07E 2860	498	1359	64:42.758	3 140:49.98E	2860	-	1416	64:42.66S	140:49.72E	2860
183 F3.47	1555 2	2-AUG-95	64:47.51S	140:47.36E 2741	498	1608	64:47.478	S 140:47.24E	2741	-	1621	64:47.43S	140:47.11E	2741
184 F3.48	1728 2	2-AUG-95	64:52.67S	140:44.57E 2613	498	1740	64:52.629	S 140:44.44E	2593	-	1753	64:52.58S	140:44.32E	2603
185 F3.1	1905 2	2-AUG-95	64:57.69S	140:40.87E 2540	498	1917	64:57.648	S 140:40.77E	2545	-	1931	64:57.62S	140:40.68E	2545
186 F3.2	2053 2	2-AUG-95	65:02.19S	140:38.50E 2581	500	2106	65:02.188	S 140:38.36E	2581	-	2122	65:02.14S	140:38.31E	2581
187 F3.3	2244 2	2-AUG-95	65:07.15S	140:35.33E 2448	498	2257	65:07.128	S 140:35.29E	2453	-	2312	65:07.08S	140:35.24E	2458
188 F3.4	0050 2	3-AUG-95	65:12.06S	140:32.47E 2227	498	0104	65:12.03	S 140:32.37E	2227	-	0118	65:11.98S	140:32.27E	2227
189 F3.5	0258 2	3-AUG-95	65:10.69S	140:20.81E 2387	500	0309	65:10.678	S 140:20.67E	2387	-	0327	65:10.61S	140:20.58E	2387
190 F3.6	0434 2	3-AUG-95	65:09.34S	140:09.38E 2566	498	0444	65:09.328	S 140:09.29E	2566	-	0457	65:09.30S	140:09.22E	2564
191 F3.7	0652 2	3-AUG-95	65:08.00S	139:57.58E 2764	498	0702	65:07.998	S 139:57.57E	2764	-	0714	65:07.98S	139:57.51E	2764
192 F3.8	0825 2	3-AUG-95	65:06.84S	139:46.30E 2493	498	0837	65:06.818	S 139:46.23E	2473	-	0855	65:06.81S	139:46.20E	2473
193 F3.9	1003 2	3-AUG-95	65:05.61S	139:35.49E 2520	532	1017	65:05.603	S 139:35.47E	2510	-	1032	65:05.56S	139:35.41E	2510
194 F3.10	1155 2	3-AUG-95	65:04.12S	139:23.08E 3000	498	1212	65:04.098	3 139:23.07E	3009	-	1226	65:04.07S	139:23.03E	3010
195 F3.11	1331 2	3-AUG-95	65:03.00S	139:12.16E 2915	498	1346	65:02.988	3 139:12.27E	2915	-	1402	65:02.92S	139:12.18E	2915
196 F3.12	1512 2	3-AUG-95	65:01.65S	139:00.33E 2617	498	1526	65:01.628	3 139:00.37E	2622	-	1538	65:01.59S	139:00.33E	2622
197 F3.13	1655 2	3-AUG-95	65:00.33S	138:49.08E 2317	498	1706	65:00.308	3 138:49.08E	2312	-	1718	65:00.25S	138:49.05E	2312
198 F3.14	1902 2	3-AUG-95	64:58.87S	138:37.50E 2522	498	1916	64:58.869	S 138:37.47E	2517	-	1930	64:58.86S	138:37.50E	2522
199 F3.15	2110 2	3-AUG-95	64:57.75S	138:25.71E 2211	498	2120	64:57.778	3 138:25.69E	-	-	2137	64:57.71S	138:25.77E	-
200 F3.16	0022 2	4-AUG-95	64:56.60S	138:14.10E 2576	500	0035	64:56.588	3 138:14.09E	2566	-	0050	64:56.55S	138:14.04E	2573
201 F3.17	0254 2	4-AUG-95	64:51.57S	138:17.44E 2626	500	0305	64:51.588	S 138:17.37E	2633	-	0323	64:51.55S	138:17.37E	2640
202 SR3	1840 2	6-AUG-95	61:20.97S	139:52.00E 4402	4394	2046	61:19.938	3 139:53.78E	4402	20.1	2230	61:19.68S	139:54.45E	4402
203 SR3	0253 2	7-AUG-95	60:51.05S	139:50.80E 4491	4462	0438	60:52.418	S 139:49.81E	-	-	0616	60:53.098	139:49.96E	-
204 SR3	0934 2	7-AUG-95	60:21.52S	139:50.65E 4505	4502	1112	60:21.245	S 139:51.14E	-	16.1	1305	60:21.52S	139:51.40E	-
205 SR3	1532 2	9-AUG-95	52:05.57S	143:29.56E 3563	3584	1703	52:06.939	S 143:30.40E	3543	15.1	1831	52:08.37S	143:31.36E	3533
206 SR3	2101 2	9-AUG-95	51:48.87S	143:38.08E 3450	3696	2240	51:48.998	S 143:39.64E	-	23.1	0027	51:48.67S	143:40.63E	-
207 SR3	0257 3	0-AUG-95	51:32.13S	143:46.77E 3757	3796	0435	51:31.898	S 143:47.71E	-	15.3	0554	51:31.35S	143:48.27E	-
208 SR3	1020 3	0-AUG-95	51:16.18S	143:54.75E 3757	3828	1206	51:16.51	3 143:55.39E	-	25.0	1326	51:16.62S	143:56.33E	-

<u>Table 1.3:</u> Summary of samples drawn from Niskin bottles at each station, including salinity (sal), dissolved oxygen (do), nutrients (nut), dissolved inorganic carbon (dic), dissolved organic carbon (doc), iodate/iodide (i), primary productivity (pp), and the following biological samples: pigments (pig), microscopial protist examination (pro), cyanobacteria counts (cya), lugols iodine fixed plankton counts (lug), scanning and transmission electron microscopy (te), subsample of protist concentrate preserved (vir), and samples for culturing (cul). Note that 1=samples taken, 0=no samples taken, 2=surface sample only (i.e. from shallowest Niskin bottle).

station	sal	do	nut	dic	doc	i	pp			-biol cya				
1 TEST 2 SR3 3 SR3 4 SR3 5 SR3 6 SR3 7 SR3 8 SR3 9 SR3 10 SR3 11 SR3 12 SR3 13 SR3 14 SR3 15 SR3 16 SR3 17 SR3 18 SR3 19 SR3 20 SR3 21 SR3 22 SR3 23 SR3 24 SR3 25 SR3 26 SR3 27 SR3 28 SR3 29 SR3 30 SR3 31 SR3 32 SR3 33 SR3 34 SR3 35 SR3 36 SR3 37 SR3 38 SR3	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0200200200200200200200200200200202020202	0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 1 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	pig 0 1 0 1 0 1 0 1 0 1 0 0 1 0 1 0 0 1 1 0 0 0 1 1 0 0 1 0 1 0 0 1 0 1 0 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 0 1 0 0 1 0 0 0 1 0 0 1 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0	pro	cya 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 0 0 1 0 1 0 0 0 1 1 0 0 0 0 1 1 0 0 0 0 1 1 0 0 0 0 1 1 0 0 0 0 1 1 0 0 0 0 1 1 0 0 0 0 1 1 0 0 0 0 0 1 0	0 0 0 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 0 0	te 0000000000000100000001000001101000000	vir 0000000000001000000010001010110	cul 000000000000010000000100000001000000

Table 1.3: (continued)

										bio	loav	/		
station	sal	do	nut	dic	doc	i	pp	pig	pro	cya	lug	te	vir	cul
47 SR3	1	1	1	0	0	0	0	0	0	0	0	0	0	0
48 SR3	1	1	1	1	0	1	1	1	1	1	0	1	1	Ö
49 SR3	1	1	1	0	Ö	0	0	1	1	0	0	0	1	Ö
50 SR3	1	1	1	2	1	0	0	0	0	0	0	0	0	0
51 SR3	1	1	1	2	0	1	0	1	1	1	0	0	1	0
52 SR3	1	1	1	0	0	0	0	0	0	0	0	0	0	Ö
53-56 F1.1-F1.5	1	1	1	Ö	Ö	Ö	Ö	0	Ö	0	0	Ö	0	Ö
57 F1.5	1	1	1	0	0	0	1	1	0	0	0	0	0	0
58-66 F1.6-1.14	1	1	1	0	0	0	0	0	0	0	0	0	0	0
67 F1.15	1	1	1	0	0	0	1	1	1	1	0	0	1	0
68-77 F1.16-1.25	1	1	1	0	0	0	0	0	0	0	0	0	0	0
78 F1.26	1	1	1	0	0	0	1	1	1	1	0	0	0	0
79-94 F1.27-1.42	1	1	1	0	0	0	0	0	0	0	0	0	0	0
95 F1.43	1	1	1	0	0	0	1	1	1	1	0	0	1	0
96-100 F1.44-1.4	8 1	1	1	0	0	0	0	0	0	0	0	0	0	0
101 SR3	1	1	1	2	1	1	0	1	1	1	0	0	1	0
102 SR3	1	1	1	2	0	0	0	0	0	0	0	0	0	0
103 SR3	1	1	1	0	0	1	0	1	1	0	0	0	1	0
104 TEST	1	0	1	0	0	0	0	0	0	0	0	0	0	0
105 TEST	1	0	0	0	0	0	0	0	0	0	0	0	0	0
106-109 F2.19-2.2	22 1	1	1	0	0	0	0	0	0	0	0	0	0	0
110 F2.23	1	1	1	0	0	0	0	1	1	0	1	0	0	0
111-113 F2.24-2.2	26 1	1	1	0	0	0	0	0	0	0	0	0	0	0
114 F2.27	1	1	1	0	2	0	0	0	0	0	0	0	0	0
115-124 F2.28-2.3		•	1	0	0	0	0	0	0	0	0	0	0	0
125 F2.38	1	1	1	0	2	0	1	1	1	0	1	0	0	0
126 F2.39	1	1	1	0	2	0	0	0	0	0	0	0	0	0
127-128 F2.40-2.4		•	1	0	0	0	0	0	0	0	0	0	0	0
129 F2.42	1	1	1	0	2	0	0	0	0	0	0	0	0	0
130 F2.43	1	1	1	0	0	0	0	0	0	0	0	0	0	0
131 F2.44	. 1	1	1	0	2	0	0	0	0	0	0	0	0	0
132-135 F2.45-2.4			1	0	0	0	0	0	0	0	0	0	0	0
136 F2.1	1	1	1	0	0	0	1	1	1	0	1	0	1	0
137 F2.2	1	1	1	0	0	0	0	0	0	0	0	0	0	0
138 F2.3	1	1	1	0	2	0	0	0	0	0	0	0	0	0
139-144 F2.4-2.9	1	1	1	0	0	0	0	0	0	0	0	0	0	0
145 F2.10	1	1	1	0	2	0	0	1	1	0	1	0	1	0
146-151 F2.11-2.1	ו סו 1		1	0	0	0	0	0	0	0	0	0	0	0
152 F2.17 153 F2.18	1	1 1	1 1	0 0	2 2	0	0	0 1	0	0	0	0	0	0
154-159 F3.18-3.2	-	-	1	0	0	0	0 0	0	0	0	0	0	0	0
160 F3.24	ı د <u>.</u> 1	1	1	0	2	0	0	0	0	0	0	0	0	0
161 F3.25	1	1	1	0	2	0	0	1	0	0	0	0	0	0
162 F3.26	1	1	1	0	2	0	0	0	0	0	0	0	0	0
163 F3.27	1	1	1	0	2	0	0	0	0	0	0	0	0	0
164-173 F3.28-3.3	-	-	1	0	0	0	0	0	0	0	0	0	0	0
174 F3.38	י יכ 1	1	1	0	2	0	0	0	0	0	0	0	0	0
174 F3.36 175 F3.39	1	1	1	0	2	0	0	1	0	0	0	0	0	0
176 F3.40	1	1	1	0	0	0	0	0	0	0	0	0	0	0
177 F3.41	1	1	1	0	2	0	0	0	0	0	0	0	0	0
178 F3.42	1	1	1	0	0	0	0	0	0	0	0	0	0	0
179 F3.43	1	1	i	0	2	0	0	0	0	0	0	0	0	0
180-181 F3.44-3.4	15 1		1	0	0	0	Ö	0	0	0	0	0	0	0

Table 1.3: (continued)

											bio	log	/		
station	sal	l	do r	nut	dic	doc	i	pp	pig	pro	cya	lug	j te	vir	cul
182 F3.46		1	1	1	0	2	0	0	0	0	0	0	0	0	0
	_	ا •	•	•	•	_	-	•	•	•	•	•	•	-	-
183-187 F3.47-3.		1	1	1	0	0	0	0	0	0	0	0	0	0	0
188-189 F3.4-F3.	5	1	1	1	0	2	0	0	0	0	0	0	0	0	0
190 F3.6	•	1	1	1	0	2	0	0	1	1	0	1	0	1	0
191 F3.7	•	1	1	1	0	0	0	0	0	0	0	0	0	0	0
192 F3.8	•	1	1	1	0	2	0	0	0	0	0	0	0	0	0
193-200 F3.9-F3.	16	1	1	1	0	0	0	0	0	0	0	0	0	0	0
201 F3.17	•	1	1	1	0	0	0	0	1	0	0	1	0	0	0
202 SR3	•	1	1	1	0	0	0	0	1	0	0	0	0	0	0
203 SR3	•	1	1	1	0	0	0	0	0	0	0	0	0	0	0
204 SR3	•	1	1	1	0	0	0	0	0	0	0	0	0	0	0
205 SR3	•	1	1	1	2	0	0	0	1	1	1	1	0	1	0
206 SR3	•	1	1	1	0	0	0	0	0	0	0	0	0	0	0
207 SR3	•	1	1	1	0	0	0	1	1	1	1	1	0	1	0
208 SR3	•	1	1	1	2	0	0	0	0	0	0	0	0	0	0

<u>Table 1.4:</u> CTD stations over current meter (CM) and inverted echo sounder (IES) moorings along SR3 transect in the vicinity of the Subantarctic Front. Note that bottom depths are calculated using a sound speed of 1498 ms<sup>-1</sup>. For CTD station positions, see Table 1.2.

CTD station no.	start time	bottom depth (m)	mooring number
12	03:18, 21/07/95	4064	I1 (IES)
16	03:38, 22/07/95	3686	12 (IES)
17	08:49, 22/07/95	3788	I4 (IES)
18	14:14, 22/07/95	3711	16 (IES)
19	19:08, 22/07/95	3583	I8 (CM+IES)
20	00:31, 23/07/95	3655	I9 (CM+IES)
21	05:03, 23/07/95	3808	I10 (CM+IES)
22	09:52, 23/07/95	3706	112 (IES)
23	14:51, 23/07/95	3778	114 (IES)
24	20:04, 23/07/95	3757	116 (IES)
25	00:55, 24/07/95	3512	118 (IES)
205	15:32, 29/08/95	3563	117 (IES)
206	21:01, 29/08/95	3450	115 (IES)
207	02:57, 30/08/95	3757	113 (IES)
208	10:20, 30/08/95	3757	111 (IES)

<u>Table 1.5a:</u> Principal investigators (\*=cruise participant) for water sampling programmes.

measurement	name	affiliation
CTD, salinity, O <sub>2</sub> , nutrients (SR3) CTD, salinity, O <sub>2</sub> (FORMEX) D.O.C. iodate/iodide primary productivity biological sampling	Steve Rintoul/*Nathan Bindoff *Nathan Bindoff/*lan Allison Tom Trull Ed Butler John Parslow Harvey Marchant	CSIRO/Antarctc CRC Antarctic CRC/Antarctic Division Antarctic CRC CSIRO CSIRO Antarctic Division
D.I.C.	Bronte Tilbrook	CSIRO

<u>Table 1.5b:</u> Scientific personnel (cruise participants).

name	measurement	affiliation
Nathan Bindoff Ross Edwards Brett Goldsworthy Phil Reid Mark Rosenberg Chris Zweck	CTD CTD, trace metals CTD CTD CTD CTD, moorings CTD	Antarctic CRC
Steve Bell Stephen Bray Martina Doblin	salinity, oxygen, nutrients salinity, oxygen, nutrients oxygen	Antarctic CRC Antarctic CRC Antarctic CRC
Mick Mackey	primary productivity	Antarctic CRC
Rick van den Enden Ian Jameson	biological sampling biological sampling	Antarctic Division Antarctic Division
lan Allison Petra Heil Ian Knott Vicky Lytle Rob Massom Anton Rada Tony Worby	voyage leader, sea ice sea ice sea ice, electronics sea ice sea ice sea ice deputy voyage leader, sea ice	Antarctic Division Antarctic CRC Antarctic CRC Antarctic CRC Antarctic CRC Antarctic CRC Antarctic Division Antarctic Division
Greg Bush Alec Duncan	upward looking sonar upward looking sonar	Curtin University Curtin University
Kevin Bartram Dion Hobcroft		Australasian Ornithologists Union Australasian Ornithologists Union
Peter Gill Debbie Thiele	whale observations whale observations	Ocean Research Foundation Ocean Research Foundation
Pamela Brodie Andrew Climie Vera Hansper Graham Hosie Andrew McEldowney Tim Pauly Tim Ryan Hyong-chul Shin Wojciech Wierzbicki	computing doctor computing sea ice biology gear officer hydroacoustics underway measurements sea ice biology electronics	Antarctic Division
Peter Colpo Adrian Pate Rick Piacenza	helicopters helicopters helicopters	Helicopter Resources Helicopter Resources Helicopter Resources
Ian McCarthy	weather forecaster	Bureau of Meteorology

#### 1.4 FIELD DATA COLLECTION METHODS

#### 1.4.1 CTD and hydrology measurements

In this section, CTD and hydrology data collection and processing methods are discussed. Preliminary results of the CTD data calibration, along with data quality information, are presented in Section 1.6. CTD instrumentation and CTD and hydrology data collection techniques are described in detail in Rosenberg et al. (1995b). Water sampling methods are also detailed in previous data reports.

#### 1.4.1.1 CTD Instrumentation

Briefly, General Oceanics Mark IIIC (i.e. WOCE upgraded) CTD units were used, with General Oceanics model 1015 pylons, and 10 litre General Oceanics Niskin bottles. A 24 position rosette package was deployed for stations 1 to 52 and 202 to 208 along the SR3 transect, with deep sea reversing thermometers (Gohla-Precision) mounted at rosette positions 2, 12 and 24. A Li-Cor photosynthetically active radiation sensor and Sea-Tech fluorometer were also attached to the package for some casts (Table 1.20). For stations 53 to 201, a 12 position rosette package was deployed. For most FORMEX stations, 6 bottles only were mounted, at alternate rosette positions, and with reversing thermometers at rosette position 2. Extra bottles were mounted for some FORMEX stations for the collection of biological samples (Table 1.3). For stations 101 to 105, 12 Niskin bottles were mounted.

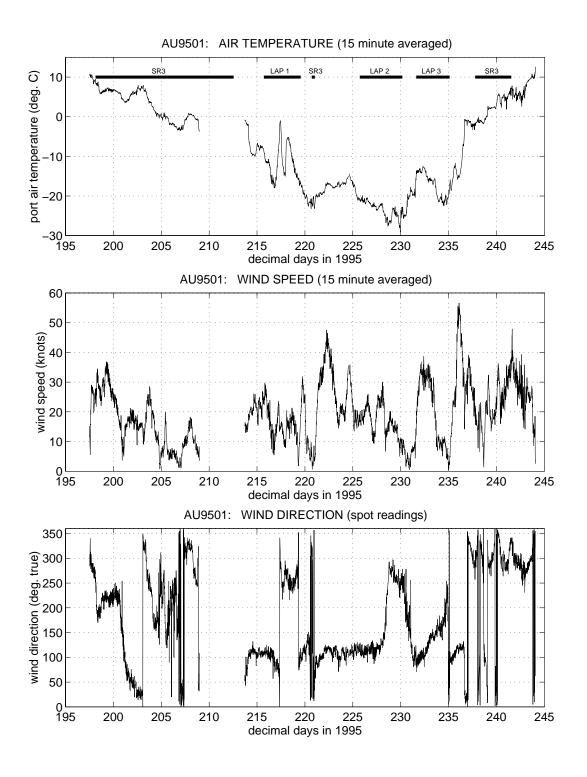
#### 1.4.1.2 CTD instrument and data calibration

Complete calibration information for the CTD pressure, platinum temperature and pressure temperature sensors are presented in Table 1.22. Post cruise pressure, platinum temperature and pressure temperature calibrations, performed at the CSIRO Division of Marine Research Calibration Facility, were available for all CTD units. The complete CTD conductivity and the limited CTD dissolved oxygen calibrations, derived respectively from the in situ Niskin bottle salinity and dissolved oxygen samples, are presented in a later section.

Manufacturer supplied calibrations were applied to the p.a.r. data, while fluorometer calibrations were performed at the Antarctic Division (Table 1.22). These calibrations are not expected to be correct - correct scaling of fluorescence data requires linkage with primary productivity data, while p.a.r. data requires recalculation using extinction coefficients for the signal strength (B. Griffiths, pers. comm.).

The CTD and hydrology data processing and calibration techniques are described in detail in Appendix 2 of Rosenberg et al. (1995b) (referred to as "CTD methodology" for the remainder of the report), with the following updates to the methodology:

- (i) the 10 seconds of CTD data prior to each bottle firing are averaged to form the CTD upcast for use in calibration (5 seconds was used previously);
- (ii) for stations 30 to 44, the minimum number of data points required in a 2 dbar bin to form an average was set to 6 (i.e. jmin=6; for other stations, jmin=10);
- (iii) in the conductivity calibration for stations 30 to 44, an additional term was applied to remove the pressure dependent conductivity residual;
- (iv) CTD raw data obtained from the CTD logging PC's no longer contain end of record characters after every 128 bytes.



<u>Figure 1.2:</u> Air temperature and wind speed and direction for cruise AU9501 from ship's underway data, including times of various cruise components (SR3 and FORMEX laps 1, 2 and 3). Note that decimal time = 0.0 at midnight of 31st December (so, e.g., midday on 2nd January = 1.5).

#### 1.4.1.3 CTD/hydrology data collection techniques in cold conditions

Extreme cold was experienced for much of the cruise (Figure 1.2), and most of the time during FORMEX the oceanographic operations were conducted in consolidated sea ice. As a result, new methods had to be developed for deployment of the rosette package. In particular, great care had to be taken to minimize freezing of the CTD sensors. After arriving on station, the ship had to first clear a hole in the sea ice (in thicker ice, this operation took up to 1 hour). During the CTD cast, stern thrusters were used to keep ice clear of the CTD wire. Bow thruster usage was minimized during FORMEX, to ensure good ADCP data whilst on station.

CTD sensor caps were filled with hypersaline water to depress the freezing point of water on the sensors. To minimize exposure of the sensors to the cold air, the caps were not drained until the package was about to be lowered into the water; and the package was lowered promptly, and while still moving out towards the end of the gantry. Adherence to these steps minimized sensor freezing, however near surface downcast conductivity data were still affected by a thin film of frozen water remaining on the conductivity cell. Upcast data were therefore used for stations 53 to 201.

When the package was retrieved, water was often frozen in the Niskin bottle spiggots, and sampling was delayed by approximately 10 to 15 minutes to allow thawing of the spiggots. On several occasions, the flow during sampling for dissolved oxygen was interrupted due to incomplete thawing, causing a long delay between opening of the Niskin bottle vent valve and taking of the sample. Dissolved oxygen samples thus affected were not analysed.

#### 1.4.1.4 Hydrology analytical methods

The analytical techniques and data processing routines employed in the Hydrographic Laboratory onboard the ship are discussed in Appendix 3 of Rosenberg et al. (1995b). Note the following changes to the methodology:

- (i) 150 ml sample bottles were used, and 1.0 ml of reagents 1, 2 and 3 were used; the corresponding calculated value for the total amount of oxygen added with the reagents = 0.017 ml;
- (ii) a mean volume of 147.00 ml for oxygen sample bottles was applied in the calculation of dissolved oxygen concentration.

#### 1.4.2 Underway measurements

Underway data collection is as described in previous data reports; data files are described in Part 5. Note that a sound speed of 1498 ms<sup>-1</sup> is used for all depth calculations, and the ship's draught of 7.3 m has been accounted for in final depth values (i.e. depths are values from the surface).

#### Table 1.6: ADCP logging parameters.

ping parameters bottom track ping parameters

no. of bins: 60 no. of bins: 128 bin length: 8 m bin length: 4 m pulse length: 8 m pulse length: 32 m

delay: 4 m

ping interval: minimum ping interval: same as profiling pings

reference layer averaging: bins 3 to 6 ensemble averaging duration: 3 min.

#### 1.4.3 ADCP

The acoustic Doppler current profiler (ADCP) instrumentation is described in Rosenberg et al. (1996). GPS data was collected by a Lowrance receiver for the first half of the cruise, and a Koden receiver for the second half. Note that the Lowrance unit received GPS positions every 2 seconds, and GPS velocities every 2 seconds, with positions and velocities received on alternate seconds; the Koden unit received both GPS positions and velocities every 1 second. ADCP data processing is discussed in more detail in Dunn (a and b, unpublished reports). Logging parameters are summarised in Table 1.6, while data results for this cruise will be discussed in a future report.

# 1.5 MAJOR PROBLEMS ENCOUNTERED

#### 1.5.1 Logistics

Rough weather on the return northward leg prevented CTD measurements being taken at 3 of the inverted echo sounder mooring locations (mooring numbers I3, I5 and I7). Time was not available to wait for calmer conditions.

#### 1.5.2 CTD sensors

No good CTD dissolved oxygen data was obtained from CTD 1103. The problem, not diagnosed until after the cruise, was traced to an incorrectly wired oxygen sensor bulkhead connector (a factory fault). As a result, usable CTD dissolved oxygen data was only obtained from the limited number of stations where CTD 1193 was used.

The conductivity cell for CTD 1193 was faulty, displaying a large transient error when first entering the water (requiring several minutes to drift to a stable value), large hysteresis between the down and upcasts, and significant pressure dependent residuals. Conductivity data was recoverable for stations 30 to 41 (see section 1.6), but was unusable for stations 42 to 44 and 104 to 105.

Following station 50, a crack was discovered in the housing window for the photosynthetically active radiation sensor. The sensor was not used for the remainder of the cruise.

#### 1.5.3 Other equipment

Very cold conditions were experienced during the cruise (Figure 1.2). When the air temperature dropped below -20°C, icing of the CTD wire became a problem, causing jamming of the wire in the spooling sheath. On the worst occasion, several turns came off the winch drum, and several hundred metres of wire were badly kinked.

The Lowrance GPS receiver, accessed by the ADCP logging system, failed on 13/07/95. The replacement Koden unit came on line on 16/07/95. The missing 3 days of GPS data for the ADCP were obtained from data logged by the Magnavox GPS unit.

#### 1.6 CTD RESULTS

This section details information relevant to the creation and quality of the final CTD and hydrology data set. For actual use of the data, the following is important:

CTD data - Tables 1.14 and 1.15, and Table 1.7; hydrology data - Table 1.19.

Historical data comparisons are made in Part 4 of this report. Data file formats are described in Part 5.

#### 1.6.1 CTD measurements - data creation and quality

CTD data calibration and processing methods are described in detail in the CTD methodology (i.e. Appendix 2 of Rosenberg et al., 1995b, with the additions listed in section 1.4.1.2 of this report). Cases for cruise au9501 which vary from this methodology are detailed in this section. CTD data quality is also discussed. For conversion to WOCE data file formats, see Part 5 of this report.

The final calibration results for conductivity/salinity and dissolved oxygen, along with the performance check for temperature, are plotted in Figures 1.3 to 1.6. For temperature, salinity and dissolved oxygen, the respective residuals ( $T_{therm}$  -  $T_{cal}$ ), ( $s_{btl}$  -  $s_{cal}$ ) and ( $o_{btl}$  -  $o_{cal}$ ) are plotted. For conductivity, the ratio  $c_{btl}/c_{cal}$  is plotted.  $T_{therm}$  and  $T_{cal}$  are respectively the protected thermometer and calibrated upcast CTD burst temperature values;  $s_{btl}$ ,  $s_{cal}$ ,  $o_{btl}$ ,  $o_{cal}$ ,  $c_{btl}$  and  $c_{cal}$ , and the mean and standard deviation values in Figures 1.3 to 1.6, are as defined in the CTD methodology (with additional definitions described below for cases where a pressure dependent residual is removed from conductivity data).

#### 1.6.1.1 Conductivity/salinity

An excellent conductivity calibration was obtained for CTD 1103 (stations 1-29, 45-103 and 106-208) - after calibrating against bottle data, low residuals were obtained between CTD and bottle values (Figures 1.4a and 1.5a). Note that a new conductivity cell was installed on this CTD at the start of the cruise. Upcast CTD data was used for stations 53 to 103 and 106-201, owing to sensor freezing (as described in section 1.4.1.3).

The conductivity cell for CTD 1193 (stations 30-44 and 104-105) was faulty, as described in section 1.5.2. Upcast CTD data were used for these stations, due to the large transient error in conductivity when entering the water, and the significant hysteresis between downcast and upcast conductivity data. The pressure dependent conductivity residual for this cell was removed by the following steps:

- (a) CTD conductivity was initially calibrated to derive conductivity residuals ( $c_{btl}$   $c_{cal}$ ), where  $c_{btl}$  and  $c_{cal}$  are as defined in the CTD methodology, noting that  $c_{cal}$  is the conductivity value after the initial calibration only i.e. prior to any pressure dependent correction.
- (b) Next, for each station grouping (Table 1.9), a linear pressure dependent fit was found for the conductivity residuals i.e. for station grouping i, fit parameters  $\alpha_i$  (Table 1.9) and  $\beta_i$  were found from

$$(c_{btl} - c_{cal})_n = \alpha_i p_n + \beta_i$$
 (eqn 1.1)

where the residuals  $(c_{btl} - c_{cal})_n$  and corresponding pressures  $p_n$  (i.e. pressures where Niskin bottles fired) are all the values accepted for conductivity calibration in the station grouping.

(c) Lastly, the conductivity calibration was repeated, this time fitting ( $c_{ctd} + \alpha_i p$ ) to the bottle values  $c_{btl}$  in order to remove the linear pressure dependence for each station grouping i (for uncalibrated conductivity  $c_{ctd}$  as defined in the CTD methodology; and note that the offsets  $\beta_i$  were not applied).

A good conductivity calibration was obtained for stations 30 to 41 using this method (Figures 1.4b and 1.5b). However for stations 42 to 44 and 104 to 105, the conductivity data was not recoverable, owing to rapid deterioration of the cell.

The final standard deviation values for the salinity residuals (Figure 1.5) indicate the CTD salinity data over the whole cruise is accurate to within  $\pm 0.002$  (PSS78).

#### 1.6.1.2 Temperature

The comparison of CTD and thermometer temperatures is shown in Figure 1.3. The thermometer value used in each case is the mean of the two protected thermometer readings (protected thermometers used are listed in Table 1.21). Note that in the figures, the "dubious" and "rejected" categories refer to corresponding bottle samples and upcast CTD bursts in the conductivity calibration, rather than to CTD/thermometer temperature values.

Platinum temperature sensor performance of CTD's 1103 and 1193 is not consistent, as shown by the different offsets in Figures 1.3a and b. For CTD 1193 (Figure 1.3b), the offset is small (~+0.001°C), indicating a reliable laboratory calibration of the platinum temperature sensor. The offset for CTD 1103 of ~-0.007°C (Figure 1.3a), using the post cruise temperature calibration, is large. If the pre cruise temperature calibration (September 1994) is applied, the offset is ~+0.007°C, thus a significant calibration drift occurred for this CTD between the two laboratory calibrations. No attempt has been made to correct for this calibration drift, and the post cruise calibration is maintained. Note that over the actual period of the cruise, there was little calibration drift for CTD 1103, other than a possible small drift for stations 202-208 (although these stations were too few in number to confirm the trend).

#### **1.6.1.3 Pressure**

As described in previous data reports, noise in the pressure signal for CTD 1193 (used for stations 30 to 44 and 104 to 105) was high, with spikes of up to 1 dbar amplitude occurring, and with a large number of missing 2 dbar bins resulting. The number of missing bins was reduced by setting to 6 the minimum number of data points required in a 2 dbar bin to form an average (i.e. jmin=6; for CTD 1103 stations, jmin=10). For remaining missing bins, values were linearly interpolated between surrounding bins, except where the local temperature gradient exceeded 0.005°C between the surrounding bins i.e. temperature gradient > 0.00125 degrees/dbar.

For stations 22, 128 and 190, data logging commenced when the CTD was already in the water, so surface pressure offset values were estimated from surrounding stations. For stations 144 and 168, conductivity cell freezing interfered with the automatic estimation of surface pressure offsets (see CTD methodology), so surface pressure offset values were estimated from a manual inspection of the pressure data. Note that for all these stations, any resulting additional error in the CTD pressure data is judged to be small (no more than 0.2 dbar).

#### 1.6.1.4 Dissolved oxygen

Usable CTD dissolved oxygen data was only obtained from CTD 1193, stations 30 to 41, as discussed in section 1.5.2. For these stations, downcast oxygen temperature and oxygen current data were merged with the upcast pressure, temperature and conductivity data (upcast dissolved oxygen data is in general not reliable). With this data set, calibration of the dissolved oxygen data then followed the usual methodology. Note that for many of these stations, near surface CTD dissolved oxygen data were bad (Table 1.12).

A small additional error in CTD dissolved oxygen data is expected to occur from the merging of downcast oxygen data with upcast pressure, temperature and conductivity data - where horizontal gradients occur, there will be some mismatch of downcast and upcast data as the ship drifts during a CTD cast. At most, this error is not expected to exceed ~3%.

The dissolved oxygen residuals are plotted in Figure 1.6. The final standard deviation values are within ~1.2% of full scale values (where full scale is approximately equal to 250  $\mu$ mol/l for pressure > 750 dbar, and 350  $\mu$ mol/l for pressure < 750 dbar). Note that the standard deviation values are a little larger than for previous cruises, indicating a larger spread in the residuals for each station (Figure

1.6). The best calibration was achieved using large values of the order 13.0 for the coefficient  $K_1$  (i.e. oxygen current slope), and large negative values of the order -2.0 for the coefficient  $K_3$  (i.e. oxygen current bias) (Table 1.16). This, however, is not considered relevant to actual data quality.

#### 1.6.1.5 Fluorescence and P.A.R. data

As discussed in section 1.4 above, fluorescence and p.a.r. are effectively uncalibrated. These data should not be used quantitatively other than for linkage with primary productivity data.

**Table 1.7:** Summary of cautions to CTD data quality.

station no.	CTD parameter	caution
1	salinity	test cast - all bottles fired at same depth; salinity accuracy reduced
22	pressure	surface pressure offset estimated from surrounding stations
31	oxygen	dissolved oxygen data could not be calibrated due to bad bottle data
42-44	oxygen	no CTD dissolved oxygen data due to bad conductivity data
45	salinity	most bottles tripped on the fly, which may introduce small inaccuracy
		into the conductivity calibration
104-105	all parameters	data not used for these stations (test casts only)
128	pressure	surface pressure offset estimated from surrounding stations
144	pressure	surface pressure offset estimated manually
168	pressure	surface pressure offset estimated manually
190	pressure	surface pressure offset estimated from surrounding stations
1-29, 45-208	oxygen	no CTD dissolved oxygen data due to faulty hardware
30-41	salinity	additional correction applied for pressure dependent conductivity
		residual
all CTD1103 stns temperature		
all stns fluorescence/p.a.r. f		fluorescence and p.a.r. sensors (where active) are uncalibrated

#### 1.6.1.6 Summary of CTD data creation

stations 1-29 and 42-208: no CTD dissolved oxygen data;

stations 30-44: all CTD data from upcast (except dissolved oxygen); pressure dependent conductivity residual removed;

stations 53-103 and 106-201: all CTD data from upcast;

Further information relevant to the creation of the calibrated CTD data is tabulated, as follows:

- \* Surface pressure offsets calculated for each station are listed in Table 1.8.
- \* CTD conductivity calibration coefficients, including the station groupings used for the conductivity calibration, are listed in Tables 1.9 and 1.10.
- \* CTD raw data scans flagged for special treatment are listed in Table 1.11.
- \* Missing 2 dbar data averages are listed in Table 1.12.
- \* 2 dbar bins which are linearly interpolated from surrounding bins are listed in Table 1.13.

- \* Suspect 2 dbar averages are listed in Tables 1.14 and 1.15.
- \* CTD dissolved oxygen calibration coefficients are listed in Table 1.16. The starting values used for the coefficients prior to iteration, and the coefficients varied during the iteration, are listed in Table 1.17.
- \* Stations containing fluorescence and photosynthetically active radiation data are listed in Table 1.20.
- \* The different protected and unprotected thermometers used for the stations are listed in Table 1.21.
- \* Laboratory calibration coefficients for the CTD's are listed in Table 1.22.

#### 1.6.1.7 Summary of CTD data quality

CTD data quality cautions for the various parameters are summarised in Table 1.7.

#### 1.6.2 Hydrology data

Quality control information relevant to the hydrology data is tabulated, as follows:

- \* Dissolved oxygen Niskin bottle samples flagged with the code -9 (rejected for CTD dissolved oxygen calibration) are listed in Table 1.18.
- \* Questionable nutrient Niskin bottle sample values are listed in Table 1.19. Note that questionable values are included in the hydrology data file, whereas bad values have been removed. Also note that there are no questionable dissolved oxygen bottle samples.

For station 45, the cast was abandoned at ~1000 m above the bottom on the downcast, due to ice bearing down on the ship. During retrieval, bottles at rosette positions 2 to 19 were tripped while the instrument package was still moving.

#### 1.6.2.1 Nutrients

As discussed in previous data reports, additional "dummy" samples drawn from the Niskin bottles were inserted in autoanalyser runs immediately following wash solution vials to artificially mask the suppression effect on subsequent phosphate samples (see section 6.2.1 in Rosenberg et al., 1995b). As a result, no phosphate data was lost.

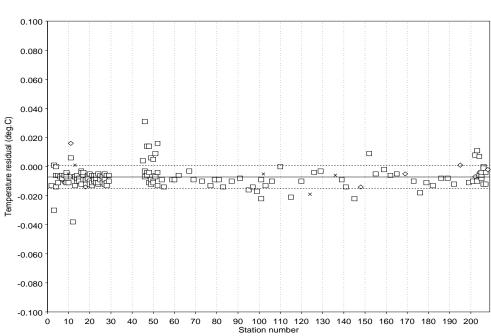
Laboratory temperature on the ship was stable, with lab temperatures at the times of nutrient analyses having a most common value of 18°C.

#### 1.6.2.2 Dissolved oxygen

Dissolved oxygen bottle data for stations 14, 23, 31 and 44 were unusable, as the bottles had not been adequately shaken following the addition of reagents during sampling.

Dissolved oxygen bottle values for stations 1 to 21 are  $\sim 6\mu$ mol/l smaller than for the remaining stations, due to drift of the laboratory standardisation values for the first 21 stations. See Part 4 of this report for a more detailed discussion.





dubious

rejected

Calibration data for cruise: Au9501

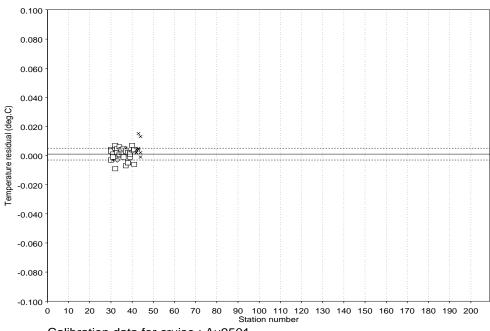
Calibration file: CTD1103.lis

good

Mean offset Temperature = -.00709312c (s.d. = 0.0078 °c)

Number of samples used = 155 out of 161

(b)



Calibration data for cruise: Au9501

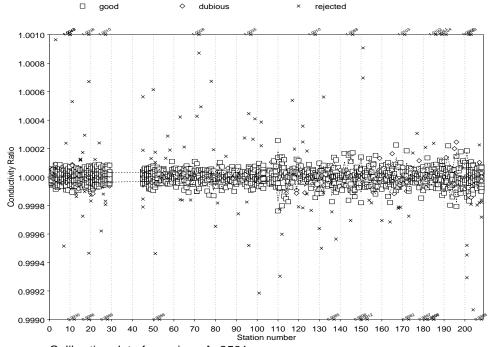
Calibration file: CTD1193.lis

Mean offset Temperature = 0.00106312c (s.d. = 0.0041 °c)

Number of samples used = 33 out of 44

Figure 1.3: Temperature residual (Ttherm - Tcal) versus station number for cruise au9501 for stations using (a) CTD1103, and (b) CTD 1193. The solid line is the mean of all the residuals; the broken lines are  $\pm$  the standard deviation of all the residuals (see CTD methodology). Note that the "dubious" and "rejected" categories refer to the conductivity calibration.

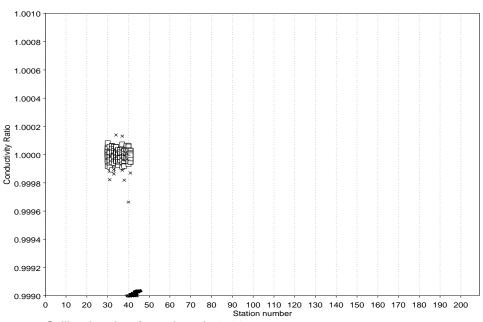




Calibration data for cruise : Au9501 Calibration file : CTD1103.lis Conductivity s.d. = 0.00005

Number of bottles used = 1731 out of 1911 Mean ratio for all bottles = 1.00000

(b)



Calibration data for cruise: Au9501

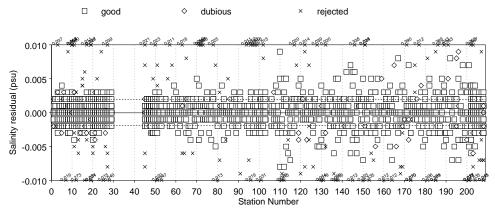
Calibration file: CTD1193.lis Conductivity s.d. = 0.00003

Number of bottles used = 275 out of 359 Mean ratio for all bottles = 1.00000

Comment:

<u>Figure 1.4:</u> Conductivity ratio  $c_{btl}/c_{cal}$  versus station number for cruise au9501 for stations using (a) CTD1103, and (b) CTD1193. The solid line follows the mean of the residuals for each station; the broken lines are  $\pm$  the standard deviation of the residuals for each station (see CTD methodology).

(a)



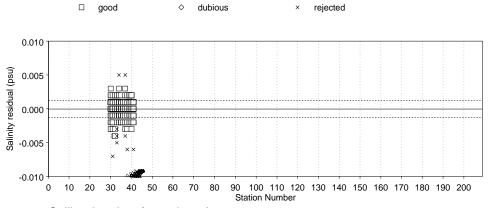
Calibration data for cruise : Au9501

Calibration file: CTD1103.lis

Mean offset salinity = 0.0000psu (s.d. = 0.0019 psu)

Number of bottles used = 1731 out of 1911

(b)



Calibration data for cruise: Au9501

Calibration file: CTD1193.lis

Mean offset salinity = 0.0000psu (s.d. = 0.0013 psu)

Number of bottles used = 275 out of 359

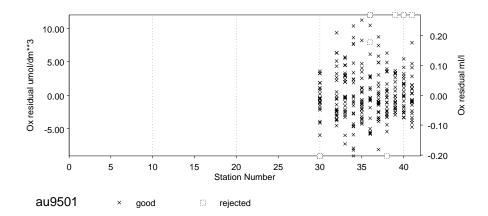
<u>Figure 1.5:</u> Salinity residual ( $s_{btl}$  -  $s_{cal}$ ) versus station number for cruise au9501 for stations using (a) CTD1103, and (b) CTD1193. The solid line is the mean of all the residuals; the broken lines are  $\pm$  the standard deviation of all the residuals (see CTD methodology).

Mean of Residual = -0.023umol/dm\*\*3

S.D. of residual = 3.591umol/dm\*\*3 (Equiv to 0.080ml/l)

Used 252 bottles out of total 358

S.D. deep (>750m) 2.977umol/dm\*\*3 (equiv to 0.067ml/l)



 $\underline{Figure~1.6:}~$  Dissolved oxygen residual (o $_{btl}$  - o $_{cal}$ ) versus station number for cruise au9501 (CTD1193 stations only).

<u>Table 1.8:</u> Surface pressure offsets (as defined in the CTD methodology). \*\* indicates that value is estimated from surrounding stations, or else determined from manual inspection of pressure data.

number offset (dbar)         number offset (dbar)         number offset (dbar)         number offset (dbar)           1         0.99         53         0.13         105         -         157         1.04           2         0.63         54         0.33         106         0.23         158         1.14           3         0.49         55         0.21         107         0.78         159         1.26           4         0.46         56         0.14         108         1.21         160         0.95           5         0.50         57         0.23         109         1.13         161         0.85           6         0.28         58         -0.24         110         0.78         162         1.04           7         0.18         59         0.05         111         1.08         162         1.04           7         0.18         59         0.05         111         1.08         162         1.04           7         0.18         59         0.05         111         1.08         162         1.04           7         0.18         59         0.05         111         1.08         162         1.04     <	pressur station	e data. surface p	station	surface p	station	surface p	station s	surface p
2 0.63 54 0.33 106 0.23 158 1.14 3 0.49 55 0.21 107 0.78 159 1.26 4 0.46 56 0.14 108 1.21 160 0.95 5 0.50 57 -0.23 109 1.13 161 0.85 6 0.28 58 -0.24 110 0.78 162 1.04 7 0.18 59 0.05 111 1.08 163 0.97 8 0.45 60 -0.16 112 1.12 164 0.97 9 0.17 61 0.25 113 0.86 165 0.59 10 0.42 62 0.29 114 0.65 166 1.15 11 -0.23 63 0.13 115 1.04 167 0.78 12 0.22 64 -0.14 116 0.97 188 0.78* 13 0.13 65 0.27 117 0.95 169 1.29 14 0.13 66 0.23 118 0.61 170 1.04 15 -0.11 67 -0.06 119 0.77 171 1.21 16 0.14 68 0.35 120 1.17 172 0.97 17 -0.01 69 0.13 121 1.17 173 1.14 18 -0.19 70 0.05 122 1.19 174 0.96 19 0.00 71 -0.11 123 1.12 1.75 0.96 19 0.00 71 -0.11 123 1.12 1.75 0.96 20 -0.22 72 0.26 124 1.09 176 0.71 21 0.00 73 0.33 125 1.06 177 0.98 22 0.00** 74 0.44 126 0.98 178 0.91 22 0.00** 74 0.44 126 0.98 178 0.91 23 -0.57 75 0.12 127 1.13 179 0.78 24 0.05 76 0.23 128 1.00** 180 1.17 25 -0.28 77 0.26 129 0.88 181 0.71 26 -0.47 81 0.32 1.33 0.98 189 0.69 34 -0.47 81 0.32 1.33 0.98 185 0.86 30 -0.69 82 0.31 134 0.67 186 1.40 33 -2.29 85 0.09 137 0.98 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 190 0.66** 35 -1.30 87 0.12 139 1.03 191 0.63 36 -0.79 88 0.30 144 0.74 192 0.82 40 -0.98 92 0.18 144 0.96 193 0.81 31 -0.66 83 0.36 135 1.01 187 0.98 34 -1.26 9.47 81 0.32 133 0.98 189 0.69 34 -1.90 86 0.28 138 0.82 190 0.66** 35 -1.30 87 0.12 139 1.03 191 0.63 36 -0.79 88 0.30 140 0.74 192 0.82 37 -1.15 89 0.29 141 0.96 193 0.81 38 -1.21 90 0.12 142 0.99 194 0.93 39 -1.73 91 0.80 143 0.55 195 1.10 40 -0.98 92 0.18 144 0.45** 196 0.65 41 -0.70 1.90 0.06 185 0.09 107 0.26 125 0.06 0.70 45 0.06 99 0.73 151 0.82 203 0.70 46 0.03 98 0.29 150 0.36 200 0.79 47 0.06 99 0.73 151 0.82 203 0.70 48 0.19 100 0.26 152 1.16 0.99 205 0.60 50 -0.02 102 0.46 155 0.91 207 0.65								
2 0.63 54 0.33 106 0.23 158 1.14 3 0.49 55 0.21 107 0.78 159 1.26 4 0.46 56 0.14 108 1.21 160 0.95 5 0.50 57 -0.23 109 1.13 161 0.85 6 0.28 58 -0.24 110 0.78 162 1.04 7 0.18 59 0.05 111 1.08 163 0.97 8 0.45 60 -0.16 112 1.12 164 0.97 9 0.17 61 0.25 113 0.86 165 0.59 10 0.42 62 0.29 114 0.65 166 1.15 11 -0.23 63 0.13 115 1.04 167 0.78 12 0.22 64 -0.14 116 0.97 188 0.78* 13 0.13 65 0.27 117 0.95 169 1.29 14 0.13 66 0.23 118 0.61 170 1.04 15 -0.11 67 -0.06 119 0.77 171 1.21 16 0.14 68 0.35 120 1.17 172 0.97 17 -0.01 69 0.13 121 1.17 173 1.14 18 -0.19 70 0.05 122 1.19 174 0.96 19 0.00 71 -0.11 123 1.12 1.75 0.96 19 0.00 71 -0.11 123 1.12 1.75 0.96 20 -0.22 72 0.26 124 1.09 176 0.71 21 0.00 73 0.33 125 1.06 177 0.98 22 0.00** 74 0.44 126 0.98 178 0.91 22 0.00** 74 0.44 126 0.98 178 0.91 23 -0.57 75 0.12 127 1.13 179 0.78 24 0.05 76 0.23 128 1.00** 180 1.17 25 -0.28 77 0.26 129 0.88 181 0.71 26 -0.47 81 0.32 1.33 0.98 189 0.69 34 -0.47 81 0.32 1.33 0.98 185 0.86 30 -0.69 82 0.31 134 0.67 186 1.40 33 -2.29 85 0.09 137 0.98 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 190 0.66** 35 -1.30 87 0.12 139 1.03 191 0.63 36 -0.79 88 0.30 144 0.74 192 0.82 40 -0.98 92 0.18 144 0.96 193 0.81 31 -0.66 83 0.36 135 1.01 187 0.98 34 -1.26 9.47 81 0.32 133 0.98 189 0.69 34 -1.90 86 0.28 138 0.82 190 0.66** 35 -1.30 87 0.12 139 1.03 191 0.63 36 -0.79 88 0.30 140 0.74 192 0.82 37 -1.15 89 0.29 141 0.96 193 0.81 38 -1.21 90 0.12 142 0.99 194 0.93 39 -1.73 91 0.80 143 0.55 195 1.10 40 -0.98 92 0.18 144 0.45** 196 0.65 41 -0.70 1.90 0.06 185 0.09 107 0.26 125 0.06 0.70 45 0.06 99 0.73 151 0.82 203 0.70 46 0.03 98 0.29 150 0.36 200 0.79 47 0.06 99 0.73 151 0.82 203 0.70 48 0.19 100 0.26 152 1.16 0.99 205 0.60 50 -0.02 102 0.46 155 0.91 207 0.65	1	0.99	53	0.13	105	-	157	1.04
3         0.49         55         0.21         107         0.78         159         1.26           4         0.46         56         0.14         108         1.21         160         0.95           5         0.50         57         -0.23         109         1.13         161         0.85           6         0.28         58         -0.24         110         0.78         162         1.04           7         0.18         59         0.05         111         1.08         163         0.97           8         0.45         60         -0.16         112         1.12         164         0.97           9         0.17         61         0.25         113         0.86         165         0.59           10         0.42         62         0.29         114         0.65         166         1.51           11         -0.23         63         0.13         115         1.04         167         0.78           12         0.22         64         -0.14         116         0.97         188         0.78***           13         0.13         65         0.23         118         0.61         170 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.23</td> <td></td> <td></td>						0.23		
4         0.46         56         0.14         108         1.21         160         0.95           5         0.50         57         -0.23         109         1.13         161         0.85           6         0.28         58         -0.24         110         0.78         162         1.04           7         0.18         59         0.05         111         1.08         163         0.97           8         0.45         60         -0.16         112         1.12         164         0.97           9         0.17         61         0.25         113         0.86         165         0.59           10         0.42         62         0.29         114         0.65         166         1.15           11         -0.23         63         0.13         115         1.04         167         0.78*           12         0.22         64         -0.14         116         0.97         168         0.78**           13         0.13         66         0.23         118         0.61         170         1.04           15         -0.11         67         -0.06         119         0.77         17								
5         0.50         57         -0.23         109         1.13         161         0.85           6         0.28         58         -0.24         110         0.78         162         1.04           7         0.18         59         0.05         111         1.08         163         0.97           8         0.45         60         -0.16         112         1.12         164         0.97           9         0.17         61         0.25         113         0.86         165         0.59           10         0.42         62         0.29         114         0.65         166         1.15           11         -0.23         63         0.13         115         1.04         167         0.78           12         0.22         64         -0.14         116         0.95         169         1.29           13         0.13         65         0.27         117         0.95         169         1.29           14         0.13         66         0.23         118         0.61         170         1.04           15         -0.11         67         -0.06         119         0.77         171<								
6         0.28         58         -0.24         110         0.78         162         1.04           7         0.18         59         0.05         111         1.08         163         0.97           8         0.45         60         -0.16         112         1.12         1164         0.97           9         0.17         61         0.25         113         0.86         165         0.59           10         0.42         62         0.29         114         0.65         166         1.15           11         -0.23         63         0.13         115         1.04         167         0.78           12         0.22         64         -0.14         116         0.97         168         0.78***           13         0.13         66         0.23         118         0.61         170         1.04           15         -0.11         67         -0.06         119         0.77         171         1.21           16         0.14         68         0.35         120         1.17         172         0.97           17         -0.01         69         0.13         121         1.17 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>								
7         0.18         59         0.05         111         1.08         163         0.97           9         0.17         61         0.25         113         0.86         165         0.59           10         0.42         62         0.29         114         0.65         166         1.15           11         -0.23         63         0.13         115         1.04         167         0.78           12         0.22         64         -0.14         116         0.97         168         0.78***           13         0.13         65         0.27         117         0.95         169         1.29           14         0.13         66         0.23         118         0.61         170         1.04           15         -0.11         67         -0.06         119         0.77         171         1.21           16         0.14         68         0.35         120         1.17         172         0.97           17         -0.01         69         0.13         121         1.17         172         0.97           17         -0.01         69         0.13         121         1.17 <th< td=""><td>6</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>	6							
8 0.45 60 -0.16 112 1.12 1.64 0.97 9 0.17 61 0.25 113 0.86 165 0.59 10 0.42 62 0.29 114 0.65 166 1.15 11 -0.23 63 0.13 115 1.04 167 0.78 12 0.22 64 -0.14 116 0.97 168 0.78** 13 0.13 65 0.27 117 0.95 169 1.29 14 0.13 66 0.23 118 0.61 170 1.04 15 -0.11 67 -0.06 119 0.77 171 1.21 16 0.14 68 0.35 120 1.17 172 0.97 17 -0.01 69 0.13 121 1.17 173 1.14 18 -0.19 70 0.05 122 1.19 174 0.96 19 0.00 71 -0.11 123 1.12 175 0.96 20 -0.22 72 0.26 124 1.09 175 0.96 20 -0.22 72 0.26 124 1.09 175 0.96 21 0.00** 74 0.44 126 0.98 178 0.91 22 0.00** 74 0.44 126 0.98 178 0.91 23 -0.57 75 0.12 127 1.13 179 0.78 24 0.05 76 0.23 128 1.00** 180 1.17 25 -0.28 77 0.26 129 0.88 181 0.71 26 -0.45 78 0.57 130 0.66 182 0.70 27 -0.29 79 0.48 131 1.03 183 0.87 28 -0.40 80 0.46 132 0.68 184 0.51 29 -0.47 81 0.32 133 0.98 185 0.86 30 -0.69 82 0.31 134 0.67 186 1.40 31 -0.66 83 0.36 135 1.01 187 0.86 32 -1.26 84 0.26 136 0.82 188 0.73 33 -2.29 85 0.09 137 0.98 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 190 0.66** 35 -1.30 87 0.12 139 1.03 191 0.63 36 -0.79 88 0.30 140 0.74 192 0.82 41 -0.71 93 0.62 145 0.41 197 1.00 42 -1.08 94 0.40 146 0.72 198 0.70 44 -0.80 96 0.46 148 0.56 200 0.79 49 0.09 101 0.29 153 0.69 205 0.60 50 -0.02 102 0.46 154 0.56 206 0.70 51 -0.01 103 0.64 155 0.91	7							
9 0.17 61 0.25 113 0.86 165 0.59 10 0.42 62 0.29 114 0.65 166 1.15 11 -0.23 63 0.13 115 1.04 167 0.78 12 0.22 64 -0.14 116 0.97 168 0.78** 13 0.13 65 0.27 117 0.95 169 1.29 14 0.13 66 0.23 118 0.61 170 1.04 15 -0.11 67 -0.06 119 0.77 171 1.21 16 0.14 68 0.35 120 1.17 172 0.97 17 -0.01 69 0.13 121 1.17 173 1.14 18 -0.19 70 0.05 122 1.19 174 0.96 19 0.00 71 -0.11 123 1.12 1.5 0.96 20 -0.22 72 0.26 124 1.09 176 0.71 21 0.00 73 0.33 125 1.06 177 0.98 22 0.00** 74 0.44 126 0.98 178 0.91 23 -0.57 75 0.12 127 1.13 179 0.78 24 0.05 76 0.23 128 1.00** 180 1.17 25 -0.28 77 0.26 129 0.88 181 0.71 26 -0.45 78 0.57 130 0.66 182 0.70 27 -0.29 79 0.48 131 1.03 183 0.87 28 -0.40 80 0.46 132 0.68 184 0.51 29 -0.47 81 0.32 133 0.98 185 0.86 30 -0.69 82 0.31 134 0.67 186 0.73 33 -2.29 85 0.09 137 0.98 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.69 34 -1.90 86 0.28 138 0.82 189 0.66** 35 -1.30 87 0.12 129 141 0.96 193 0.81 38 -1.21 90 0.12 142 0.99 194 0.93 39 -1.73 91 0.80 144 0.45** 196 0.65* 41 -0.71 93 0.62 145 0.41 197 1.00 42 -0.98 92 0.18 144 0.45** 196 0.65* 41 -0.71 93 0.62 145 0.41 197 1.00 43 -1.26 95 0.26 147 0.53 199 0.60 44 -0.80 96 0.46 148 0.56 200 0.79 43 -1.26 95 0.26 147 0.53 199 0.60 44 -0.80 96 0.46 148 0.56 200 0.79 45 -0.00 101 0.29 153 0.69 205 0.60 46 0.23 98 0.29 150 0.36 202 0.68 47 -0.06 99 0.73 151 0.82 203 0.70 48 0.19 100 0.26 152 1.16 204 0.27 49 0.09 101 0.29 153 0.69 205 0.60		0.45		-0.16	112	1.12	164	0.97
11         -0.23         63         0.13         115         1.04         167         0.78***           12         0.22         64         -0.14         116         0.97         168         0.78***           13         0.13         65         0.27         117         0.95         169         1.29           14         0.13         66         0.23         118         0.61         170         1.04           15         -0.11         67         -0.06         119         0.77         171         1.21           16         0.14         68         0.35         120         1.17         172         0.97           17         -0.01         69         0.13         121         1.17         173         1.14           18         -0.19         70         0.05         122         1.19         174         0.96           19         0.00         71         -0.11         123         1.12         175         0.96           19         0.00         73         0.33         125         1.06         177         0.98           20         -0.22         72         0.26         124         1.09		0.17		0.25	113	0.86	165	0.59
12         0.22         64         -0.14         116         0.97         168         0.78**           13         0.13         65         0.27         117         0.95         169         1.29           14         0.13         66         0.23         118         0.61         170         1.04           15         -0.11         67         -0.06         119         0.77         171         1.21           16         0.14         68         0.35         120         1.17         173         1.14           18         -0.19         70         0.05         122         1.19         174         0.96           19         0.00         71         -0.11         123         1.12         175         0.96           20         -0.22         72         0.26         124         1.09         176         0.71           21         0.00         73         0.33         125         1.06         177         0.98           22         0.00***         74         0.44         126         0.98         178         0.91           23         -0.57         75         0.12         127         1.13	10	0.42	62	0.29	114	0.65	166	1.15
13         0.13         65         0.27         117         0.95         169         1.29           14         0.13         66         0.23         118         0.61         170         1.04           15         -0.11         67         -0.06         119         0.77         171         1.21           16         0.14         68         0.35         120         1.17         172         0.97           17         -0.01         69         0.13         121         1.17         173         1.14           18         -0.19         70         0.05         122         1.19         174         0.96           19         0.00         71         -0.11         123         1.12         175         0.96           20         -0.22         72         0.26         124         1.09         176         0.71           21         0.00         73         0.33         125         1.06         177         0.98           22         0.00***         74         0.44         126         0.98         178         0.91           23         -0.57         75         0.12         127         1.13	11	-0.23	63	0.13	115	1.04	167	0.78
14         0.13         66         0.23         118         0.61         170         1.04           15         -0.11         67         -0.06         119         0.77         171         1.21           16         0.14         68         0.35         120         1.17         172         0.97           17         -0.01         69         0.13         121         1.17         173         1.14           18         -0.19         70         0.05         122         1.19         174         0.96           19         0.00         71         -0.11         123         1.12         175         0.96           20         -0.22         72         0.26         124         1.09         176         0.71           21         0.00         73         0.33         125         1.06         177         0.98           22         0.00***         74         0.44         126         0.98         178         0.91           23         -0.57         75         0.12         127         1.13         179         0.78           24         0.05         76         0.23         128         1.00***	12	0.22	64	-0.14	116	0.97	168	0.78**
15         -0.11         67         -0.06         119         0.77         171         1.21           16         0.14         68         0.35         120         1.17         172         0.97           17         -0.01         69         0.13         121         1.17         173         1.14           18         -0.19         70         0.05         122         1.19         174         0.96           19         0.00         71         -0.11         123         1.12         175         0.96           20         -0.22         72         0.26         124         1.09         176         0.71           21         0.00         73         0.33         125         1.06         177         0.98           22         0.00**         74         0.44         126         0.98         178         0.91           23         -0.57         75         0.12         127         1.13         179         0.78           24         0.05         76         0.23         128         1.00***         180         1.17           25         -0.28         77         0.26         129         0.88	13	0.13	65	0.27	117	0.95	169	1.29
16         0.14         68         0.35         120         1.17         172         0.97           17         -0.01         69         0.13         121         1.17         173         1.14           18         -0.19         70         0.05         122         1.19         174         0.96           19         0.00         71         -0.11         123         1.12         175         0.96           20         -0.22         72         0.26         124         1.09         176         0.71           21         0.00         73         0.33         125         1.06         177         0.98           22         0.00**         74         0.44         126         0.98         178         0.91           23         -0.57         75         0.12         127         1.13         179         0.78           24         0.05         76         0.23         128         1.00**         180         1.17           25         -0.28         77         0.26         129         0.88         181         0.71           26         -0.45         78         0.57         130         0.66	14	0.13	66	0.23	118	0.61	170	1.04
17         -0.01         69         0.13         121         1.17         173         1.14           18         -0.19         70         0.05         122         1.19         174         0.96           19         0.00         71         -0.11         123         1.12         175         0.96           20         -0.22         72         0.26         124         1.09         176         0.71           21         0.00         73         0.33         125         1.06         177         0.98           22         0.00**         74         0.44         126         0.98         178         0.91           23         -0.57         75         0.12         127         1.13         179         0.78           24         0.05         76         0.23         128         1.00***         180         1.17           25         -0.28         77         0.26         129         0.88         181         0.71           26         -0.45         78         0.57         130         0.66         182         0.70           27         -0.29         79         0.48         131         1.03	15	-0.11	67	-0.06	119	0.77	171	1.21
18         -0.19         70         0.05         122         1.19         174         0.96           19         0.00         71         -0.11         123         1.12         175         0.96           20         -0.22         72         0.26         124         1.09         176         0.71           21         0.00         73         0.33         125         1.06         177         0.98           22         0.00***         74         0.44         126         0.98         178         0.91           23         -0.57         75         0.12         127         1.13         179         0.78           24         0.05         76         0.23         128         1.00***         180         1.17           25         -0.28         77         0.26         129         0.88         181         0.71           26         -0.45         78         0.57         130         0.66         182         0.70           27         -0.29         79         0.48         131         1.03         183         0.87           28         -0.47         81         0.32         133         0.98	16							
19         0.00         71         -0.11         123         1.12         175         0.96           20         -0.22         72         0.26         124         1.09         176         0.71           21         0.00         73         0.33         125         1.06         177         0.98           22         0.00***         74         0.44         126         0.98         178         0.91           23         -0.57         75         0.12         127         1.13         179         0.78           24         0.05         76         0.23         128         1.00***         180         1.17           25         -0.28         77         0.26         129         0.88         181         0.71           26         -0.45         78         0.57         130         0.66         182         0.70           27         -0.29         79         0.48         131         1.03         183         0.87           28         -0.40         80         0.46         132         0.68         184         0.51           29         -0.47         81         0.32         133         0.98								
20         -0.22         72         0.26         124         1.09         176         0.71           21         0.00         73         0.33         125         1.06         177         0.98           22         0.00**         74         0.44         126         0.98         178         0.91           23         -0.57         75         0.12         127         1.13         179         0.78           24         0.05         76         0.23         128         1.00**         180         1.17           25         -0.28         77         0.26         129         0.88         181         0.71           26         -0.45         78         0.57         130         0.66         182         0.70           27         -0.29         79         0.48         131         1.03         183         0.87           28         -0.40         80         0.46         132         0.68         184         0.51           29         -0.47         81         0.32         133         0.98         185         0.86           30         -0.69         82         0.31         134         0.67	18							
21         0.00         73         0.33         125         1.06         177         0.98           22         0.00***         74         0.44         126         0.98         178         0.91           23         -0.57         75         0.12         127         1.13         179         0.78           24         0.05         76         0.23         128         1.00***         180         1.17           25         -0.28         77         0.26         129         0.88         181         0.71           26         -0.45         78         0.57         130         0.66         182         0.70           27         -0.29         79         0.48         131         1.03         183         0.87           28         -0.40         80         0.46         132         0.68         184         0.51           29         -0.47         81         0.32         133         0.98         185         0.86           30         -0.69         82         0.31         134         0.67         186         1.40           31         -0.66         83         0.36         135         1.01	19							
22         0.00**         74         0.44         126         0.98         178         0.91           23         -0.57         75         0.12         127         1.13         179         0.78           24         0.05         76         0.23         128         1.00**         180         1.17           25         -0.28         77         0.26         129         0.88         181         0.71           26         -0.45         78         0.57         130         0.66         182         0.70           27         -0.29         79         0.48         131         1.03         183         0.87           28         -0.40         80         0.46         132         0.68         184         0.51           29         -0.47         81         0.32         133         0.98         185         0.86           30         -0.69         82         0.31         134         0.67         186         1.40           31         -0.66         83         0.36         135         1.01         187         0.86           32         -1.26         84         0.26         136         0.82								
23         -0.57         75         0.12         127         1.13         179         0.78           24         0.05         76         0.23         128         1.00**         180         1.17           25         -0.28         77         0.26         129         0.88         181         0.71           26         -0.45         78         0.57         130         0.66         182         0.70           27         -0.29         79         0.48         131         1.03         183         0.87           28         -0.40         80         0.46         132         0.68         184         0.51           29         -0.47         81         0.32         133         0.98         185         0.86           30         -0.69         82         0.31         134         0.67         186         1.40           31         -0.66         83         0.36         135         1.01         187         0.86           32         -1.26         84         0.26         136         0.82         188         0.73           33         -2.29         85         0.09         137         0.98								
24         0.05         76         0.23         128         1.00***         180         1.17           25         -0.28         77         0.26         129         0.88         181         0.71           26         -0.45         78         0.57         130         0.66         182         0.70           27         -0.29         79         0.48         131         1.03         183         0.87           28         -0.40         80         0.46         132         0.68         184         0.51           29         -0.47         81         0.32         133         0.98         185         0.86           30         -0.69         82         0.31         134         0.67         186         1.40           31         -0.66         83         0.36         135         1.01         187         0.86           32         -1.26         84         0.26         136         0.82         188         0.73           33         -2.29         85         0.09         137         0.98         189         0.69           34         -1.90         86         0.28         138         0.82								
25         -0.28         77         0.26         129         0.88         181         0.71           26         -0.45         78         0.57         130         0.66         182         0.70           27         -0.29         79         0.48         131         1.03         183         0.87           28         -0.40         80         0.46         132         0.68         184         0.51           29         -0.47         81         0.32         133         0.98         185         0.86           30         -0.69         82         0.31         134         0.67         186         1.40           31         -0.66         83         0.36         135         1.01         187         0.86           32         -1.26         84         0.26         136         0.82         188         0.73           33         -2.29         85         0.09         137         0.98         189         0.69           34         -1.90         86         0.28         138         0.82         190         0.66***           35         -1.30         87         0.12         139         1.03								
26         -0.45         78         0.57         130         0.66         182         0.70           27         -0.29         79         0.48         131         1.03         183         0.87           28         -0.40         80         0.46         132         0.68         184         0.51           29         -0.47         81         0.32         133         0.98         185         0.86           30         -0.69         82         0.31         134         0.67         186         1.40           31         -0.66         83         0.36         135         1.01         187         0.86           32         -1.26         84         0.26         136         0.82         188         0.73           33         -2.29         85         0.09         137         0.98         189         0.69           34         -1.90         86         0.28         138         0.82         190         0.66**           35         -1.30         87         0.12         139         1.03         191         0.63           36         -0.79         88         0.30         140         0.74								
27         -0.29         79         0.48         131         1.03         183         0.87           28         -0.40         80         0.46         132         0.68         184         0.51           29         -0.47         81         0.32         133         0.98         185         0.86           30         -0.69         82         0.31         134         0.67         186         1.40           31         -0.66         83         0.36         135         1.01         187         0.86           32         -1.26         84         0.26         136         0.82         188         0.73           33         -2.29         85         0.09         137         0.98         189         0.69           34         -1.90         86         0.28         138         0.82         190         0.66**           35         -1.30         87         0.12         139         1.03         191         0.63           36         -0.79         88         0.30         140         0.74         192         0.82           37         -1.15         89         0.29         141         0.96								
28         -0.40         80         0.46         132         0.68         184         0.51           29         -0.47         81         0.32         133         0.98         185         0.86           30         -0.69         82         0.31         134         0.67         186         1.40           31         -0.66         83         0.36         135         1.01         187         0.86           32         -1.26         84         0.26         136         0.82         188         0.73           33         -2.29         85         0.09         137         0.98         189         0.69           34         -1.90         86         0.28         138         0.82         190         0.66***           35         -1.30         87         0.12         139         1.03         191         0.63           36         -0.79         88         0.30         140         0.74         192         0.82           37         -1.15         89         0.29         141         0.96         193         0.81           38         -1.21         90         0.12         142         0.99								
29         -0.47         81         0.32         133         0.98         185         0.86           30         -0.69         82         0.31         134         0.67         186         1.40           31         -0.66         83         0.36         135         1.01         187         0.86           32         -1.26         84         0.26         136         0.82         188         0.73           33         -2.29         85         0.09         137         0.98         189         0.69           34         -1.90         86         0.28         138         0.82         190         0.66***           35         -1.30         87         0.12         139         1.03         191         0.63           36         -0.79         88         0.30         140         0.74         192         0.82           37         -1.15         89         0.29         141         0.96         193         0.81           38         -1.21         90         0.12         142         0.99         194         0.93           39         -1.73         91         0.80         143         0.55								
30         -0.69         82         0.31         134         0.67         186         1.40           31         -0.66         83         0.36         135         1.01         187         0.86           32         -1.26         84         0.26         136         0.82         188         0.73           33         -2.29         85         0.09         137         0.98         189         0.69           34         -1.90         86         0.28         138         0.82         190         0.66***           35         -1.30         87         0.12         139         1.03         191         0.63           36         -0.79         88         0.30         140         0.74         192         0.82           37         -1.15         89         0.29         141         0.96         193         0.81           38         -1.21         90         0.12         142         0.99         194         0.93           39         -1.73         91         0.80         143         0.55         195         1.10           40         -0.98         92         0.18         144         0.45***								
31         -0.66         83         0.36         135         1.01         187         0.86           32         -1.26         84         0.26         136         0.82         188         0.73           33         -2.29         85         0.09         137         0.98         189         0.69           34         -1.90         86         0.28         138         0.82         190         0.66***           35         -1.30         87         0.12         139         1.03         191         0.63           36         -0.79         88         0.30         140         0.74         192         0.82           37         -1.15         89         0.29         141         0.96         193         0.81           38         -1.21         90         0.12         142         0.99         194         0.93           39         -1.73         91         0.80         143         0.55         195         1.10           40         -0.98         92         0.18         144         0.45***         196         0.65           41         -0.71         93         0.62         145         0.41								
32         -1.26         84         0.26         136         0.82         188         0.73           33         -2.29         85         0.09         137         0.98         189         0.69           34         -1.90         86         0.28         138         0.82         190         0.66***           35         -1.30         87         0.12         139         1.03         191         0.63           36         -0.79         88         0.30         140         0.74         192         0.82           37         -1.15         89         0.29         141         0.96         193         0.81           38         -1.21         90         0.12         142         0.99         194         0.93           39         -1.73         91         0.80         143         0.55         195         1.10           40         -0.98         92         0.18         144         0.45***         196         0.65           41         -0.71         93         0.62         145         0.41         197         1.00           42         -1.08         94         0.40         146         0.72								
33         -2.29         85         0.09         137         0.98         189         0.69           34         -1.90         86         0.28         138         0.82         190         0.66***           35         -1.30         87         0.12         139         1.03         191         0.63           36         -0.79         88         0.30         140         0.74         192         0.82           37         -1.15         89         0.29         141         0.96         193         0.81           38         -1.21         90         0.12         142         0.99         194         0.93           39         -1.73         91         0.80         143         0.55         195         1.10           40         -0.98         92         0.18         144         0.45***         196         0.65           41         -0.71         93         0.62         145         0.41         197         1.00           42         -1.08         94         0.40         146         0.72         198         0.70           43         -1.26         95         0.26         147         0.53								
34         -1.90         86         0.28         138         0.82         190         0.66**           35         -1.30         87         0.12         139         1.03         191         0.63           36         -0.79         88         0.30         140         0.74         192         0.82           37         -1.15         89         0.29         141         0.96         193         0.81           38         -1.21         90         0.12         142         0.99         194         0.93           39         -1.73         91         0.80         143         0.55         195         1.10           40         -0.98         92         0.18         144         0.45***         196         0.65           41         -0.71         93         0.62         145         0.41         197         1.00           42         -1.08         94         0.40         146         0.72         198         0.70           43         -1.26         95         0.26         147         0.53         199         0.60           44         -0.80         96         0.46         148         0.56								
35         -1.30         87         0.12         139         1.03         191         0.63           36         -0.79         88         0.30         140         0.74         192         0.82           37         -1.15         89         0.29         141         0.96         193         0.81           38         -1.21         90         0.12         142         0.99         194         0.93           39         -1.73         91         0.80         143         0.55         195         1.10           40         -0.98         92         0.18         144         0.45**         196         0.65           41         -0.71         93         0.62         145         0.41         197         1.00           42         -1.08         94         0.40         146         0.72         198         0.70           43         -1.26         95         0.26         147         0.53         199         0.60           44         -0.80         96         0.46         148         0.56         200         0.79           45         0.65         97         0.14         149         0.56								
36         -0.79         88         0.30         140         0.74         192         0.82           37         -1.15         89         0.29         141         0.96         193         0.81           38         -1.21         90         0.12         142         0.99         194         0.93           39         -1.73         91         0.80         143         0.55         195         1.10           40         -0.98         92         0.18         144         0.45**         196         0.65           41         -0.71         93         0.62         145         0.41         197         1.00           42         -1.08         94         0.40         146         0.72         198         0.70           43         -1.26         95         0.26         147         0.53         199         0.60           44         -0.80         96         0.46         148         0.56         200         0.79           45         0.65         97         0.14         149         0.56         201         0.82           46         0.23         98         0.29         150         0.36								
37         -1.15         89         0.29         141         0.96         193         0.81           38         -1.21         90         0.12         142         0.99         194         0.93           39         -1.73         91         0.80         143         0.55         195         1.10           40         -0.98         92         0.18         144         0.45**         196         0.65           41         -0.71         93         0.62         145         0.41         197         1.00           42         -1.08         94         0.40         146         0.72         198         0.70           43         -1.26         95         0.26         147         0.53         199         0.60           44         -0.80         96         0.46         148         0.56         200         0.79           45         0.65         97         0.14         149         0.56         201         0.82           46         0.23         98         0.29         150         0.36         202         0.68           47         -0.06         99         0.73         151         0.82								
38         -1.21         90         0.12         142         0.99         194         0.93           39         -1.73         91         0.80         143         0.55         195         1.10           40         -0.98         92         0.18         144         0.45**         196         0.65           41         -0.71         93         0.62         145         0.41         197         1.00           42         -1.08         94         0.40         146         0.72         198         0.70           43         -1.26         95         0.26         147         0.53         199         0.60           44         -0.80         96         0.46         148         0.56         200         0.79           45         0.65         97         0.14         149         0.56         201         0.82           46         0.23         98         0.29         150         0.36         202         0.68           47         -0.06         99         0.73         151         0.82         203         0.70           48         0.19         100         0.26         152         1.16								
39         -1.73         91         0.80         143         0.55         195         1.10           40         -0.98         92         0.18         144         0.45**         196         0.65           41         -0.71         93         0.62         145         0.41         197         1.00           42         -1.08         94         0.40         146         0.72         198         0.70           43         -1.26         95         0.26         147         0.53         199         0.60           44         -0.80         96         0.46         148         0.56         200         0.79           45         0.65         97         0.14         149         0.56         201         0.82           46         0.23         98         0.29         150         0.36         202         0.68           47         -0.06         99         0.73         151         0.82         203         0.70           48         0.19         100         0.26         152         1.16         204         0.27           49         0.09         101         0.29         153         0.69								
40       -0.98       92       0.18       144       0.45**       196       0.65         41       -0.71       93       0.62       145       0.41       197       1.00         42       -1.08       94       0.40       146       0.72       198       0.70         43       -1.26       95       0.26       147       0.53       199       0.60         44       -0.80       96       0.46       148       0.56       200       0.79         45       0.65       97       0.14       149       0.56       201       0.82         46       0.23       98       0.29       150       0.36       202       0.68         47       -0.06       99       0.73       151       0.82       203       0.70         48       0.19       100       0.26       152       1.16       204       0.27         49       0.09       101       0.29       153       0.69       205       0.60         50       -0.02       102       0.46       154       0.56       206       0.70         51       -0.01       103       0.64       155       0.9								
41       -0.71       93       0.62       145       0.41       197       1.00         42       -1.08       94       0.40       146       0.72       198       0.70         43       -1.26       95       0.26       147       0.53       199       0.60         44       -0.80       96       0.46       148       0.56       200       0.79         45       0.65       97       0.14       149       0.56       201       0.82         46       0.23       98       0.29       150       0.36       202       0.68         47       -0.06       99       0.73       151       0.82       203       0.70         48       0.19       100       0.26       152       1.16       204       0.27         49       0.09       101       0.29       153       0.69       205       0.60         50       -0.02       102       0.46       154       0.56       206       0.70         51       -0.01       103       0.64       155       0.91       207       0.65								
42       -1.08       94       0.40       146       0.72       198       0.70         43       -1.26       95       0.26       147       0.53       199       0.60         44       -0.80       96       0.46       148       0.56       200       0.79         45       0.65       97       0.14       149       0.56       201       0.82         46       0.23       98       0.29       150       0.36       202       0.68         47       -0.06       99       0.73       151       0.82       203       0.70         48       0.19       100       0.26       152       1.16       204       0.27         49       0.09       101       0.29       153       0.69       205       0.60         50       -0.02       102       0.46       154       0.56       206       0.70         51       -0.01       103       0.64       155       0.91       207       0.65								
43       -1.26       95       0.26       147       0.53       199       0.60         44       -0.80       96       0.46       148       0.56       200       0.79         45       0.65       97       0.14       149       0.56       201       0.82         46       0.23       98       0.29       150       0.36       202       0.68         47       -0.06       99       0.73       151       0.82       203       0.70         48       0.19       100       0.26       152       1.16       204       0.27         49       0.09       101       0.29       153       0.69       205       0.60         50       -0.02       102       0.46       154       0.56       206       0.70         51       -0.01       103       0.64       155       0.91       207       0.65								
44       -0.80       96       0.46       148       0.56       200       0.79         45       0.65       97       0.14       149       0.56       201       0.82         46       0.23       98       0.29       150       0.36       202       0.68         47       -0.06       99       0.73       151       0.82       203       0.70         48       0.19       100       0.26       152       1.16       204       0.27         49       0.09       101       0.29       153       0.69       205       0.60         50       -0.02       102       0.46       154       0.56       206       0.70         51       -0.01       103       0.64       155       0.91       207       0.65								
45     0.65     97     0.14     149     0.56     201     0.82       46     0.23     98     0.29     150     0.36     202     0.68       47     -0.06     99     0.73     151     0.82     203     0.70       48     0.19     100     0.26     152     1.16     204     0.27       49     0.09     101     0.29     153     0.69     205     0.60       50     -0.02     102     0.46     154     0.56     206     0.70       51     -0.01     103     0.64     155     0.91     207     0.65								
46       0.23       98       0.29       150       0.36       202       0.68         47       -0.06       99       0.73       151       0.82       203       0.70         48       0.19       100       0.26       152       1.16       204       0.27         49       0.09       101       0.29       153       0.69       205       0.60         50       -0.02       102       0.46       154       0.56       206       0.70         51       -0.01       103       0.64       155       0.91       207       0.65								
47     -0.06     99     0.73     151     0.82     203     0.70       48     0.19     100     0.26     152     1.16     204     0.27       49     0.09     101     0.29     153     0.69     205     0.60       50     -0.02     102     0.46     154     0.56     206     0.70       51     -0.01     103     0.64     155     0.91     207     0.65								
48     0.19     100     0.26     152     1.16     204     0.27       49     0.09     101     0.29     153     0.69     205     0.60       50     -0.02     102     0.46     154     0.56     206     0.70       51     -0.01     103     0.64     155     0.91     207     0.65								
49     0.09     101     0.29     153     0.69     205     0.60       50     -0.02     102     0.46     154     0.56     206     0.70       51     -0.01     103     0.64     155     0.91     207     0.65								
50     -0.02     102     0.46     154     0.56     206     0.70       51     -0.01     103     0.64     155     0.91     207     0.65								
51 -0.01 103 0.64 155 0.91 207 0.65								

<u>Table 1.9:</u> CTD conductivity calibration coefficients.  $F_1$ ,  $F_2$  and  $F_3$  are respectively conductivity bias, slope and station-dependent correction calibration terms. n is the number of samples retained for calibration in each station grouping;  $\sigma$  is the standard deviation of the conductivity residual for the n samples in the station grouping (see CTD methodology);  $\alpha$  is the correction applied to CTD conductivities due to pressure dependence of the conductivity residuals for stations 30 to 41 (eqn 1.1).

	i stations oo to	+1 (cqii iii).				
stn grouping	$F_1$	$F_2$	$F_3$	n	σ	$\alpha$
001 to 003	15532800	0.10106622E-02	11470793E-08	43	0.001506	
004 to 006	12422183	0.10097721E-02	22838255E-07	66	0.001231	
007 to 011	11687464	0.10094945E-02	12108803E-07	108	0.001224	
012 to 013	10839249	0.10098253E-02	56286375E-07	43	0.001083	
014 to 017	10910666	0.10089800E-02	0.85821839E-08	85	0.001106	
018 to 024	10605356	0.10089344E-02	0.58253139E-08	152	0.001306	
025 to 026	11794039	0.10094659E-02	15959792E-08	43	0.001174	
027 to 029	11923390	0.10095053E-02	73952908E-09	65	0.000989	
030 to 032	84092238E-01	0.94275256E-03	0.65573267E-08	70	0.001063	1.207501E-06
033 to 037	83614084E-01	0.94281093E-03	0.34424272E-08	114	0.000946	1.239768E-06
038 to 041	84436830E-01	0.94285378E-03	0.28708290E-08	91	0.000948	1.321621E-06
042 to 044	-	-	-	-	-	-
045 to 047	50710766E-01	0.10080721E-02	17528905E-07		0.000900	
048 to 050	55259689E-01	0.10074674E-02	12693342E-09		0.001153	
051 to 052	51316066E-01	0.10065250E-02	0.14941010E-07		0.000960	
053 to 056	42571330E-01	0.10096393E-02	47862704E-07		0.000847	
057 to 061	46105712E-01	0.10066443E-02	0.76930518E-08	28	0.001093	
062 to 068	36372532E-01	0.10063733E-02	0.69886140E-08		0.001138	
069 to 071	56595171E-01	0.10105745E-02	42261552E-07		0.001753	
072 to 074	43002639E-01	0.10087385E-02	23044300E-07	15		
075 to 083	46658731E-01	0.10068495E-02	0.30955746E-08	48	0.001327	
084 to 086	42416890E-01	0.10070047E-02	50938148E-09		0.000828	
087 to 089	31545437E-01	0.10082777E-02	19533903E-07		0.001211	
090 to 092	28704235E-01	0.10077391E-02	13458843E-07	17		
093 to 094	49118959E-01	0.10094562E-02	23536990E-07	11	0.000925	
095 to 097	62152866E-01	0.10025474E-02	0.53099831E-07	14	0.001575	
098 to 101	14314088E-01	0.10047888E-02	0.12315666E-07	27		
102 to 103	34956256E-01	0.10099761E-02	31950269E-07	22	0.001035	
104 to 105	-	-	-		-	
106 to 107	23593039E-01	0.10371770E-02	28856875E-06	11	0.001335	
108 to 109	19791365E-01	0.10130541E-02	63060262E-07		0.001446	
110 to 112	49023601E-01	0.10131578E-02	53759663E-07		0.003549	
113 to 129	40135147E-01	0.10069183E-02	85806002E-09		0.001647	
130 to 132	85296545E-02	0.10054166E-02	0.27726516E-08		0.001904	
133 to 134	25781684E-01	0.10052848E-02	0.71546988E-08		0.001136	
135 to 137	42318480E-01	0.10019220E-02	0.34902679E-07		0.002036	
138 to 140	14699730E-01	0.10035095E-02	0.14410654E-07		0.001514	
141 to 144	19358440E-01	0.10084928E-02	19248580E-07		0.001984	
145 to 148	28011470E-01	0.10051157E-02	0.68803976E-08		0.002432	
149 to 151	0.25657995E-01	0.10022988E-02	0.11828427E-07		0.002039	
152 to 153	45270083E-01	0.98897546E-03	0.11541208E-06	11	0.001242	
154 to 162	31067531E-01	0.10055354E-02	0.36686988E-10		0.001819	
163 to 167	34521659E-01	0.10018974E-02	0.23188345E-07		0.002383	
168 to 171	38682948E-01	0.10051592E-02	0.46065747E-08	19	0.001338	
172 to 174	38558169E-01	0.10161118E-02	58916707E-07		0.002094	
175 to 177	38509621E-01	0.10074843E-02	87849944E-08		0.000734	
178 to 180	55547340E-01	0.10069200E-02	19492192E-08	18	0.001820	
181 to 183	33533182E-01	0.99319718E-03	0.69701424E-07	16	0.001522	
184 to 188	30982703E-01	0.10032052E-02	0.14044956E-07	26	0.001601	
189 to 191	15491941E-01	0.99199340E-03	0.69487626E-07	16	0.002096	
192 to 195	28909825E-01	0.10034465E-02	0.11624303E-07	24	0.002599	
196 to 197	0.21113085E-01	0.99194842E-03	0.61703687E-07		0.003203	
198 to 201	28802603E-01	0.10147873E-02	44840249E-07	21	0.002606	
202 to 204	73871355E-01	0.10032132E-02	0.20954622E-07	68	0.001897	
205 to 208	10645228	0.10152894E-02	31595576E-07	78	0.001305	

stn no.	(F <sub>2</sub> + F <sub>3</sub> . N)	stn no.	(F <sub>2</sub> + F <sub>3</sub> . N)	stn no.	(F <sub>2</sub> + F <sub>3</sub> . N)	stn no.	(F <sub>2</sub> + F <sub>3</sub> . N)
1	0.10106610E-02	53	0.10071026E-02	105	<u>-</u>	157	0.10055412E-02
2	0.10106599E-02	54	0.10070547E-02	106	0.10065887E-02	158	0.10055412E-02
3	0.10106587E-02	55	0.10070069E-02	107	0.10063001E-02	159	0.10055412E-02
4	0.10096808E-02	56	0.10069590E-02	108	0.10062436E-02	160	0.10055413E-02
5	0.10096579E-02	57	0.10070828E-02	109	0.10061805E-02	161	0.10055413E-02
6	0.10096351E-02	58	0.10070905E-02	110	0.10072443E-02	162	0.10055413E-02
7	0.10094098E-02	59	0.10070982E-02	111	0.10071905E-02	163	0.10056771E-02
8	0.10093977E-02	60	0.10071059E-02	112	0.10071368E-02	164	0.10057003E-02
9	0.10093856E-02	61	0.10071136E-02	113	0.10068213E-02	165	0.10057235E-02
10	0.10093735E-02	62	0.10068066E-02	114	0.10068205E-02	166	0.10057467E-02
11	0.10093613E-02	63	0.10068135E-02	115	0.10068196E-02	167	0.10057699E-02
12	0.10091499E-02	64	0.10068205E-02	116	0.10068188E-02	168	0.10059331E-02
13	0.10090936E-02	65	0.10068275E-02	117	0.10068179E-02	169	0.10059377E-02
14	0.10091001E-02	66	0.10068345E-02	118	0.10068170E-02	170	0.10059423E-02
15	0.10091087E-02	67	0.10068415E-02	119	0.10068162E-02	171	0.10059469E-02
16	0.10091173E-02	68	0.10068485E-02	120	0.10068153E-02	172	0.10059781E-02
17	0.10091259E-02	69	0.10076584E-02	121	0.10068145E-02	173	0.10059192E-02
18	0.10090393E-02	70	0.10076162E-02	122	0.10068136E-02	174	0.10058603E-02
19	0.10090451E-02	71	0.10075739E-02	123	0.10068127E-02	175	0.10059469E-02
20	0.10090510E-02	72	0.10070793E-02	124	0.10068119E-02	176	0.10059381E-02
21	0.10090568E-02	73	0.10070563E-02	125	0.10068110E-02	177	0.10059294E-02
22	0.10090626E-02	74 75	0.10070333E-02	126	0.10068102E-02 0.10068093E-02	178	0.10065731E-02
23 24	0.10090684E-02 0.10090743E-02	75 76	0.10070817E-02 0.10070848E-02	127 128	0.10068085E-02	179 180	0.10065711E-02 0.10065692E-02
2 <del>4</del> 25	0.10090743E-02 0.10094260E-02	76 77	0.10070848E-02 0.10070879E-02	129	0.10068076E-02	181	0.10058131E-02
26	0.10094244E-02	78	0.10070879E-02 0.10070910E-02	130	0.10068076E-02 0.10057770E-02	182	0.10058131E-02 0.10058828E-02
27	0.10094244E-02 0.10094854E-02	79	0.10070910E-02 0.10070941E-02	131	0.10057770E-02 0.10057798E-02	183	0.10058525E-02
28	0.10094846E-02	80	0.10070941E-02 0.10070972E-02	132	0.10057750E-02 0.10057826E-02	184	0.10059325E-02 0.10057895E-02
29	0.10094839E-02	81	0.10070372E 02 0.10071003E-02	133	0.10067626E 02	185	0.10057036E-02
30	0.94294928E-03	82	0.10071034E-02	134	0.10062436E-02	186	0.10058176E-02
31	0.94295584E-03	83	0.10071065E-02	135	0.10066339E-02	187	0.10058317E-02
32	0.94296239E-03	84	0.10069620E-02	136	0.10066688E-02	188	0.10058457E-02
33	0.94292453E-03	85	0.10069614E-02	137	0.10067037E-02	189	0.10051266E-02
34	0.94292798E-03	86	0.10069609E-02	138	0.10054981E-02	190	0.10051960E-02
35	0.94293142E-03	87	0.10065783E-02	139	0.10055126E-02	191	0.10052655E-02
36	0.94293486E-03	88	0.10065588E-02	140	0.10055270E-02	192	0.10056784E-02
37	0.94293830E-03	89	0.10065392E-02	141	0.10057787E-02	193	0.10056900E-02
38	0.94296287E-03	90	0.10065278E-02	142	0.10057595E-02	194	0.10057016E-02
39	0.94296574E-03	91	0.10065143E-02	143	0.10057402E-02	195	0.10057133E-02
40	0.94296861E-03	92	0.10065008E-02	144	0.10057210E-02	196	0.10040423E-02
41	0.94297148E-03	93	0.10072673E-02	145	0.10061134E-02	197	0.10041040E-02
42	-	94	0.10072437E-02	146	0.10061203E-02	198	0.10059090E-02
43	-	95	0.10075919E-02	147	0.10061271E-02	199	0.10058641E-02
44	- 0.40070000E-00	96	0.10076450E-02	148	0.10061340E-02	200	0.10058193E-02
45 46	0.10072833E-02 0.10072658E-02	97	0.10076981E-02	149	0.10040612E-02	201	0.10057744E-02
46 47	0.10072656E-02 0.10072483E-02	98	0.10059957E-02 0.10060080E-02	150	0.10040730E-02 0.10040849E-02	202	0.10074460E-02
47 48	0.10072463E-02 0.10074613E-02	99 100	0.10060080E-02 0.10060203E-02	151 152	0.10040849E-02 0.10065181E-02	203 204	0.10074670E-02 0.10074879E-02
49	0.10074613E-02 0.10074612E-02	101	0.10060203E-02 0.10060327E-02	153	0.10065161E-02 0.10066335E-02	204	0.10074879E-02 0.10088123E-02
50	0.10074612E-02 0.10074611E-02	101	0.10060327E-02 0.10067172E-02	154	0.1005535E-02	206	0.10088723E-02 0.10087808E-02
51	0.10074011E-02 0.10072870E-02	103	0.1006/172E-02 0.10066853E-02	155	0.10055411E-02	207	0.10087492E-02
52	0.10072070E-02	104	-	156	0.10055411E-02	208	0.10087176E-02
-							

<u>Table 1.11:</u> CTD raw data scans, mostly in the vicinity of artificial density inversions, flagged for special treatment. Note that the pressure listed is approximate only; possible actions taken are either to ignore the raw data scans for all further calculations, or to apply a linear interpolation over the region of the bad data scans. Causes of bad data, listed in the last column, are detailed in the CTD methodology. For the raw scan number ranges, the lowest and highest scan numbers are not included in the ignore or interpolate actions.

station	approximate	raw scan	action	reason
number	pressure (dbar)	numbers	taken	
11	829	48358-48395	ignore	fouling of cond. cell
16	612	47637-47757	ignore	fouling of cond. cell
19	1850	75468-75585	ignore	fouling of cond. cell
23	206	16580-16738	ignore	wake effect
27	3030	126764-126858	ignore	fouling of cond. cell
49	234	21892-21901	ignore	fouling of cond. cell
68	458	19625-19640	ignore	fouling of cond. cell
81	20	43646-43867	ignore	fouling of cond. cell
100	12	33403-33449	ignore	fouling of cond. cell
204	186	13007-13104	ignore	wake effect
208	2468	100929-100979	ignore	fouling of cond. cell

<u>Table 1.12:</u> Missing data points in 2 dbar-averaged files. "1" indicates missing data for the indicated parameters: T=temperature; S=salinity,  $\sigma_T$ , specific volume anomaly and geopotential anomaly; O=dissolved oxygen; PAR=photosynthetically active radiation; F=fluorescence. Note that jmin is the minimum number of data points required in a 2 dbar bin to form the 2 dbar average (see CTD methodology).

						reason
where data missing	Τ	S	0	PAR	F	
1202	1	1		1		no. of data pts in 2 dbar bin < jmin
612	1	1		1		fouling of cond. cell
804	1	1		1		no. of data pts in 2 dbar bin < jmin
2-26	1	1		1		CTD data logging started at 27 dbar
2022, 2844	1	1		1		no. of data pts in 2 dbar bin < jmin
2-68			1			bad oxygen data
entire profile			1			no bottle data for calibration
310	1	1		1		no. of data pts in 2 dbar bin < jmin
3638	1	1		1		no. of data pts in 2 dbar bin < jmin
322	1	1		1		no. of data pts in 2 dbar bin < jmin
14-48			1			bad oxygen data
2-26			1			bad oxygen data
2324,2686,2974,4182	1	1		1		no. of data pts in 2 dbar bin < jmin
2-22,76			1			bad oxygen data
2-28			1			bad oxygen data
	1	1		1		no. of data pts in 2 dbar bin < jmin
12-28			1			bad oxygen data
244	1	1		1		no. of data pts in 2 dbar bin < jmin
18-34			1			bad oxygen data
10-28			1			bad oxygen data
entire profile		1	1			bad conductivity data
4466	1	1		1		no. of data pts in 2 dbar bin < jmin
entire profile	1	1	1			data not used
entire profile	1	1	1			data not used
672	1	1				no. of data pts in 2 dbar bin < jmin
entire profile			1			faulty oxygen sensor hardware
entire profile			1			faulty oxygen sensor hardware
entire profile			1			faulty oxygen sensor hardware
entire profile				1		PAR sensor not installed
entire profile					1	fluorometer not installed
	1202 612 804 2-26 2022, 2844 2-68 entire profile 310 3638 322 14-48 2-26 2324,2686,2974,4182 2-22,76 2-28 130, 1934 12-28 244 18-34 10-28 entire profile 4466 entire profile	where data missing T 1202 1 612 1 804 1 2-26 1 2022, 2844 1 2-68 entire profile 310 1 3638 1 322 1 14-48 2-26 2324,2686,2974,4182 1 2-22,76 2-28 130, 1934 1 12-28 244 1 18-34 10-28 entire profile 4466 1	where data missing T S 1202	where data missing       T S O         1202       1 1         612       1 1         804       1 1         2-26       1 1         2022, 2844       1 1         2-68       1         entire profile       1         310       1 1         3638       1 1         322       1 1         14-48       1         2-26       1         2324,2686,2974,4182       1 1         2-28       1         130, 1934       1 1         12-28       1         244       1 1         18-34       1         10-28       1         entire profile       1 1         enti	where data missing       T S O PAR         1202       1 1 1 1         612       1 1 1 1         804       1 1 1 1         2-26       1 1 1 1         2022, 2844       1 1 1 1         2-68       1 entire profile         310       1 1 1 1         3638       1 1 1 1         322       1 1 1 1         14-48       1 2-26         2324,2686,2974,4182       1 1 1 1         2-28       1 1 1 1         130, 1934       1 1 1 1         12-28       1 1 1 1         244       1 1 1 1         18-34       1 1 1 1         10-28       1 entire profile         entire profile       1 1 1 1         entire profile       1 1 1 1 </td <td>where data missing       T S O PAR F         1202       1 1 1 1         612       1 1 1 1         804       1 1 1 1         2-26       1 1 1 1         2022, 2844       1 1 1 1         2-68       1 entire profile         310       1 1 1 1         3638       1 1 1 1         322       1 1 1 1         14-48       1 2-26         2324,2686,2974,4182       1 1 1 1         2-28       1 1 1 1         130, 1934       1 1 1 1         12-28       1 1 1 1         244       1 1 1 1         18-34       1 1 1 1         10-28       1 entire profile         entire profile       1 1 1         <td< td=""></td<></td>	where data missing       T S O PAR F         1202       1 1 1 1         612       1 1 1 1         804       1 1 1 1         2-26       1 1 1 1         2022, 2844       1 1 1 1         2-68       1 entire profile         310       1 1 1 1         3638       1 1 1 1         322       1 1 1 1         14-48       1 2-26         2324,2686,2974,4182       1 1 1 1         2-28       1 1 1 1         130, 1934       1 1 1 1         12-28       1 1 1 1         244       1 1 1 1         18-34       1 1 1 1         10-28       1 entire profile         entire profile       1 1 1         entire profile       1 1 1 <td< td=""></td<>

<u>Table 1.13:</u> 2 dbar averages interpolated from surrounding 2 dbar values, for the indicated paramaters: T=temperature; S=salinity,  $\sigma_T$ , specific volume anomaly and geopotential anomaly; O=dissolved oxygen; PAR=photosynthetically active radiation.

station	interpolated	parameters
number	2 dbar values	interpolated
19	1782, 1850	T, S, PAR
27	3032	T, S, PAR
30	560,608,1122	T, S, PAR
31	3076	T, S, PAR
32	300,440,882,902,2260,2454,3064	T, S, PAR
33	666,856,900	T, S, PAR
34	544	T, S, PAR
35	1466,2072,2960	T, S, PAR
36	1672, 4048	T, S, PAR
37	570,1774,2164	T, S, PAR
38	1428	T, S, PAR
39	948,1380,1526,1566	T, S, PAR
40	676,1926,3196	T, S, PAR
41	4036	T, S, PAR
81	18, 20	T, S
204	2042	T, S
205	1784	T, S

<u>Table 1.14a:</u> Suspect 2 dbar averages. Note: for suspect salinity values, the following are also suspect:  $\sigma_T$ , specific volume anomaly, and geopotential anomaly.

station	suspect 2 d	dbar values (dbar)	reason
number	bad	questionable	
Suspect salinity	values		
2	142	-	salinity spike due to wake effect
13	-	304	salinity spike in steep local gradient
14	-	328-330	salinity spike in steep local gradient
16	-	386-388	salinity spike in steep local gradient
19	-	266-268	salinity spike in steep local gradient

<u>Table 1.14b:</u> Suspect 2 dbar-averaged data from near the surface (applies to all parameters other than dissolved oxygen, except where noted).

stn	suspect	2dbar values(db	oar)	stn s	suspect	2dbar values(dl	bar)
no.	bad	questionable	comment	no.	bad	questionable	comment
1	2,4	-	-	48-49	2,4,6	-	-
2	2	-	-	50-52	2,4	-	-
3-7	2,4	-	-	72	-	2	temperature ok
8	2,4,6	-	-	84	-	2	temperature ok
9-12	2,4	-	-	85	-	6	temperature ok
13	2	-	-	100	6-12	-	temperature ok
14-15	5 2,4	-	-	115	-	2,4	temperature ok
16-19	9 2	-	-	116	-	2	temperature ok
20	2,4	-	-	123	-	2,4,8	temperature ok
21	2	-	-	153	-	18	temperature ok
23	2,4,6	-	-	172	-	10	temperature ok
24	2,4	-	-	200	-	2	temperature ok
25	2	-	-	201	-	2	temperature ok
26	2,4	-	-	202	2	4	-
27-28	3 2	-	-	203	2,4	6,8	-
29	2,4	-	-	204	2	4	-
45	2,4,6	-	-	205	2	-	-
46-47	7 2,4	-	-	206-20	7 2	4	-

Table 1.15: Suspect 2 dbar-averaged dissolved oxygen data.

stn suspect 2dbar values(dbar)
no. bad questionable

32 - 2, 14-28
34 - 2-22
38 - 3906-4044

<u>Table 1.16:</u> CTD dissolved oxygen calibration coefficients.  $K_1$ ,  $K_2$ ,  $K_3$ ,  $K_4$ ,  $K_5$  and  $K_6$  are respectively oxygen current slope, oxygen sensor time constant, oxygen current bias, temperature correction term, weighting factor, and pressure correction term. dox is equal to 2.8 $\sigma$  (for  $\sigma$  as defined by eqn A2.24 in the CTD methodology); n is the number of samples retained for calibration in each station or station grouping.

station number	K <sub>1</sub>	K <sub>2</sub>	K <sub>3</sub>	$K_4$	K <sub>5</sub>	$K_6$	dox	n
30	12.057	5.0000	-1.570	-0.16340	0.67515	0.16214E-03	0.15525	22
32	13.933	5.0000	-1.999	-0.19355	0.78517	0.93553E-04	0.24321	24
33	10.938	5.0000	-1.510	-0.14316	0.12891	0.33452E-04	0.21989	24
34	13.713	5.0000	-2.051	-0.14829	0.91995	0.11928E-03	0.34838	24
35	14.503	5.0000	-1.990	-0.24202	0.69512	0.74484E-04	0.24419	24
36	24.416	5.0000	-3.394	-0.42081	0.81637	0.75967E-04	0.28902	20
37	12.645	5.0000	-1.703	-0.20725	0.56959	0.58486E-04	0.25036	24
38	12.389	5.0000	-1.872	-0.11335	0.60504	0.11011E-03	0.19553	23
39	12.977	8.0000	-1.700	-0.23495	0.69338	0.64992E-04	0.13824	22
40	16.556	5.0000	-2.359	-0.26428	0.82111	0.92212E-04	0.16173	22
41	12.979	5.0000	-1.746	-0.21918	0.71336	0.97135E-04	0.18931	23

<u>Table 1.17:</u> Starting values for CTD dissolved oxygen calibration coefficients prior to iteration, and coefficients varied during iteration (see CTD methodology). Note that coefficients not varied during iteration are held constant at the starting value.

station numbe	K₁ r	K <sub>2</sub>	K <sub>3</sub>	K <sub>4</sub>	<b>K</b> <sub>5</sub>	<b>K</b> <sub>6</sub>	coe vari	fficients ed
30	12.0500	5.0000	-1.300	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
32	11.5000	5.0000	-1.440	-0.500E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
33	11.6000	5.0000	-1.600	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
34	12.4000	5.0000	-1.450	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
35	12.7000	5.0000	-1.650	-0.400E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
36	10.8000	5.0000	-0.400	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
37	12.7500	5.0000	-1.650	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
38	12.6500	5.0000	-1.700	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
39	12.4300	8.0000	-1.650	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
40	14.1000	5.0000	-1.650	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
41	12.6000	5.0000	-1.650	-0.500E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$

<u>Table 1.18:</u> Dissolved oxygen Niskin bottle samples flagged as -9 for dissolved oxygen calibration. Note that this does not necessarily indicate a bad bottle sample - in many cases, flagging is due to bad CTD dissolved oxygen data.

station	rosette
number	position
30	24,23
36	23,19,18,17
38	24
39	20
40	23,20
41	21

Table 1.19: Questionable nutrient sample values (not deleted from hydrology data file).

PHOSPHATE		NITR	RATE	SILIC	SILICATE		
station number	rosette position	station number	rosette position	station number	rosette position		
5 8	13 1,2	5	13				
9 27	1,5,7 11,13	9	1,5,7				
29	2,17	29 44	2,17 13	29	2		
45 46	whole stn whole stn						

<u>Table 1.20:</u> Stations containing fluorescence (fl) and photosynthetically active radiation (par) 2 dbar-averaged data.

stations with fl data	stations with par data
1 to 4	1 to 50

 $\underline{\textbf{Table 1.21:}} \quad \textbf{Protected and unprotected reversing thermometers used (serial numbers are listed).}$ 

protected thern	nometers		
station	rosette position 24	rosette position 12	rosette position 2
numbers	thermometers	thermometers	thermometers
1 to 52	12095,12096	12094	12119,12120
53 to 100	-	-	12119,12120
101-105	-	12095,12096	12119,12120
100 to 128	-	-	12119,12120
129 to 201	-	-	12119,12094
202 to 208	12095,12096	12094	12119,12120
unprotected the	ormomotore		
	ennometers		
station	emometers	rosette position 12	rosette position 2
<b>'</b> .	ermometers	rosette position 12 thermometers	rosette position 2 thermometers
station	ermometers	•	•
station numbers	ermometers	thermometers	thermometers
station numbers 1 to 52	emometers	thermometers	thermometers 11993
station numbers 1 to 52 53 to 100	emometers	thermometers	thermometers 11993 11993
station numbers 1 to 52 53 to 100 101-105	emometers	thermometers	thermometers 11993 11993 11993
station numbers 1 to 52 53 to 100 101-105 100 to 128	emometers	thermometers	thermometers 11993 11993 11993 11993

<u>Table 1.22:</u> Calibration coefficients and calibration dates for CTD serial numbers 1103 and 1193 (unit nos 7 and 5 respectively) used during RSV Aurora Australis cruise AU9501. Note that an additional pressure bias term due to the station dependent surface pressure offset exists for each station (eqn A2.1 in the CTD methodology). Also note that platinum temperature calibrations are for the ITS-90 scale.

CTD serial 11 coefficient	03 (unit no. 7) value of coefficient	CTD ser coefficie	ial 1193 (unit no. 5) nt value of coefficient
pressure calibration concentration callocallocallocallocallocallocallocall		pressure calibratic CSIRO Calibratic pcal0 pcal1 pcal2 pcal3 pcal4	ion coefficients on Facility - 09/11/1995 -8.810839 1.007713e-01 1.985674e-09 -1.521121e-14 0.0
platinum temperature CSIRO Calibration Fa Tcal0 Tcal1 Tcal2	calibration coefficients cility - 26/09/1995 0.23396e-01 0.49983e-03 0.35049e-11		ature calibration coefficients on Facility - 26/09/1995 -0.20560e-01 0.49936e-03 0.27541e-11
CSIRO Calibration Fa	calibration coefficients cility - 08/11/1995 1.695615e+02 -3.240390e-03 0.0		ature calibration coefficients on Facility - 09/11/1995 1.167581e+02 -2.450758e-03 0.0 0.0
coefficients for temper pressure CSIRO Calibration Fa T <sub>0</sub> S <sub>1</sub> S <sub>2</sub>		pressure	emperature correction to on Facility - 09/11/1995 20.00 -1.474830e-05 -7.847037e-02
	I coefficients applied to five radiation (par) (supplied 1.1.115084e+01 3.402400e-04 0.0 -4.499860 1.373290e-04		ntarctic Division, January 1996) and r) raw digitiser counts

par2

-3.452156e-23

#### Part 2

# Aurora Australis Marine Science Cruise AU9604 - Oceanographic Field Measurements and Analysis

#### **ABSTRACT**

Oceanographic measurements were conducted along a series of meridional and zonal sections along the Antarctic continental shelf and slope region between 80 and 150°E, from January to March 1996. A total of 147 CTD vertical profile stations were taken, most to near bottom. Over 2450 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients, chlorofluorocarbons, oxygen 18, primary productivity, and biological parameters, using a 24 bottle rosette sampler. Near surface current data were collected using a ship mounted ADCP. Measurement and data processing techniques are summarised, and a summary of the data is presented in graphical and tabular form.

#### 2.1 INTRODUCTION

Marine science cruise AU9604, the fifth oceanographic cruise of the Cooperative Research Centre for the Antarctic and Southern Ocean Environment (Antarctic CRC), was conducted aboard the Australian Antarctic Division vessel RSV Aurora Australia from January to March 1996. The major constituent of the cruise was a joint oceanographic and biological survey along the continental shelf and slope region of Antarctica between 80 and 150°E (Figure 2.1). The primary objectives of the oceanographic survey, named MARGINEX (Antarctic Margin Experiment), were:

- 1. to estimate the rate of formation of surface and Antarctic Bottom Water masses;
- 2. to define the evolution and modification of Antarctic water masses along the shelf and slope in the experimental region;
- 3. to estimate the relative importance of air-sea interaction and advection of surface and deep waters on property changes in the major water masses.

The biology program comprised of a hydroacoustic survey of krill population in the region, to enable setting of catch limits (principal investigator Steve Nicol, Australian Antarctic Division). The linked oceanography-biology objective was to determine the relationship between the distribution and production of marine biota and the physical and biogeochemical conditions along the Antarctic shelf break.

Two bottom-mounted pressure recorders (principal investigators Tom Whitworth, University of Texas A&M, and Dale Pillsbury, Oregon State University) were successfully recovered from the northern and southern ends of the WOCE SR3 meridional section. A current meter mooring (principal investigator Ted Foster, University of Delaware) was also recovered from the eastern end of the MARGINEX study region. Two upward looking sonar moorings (principal investigator Ian Allison, Australian Antarctic Division) were deployed in the vicinity of Davis (Figure 2.1). Eight drifting buoys were also deployed throughout the voyage.

This report describes the collection of oceanographic data from MARGINEX, and summarises the chemical analysis and data processing methods employed. All information required for use of the data set is presented in tabular and graphical form.

# 2.2 CRUISE ITINERARY

In early January 1996, prior to the cruise proper, marine trials were conducted from the Aurora Australis at Port Arthur, and south of Maatsuyker Island. A shallow CTD cast was taken at Port Arthur for calibration of the hydroacoustic equipment, and a deep cast was taken south of Tasmania for testing of CTD instrumentation. At the northern end of the SR3 section, an unsuccessful attempt was made to recover the pressure recorder mooring designated Hobart91b (Table 2.4). The pressure recorder mooring designated Hobart94 was successfully recovered from the same approximate location, and the mooring Hobart96 was deployed as a replacement.

The first CTD cast on the cruise proper was taken en route to Davis, to test CTD equipment and measure Niskin bottle CFC blank levels. Following cargo operations at Davis, the two upward looking sonar moorings were deployed, with a CTD cast taken at both mooring locations. CTD legs 1 and 4 were completed, with leg 4 finishing at station 42 near the edge of the Shackleton Ice Shelf. A speculative CTD cast was taken at station 43 to investigate possible ice crystal formation in water flowing over a sill (T. Pauly, pers. comm.). CTD legs 6 and 7 were then completed. After leg 7, a search was made of the old ULS mooring site SONEAR (Bush, 1994). Note that this was the third and final search for SONEAR. The mooring could not be located, so the ship proceeded to Casey for cargo operations.

At Casey, a shallow CTD cast (station 65) was taken for calibration of the hydroacoustic equipment in cold water. After Casey, the remaining CTD legs 9, 11, 13, 16 and 18 were completed. Leg 16 was interrupted briefly for pressure recorder mooring work: the mooring Dumont94 was successfully recovered, and the mooring Dumont96 was deployed as a replacement (Table 2.4).

Note that the southern end of all the meridional CTD sections were closed on the shelf or at the shelf break, with the exception of leg 18 - this leg had to be terminated early at a depth of ~2100 m on the continental slope, due to thickening sea ice conditions.

After completion of MARGINEX, grappling operations commenced to attempt recovery of 3 current meter moorings (Table 2.4). The mooring CM2 was recovered, and a CTD cast (station 145) was taken at the mooring location. Moorings CM1 and CM3 were not found. Two final shallow CTD casts were taken to attempt to sample shuga ice for biological analysis. The ship then proceeded to Macquarie Island for cargo operations, then returned to Hobart.

#### Table 2.1: Summary of cruise itinerary.

Expedition Designation
Cruise AU9604 (cruise acronym BROKE), encompassing MARGINEX

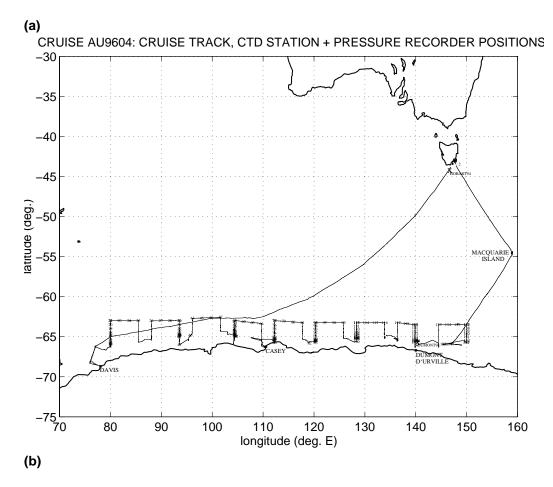
Chief Scientists
Nathan Bindoff, Antarctic CRC
Steve Nicol, Antarctic Division

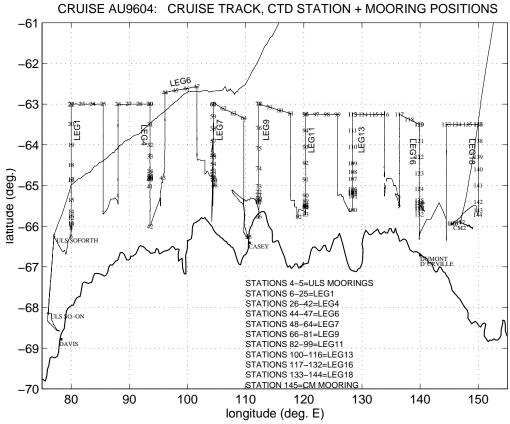
Ship RSV Aurora Australis

Ports of Call

Davis Casey Macquarie Island

Cruise Dates
January 19 to March 31 1996





<u>Figure 2.1a and b:</u> Cruise track, CTD station and mooring positions for RSV Aurora Australis cruise AU9604. Note that positions for pressure recorders are for recovered moorings only.

## 2.3 CRUISE SUMMARY

## 2.3.1 CTD casts and water samples

In the course of the cruise, 147 CTD casts were completed, 138 of which were along the MARGINEX study region (Figures 2.1a and b), with most casts reaching to within 20 m of the sea floor (Table 2.2). 8 meridional CTD sections and 9 shorter approximately zonal CTD sections were completed, providing closure for 7 different study areas (Figure 2.1b). Over 2450 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients (orthophosphate, nitrate plus nitrite, and reactive silicate), chlorofluorocarbons, oxygen 18, primary productivity, and biological parameters, using a 24 bottle rosette sampler. Table 2.3 provides a summary of samples drawn at each station. Principal investigators for the various water sampling programmes are listed in Table 2.6a. For all stations, the different samples were drawn in a fixed sequence (see previous data reports).

Table 2.2 (following 5 pages): Summary of station information for RSV Aurora Australis cruise AU9604. The information shown includes time, date, position and ocean depth for the start of the cast, at the bottom of the cast, and for the end of the cast. The maximum pressure reached for each cast, and the altimeter reading at the bottom of each cast (i.e. elevation above the sea bed) are also included. Missing ocean depth values are due to noise from the ship's bow thrusters interfering with the echo sounder. For casts which do not reach to within 100 m of the bed (i.e. the altimeter range), or for which the altimeter was not functioning, there is no altimeter value. For station names, LEGx is the MARGINEX CTD leg number (Figure 2.1b), TEST is a test cast, CAL is a cast for calibration of the hydroacoustic equipment, ULS is an upward looking sonar mooring site, CM is a current meter mooring site, and BIO is a speculative dip for biological analyses. Note that all times are UTC (i.e. GMT). CTD unit 7 (serial no. 1103) was used for stations 3 to 144; CTD unit 5 (serial no. 1193) was used for stations 1 to 2, and 145 to 147.

station	START	maxP	BOTTOM	END
number	time date latitude longitude depth(m)	(dbar)	time latitude longitude depth(m) altimeter	time latitude longitude depth(m)
	3 ,	()	3 , , , ,	3 ,
1 CAL	0604 5-JAN-96 43:08.34S 147:52.26E 27	26	0610 43:08.34S 147:52.26E - 8.1	0619 43:08.34S 147:52.26E -
2 TEST	1436 5-JAN-96 43:26.20S 148:35.20E 3635	3552	1605 43:27.10S 148:34.75E - 21.9	1711 43:28.00S 148:34.23E 3604
3 TEST	2112 20-JAN-96 49:54.55\$ 139:49.87E 3737	3924	2252 49:55.30S 139:50.70E - 32.9	0006 49:55.74S 139:51.17E -
4 ULS	2002 28-JAN-96 68:08.32S 76:02.67E 484	472	2014 68:08.38S 76:02.51E 479 12.6	2037 68:08.43S 76:01.96E 483
5 ULS	1059 29-JAN-96 66:15.50\$ 77:03.37E 2918	404	1118 66:15.51S 77:03.40E	1137 66:15.51S 77:03.41E -
6 LEG1	0331 30-JAN-96 66:14.12S 80:00.21E 396	382	0400 66:14.21S 79:59.71E - 9.5	0444 66:14.33\$ 79:58.92E 398
7 LEG1	0624 30-JAN-96 66:06.79S 79:59.50E 644	624	0653 66:06.89S 79:58.81E 638 9.7	0737 66:06.87S 79:57.87E 638
8 LEG1	1024 30-JAN-96 66:01.90S 79:59.94E 890	874	1058 66:01.98S 80:00.29E 870 2.5	1147 66:01.86S 80:00.16E 900
9 LEG1	1316 30-JAN-96 66:00.86S 79:59.92E 1208	1206	1407 66:00.60S 79:59.82E 1249 14.7	1516 66:00.25S 79:58.89E 1229
10 LEG1	1640 30-JAN-96 65:56.72S 79:59.60E 1668	1656	1731 65:56.69S 79:59.73E - 11.2	1838 65:56.72S 79:59.11E -
11 LEG1	2018 30-JAN-96 65:55.24S 80:00.29E 2099	2046	2115 65:55.26S 80:00.34E 2089 8.7	2232 65:55.33S 80:00.10E -
12 LEG1	0000 31-JAN-96 65:47.99S 80:00.09E 2457	2522	0108 65:47.99S 79:59.64E - 10.5	0229 65:48.29S 79:59.29E 2457
13 LEG1	0534 31-JAN-96 65:44.55\$ 79:59.65E 2866	2782	0701 65:44.74S 79:57.14E 2816 14.7	0841 65:45.34S 79:57.48E -
14 LEG1	1153 31-JAN-96 65:38.11S 79:58.89E 3174	3144	1319 65:38.52S 79:58.60E - 24.5	1436 65:39.05S 79:58.41E -
15 LEG1	1701 31-JAN-96 65:21.56S 79:59.92E 3384	3396	1829 65:21.81S 79:58.52E - 13.8	1958 65:21.99S 79:57.64E -
16 LEG1	0255 1-FEB-96 64:51.51S 80:00.14E 3634	168	0309 64:51.45S 79:59.86E	0329 64:51.36S 79:59.62E -
17 LEG1	0359 1-FEB-96 64:51.36S 79:59.68E 3634	3640	0526 64:51.10S 79:58.72E - 20.4	0703 64:50.88S 79:57.35E -
18 LEG1	1124 1-FEB-96 64:29.91S 79:59.89E 3634	3668	1303 64:29.12S 80:00.52E - 15.0	1422 64:28.86S 80:00.75E -
19 LEG1	1852 1-FEB-96 64:00.00S 79:59.82E 3686	3706	2020 63:59.68S 79:59.42E - 18.3	2157 63:59.22S 79:59.40E -
20 LEG1	0317 2-FEB-96 63:29.26S 79:59.21E 3737	3756	0447 63:29.22S 79:58.85E - 13.2	0637 63:29.35\$ 79:58.61E -
21 LEG1	1121 2-FEB-96 63:00.08S 80:00.01E 3583	166	1127 63:00.16S 80:00.18E	1146 63:00.09S 80:00.09E -
22 LEG1	1226 2-FEB-96 63:00.13S 79:59.83E 3583	3574	1347 63:00.37\$ 79:59.83E - 12.0	1508 63:00.79S 80:00.58E -
23 LEG1	2159 2-FEB-96 62:59.97S 81:50.12E 2866	2862	2304 62:59.76S 81:49.48E - 15.1	0023 62:59.42\$ 81:49.30E -
24 LEG1	0526 3-FEB-96 62:59.98\$ 83:39.99E 2508	2490	0628 62:59.78\$ 83:40.09E - 14.4	0754 62:59.65\$ 83:39.98E -
25 LEG1	1531 3-FEB-96 62:59.92\$ 85:30.09E 3757	3784	1705 62:59.52\$ 85:30.42E - 14.5	1901 62:58.98\$ 85:29.65E 3757
26 LEG4	2009 5-FEB-96 62:59.87\$ 88:03.66E 3788	3800	2137 63:00.64\$ 88:02.91E - 13.7	2306 63:01.20S 88:02.52E 3840
27 LEG4	0318 6-FEB-96 62:59.92S 89:54.00E 3931	4008	0457 63:00.26\$ 89:53.45E - 17.1	0647 63:00.63\$ 89:52.68E 4044
28 LEG4	1114 6-FEB-96 62:59.86S 91:43.78E 4095	3714	1247 63:00.04S 91:44.01E - 13.9	1425 62:59.82S 91:43.32E -
29 LEG4	1909 6-FEB-96 63:00.01S 93:34.02E 3327	170	1917 63:00.00\$ 93:33.83E	1933 62:59.98\$ 93:33.43E -
30 LEG4	2010 6-FEB-96 62:59.98S 93:33.81E 3327	3318	2134 63:00.34\$ 93:32.97E - 14.1	2305 63:00.23\$ 93:31.72E 3327
31 LEG4	0327 7-FEB-96 63:30.10S 93:33.70E 3194	3182	0436 63:30.16S 93:34.06E - 14.3	0604 63:30.25S 93:33.00E -
32 LEG4	1103 7-FEB-96 64:00.01S 93:33.79E 3297	3262	1218 64:00.07S 93:33.86E - 10.9	1350 64:00.30S 93:33.61E -
33 LEG4	1645 7-FEB-96 64:17.45S 93:33.59E 3051	3034	1804 64:17.82S 93:34.18E 3051 15.3	1941 64:17.98S 93:33.30E -
34 LEG4	0058 8-FEB-96 64:38.25S 93:33.84E 2651	2638	0159 64:38.16S 93:33.78E 2651 13.0	0317 64:37.96S 93:33.16E 2651
35 LEG4	0435 8-FEB-96 64:43.97S 93:33.81E 2260	2252	0537 64:43.93S 93:32.61E - 14.0	0655 64:44.03S 93:31.82E 2268
36 LEG4	0812 8-FEB-96 64:46.98S 93:33.22E 1791	1730	0905 64:47.22\$ 93:32.90E 1730 14.4	1006 64:47.54S 93:31.79E 1669

station	START	maxP	воттом	END
number	time date latitude longitude depth(m)	(dbar)	time latitude longitude depth(m) altimeter	time latitude longitude depth(m)
		( )	3 , , , , , , , , , , , , , , , , ,	5 3 4 4 4 7
37 LEG4	1137 8-FEB-96 64:48.06S 93:33.22E 1492	1440	1227 64:48.44S 93:31.62E 1413 17.9	1320 64:48.98S 93:30.22E -
38 LEG4	1427 8-FEB-96 64:48.75S 93:33.40E 1278	1210	1506 64:49.20S 93:32.41E 1229 11.5	1545 64:49.73S 93:31.74E -
39 LEG4	1651 8-FEB-96 64:50.05\$ 93:32.25E 925	888	1728 64:50.43S 93:30.77E 870 6.6	1815 64:50.91S 93:28.89E 772
40 LEG4	2027 8-FEB-96 64:51.05\$ 93:32.73E 593	522	2059 64:51.34S 93:32.08E 532 14.3	2136 64:51.59S 93:31.30E 512
41 LEG4	0109 9-FEB-96 65:01.62S 93:32.63E 467	450	0128 65:01.62S 93:32.32E 463 13.6	0156 65:01.71S 93:31.90E 463
42 LEG4	1210 9-FEB-96 66:00.04S 93:33.62E 1228	1198	1253 65:59.88S 93:32.80E 1228 13.6	1341 65:59.85S 93:32.06E 1228
43 CAL	0454 10-FEB-96 64:48.96S 95:44.40E 108	100	0458 64:48.97S 95:44.45E - 13.4	0509 64:48.93S 95:44.20E 112
44 LEG6	0026 11-FEB-96 62:42.58S 96:07.38E 3583	3622	0142 62:42.13S 96:07.42E 3614 14.4	0304 62:41.68S 96:07.15E 3635
45 LEG6	0823 11-FEB-96 62:39.84S 97:56.92E 3839	3886	0955 62:40.34S 97:55.12E - 17.2	1118 62:40.83S 97:53.93E -
46 LEG6	1623 11-FEB-96 62:37.06S 99:47.17E 4095	4124	1805 62:37.32S 99:47.70E 4095 13.2	2000 62:37.45S 99:48.79E 4095
47 LEG6	0021 12-FEB-96 62:34.16S 101:37.59E 4761	4244	0150 62:33.61S 101:37.62E 4761 16.2	0353 62:33.70S 101:36.99E 4761
48 LEG7	0841 13-FEB-96 65:00.15S 104:39.62E 356	344	0857 65:00.19S 104:39.90E - 11.4	0926 65:00.31S 104:39.71E 359
49 LEG7	1102 13-FEB-96 64:53.41S 104:37.66E 630	618	1125 64:53.38S 104:37.53E 635 15.8	1159 64:53.35S 104:37.23E 644
50 LEG7	1256 13-FEB-96 64:50.03S 104:29.44E 955	942	1328 64:49.91S 104:29.16E 955 14.2	1405 64:49.74S 104:28.92E 981
51 LEG7	1608 13-FEB-96 64:47.13S 104:27.18E 1251	1238	1658 64:46.89S 104:26.63E 1251 14.1	1759 64:46.62S 104:25.98E 1254
52 LEG7	1924 13-FEB-96 64:43.78S 104:24.01E 1561	1556	2017 64:43.66S 104:23.76E 1561 13.9	2112 64:43.59S 104:23.76E 1575
53 LEG7	2229 13-FEB-96 64:38.27S 104:25.09E 1817	1786	2315 64:38.24S 104:24.51E 1761 15.0	0015 64:38.16S 104:23.74E 1704
54 LEG7	0241 14-FEB-96 64:27.87S 104:26.01E 2129	2114	0334 64:27.83S 104:25.60E 2109 15.6	0452 64:28.00S 104:24.45E 2048
55 LEG7	0729 14-FEB-96 64:17.68S 104:25.51E 2570	2572	0835 64:17.62S 104:25.69E - 14.4	0953 64:17.68S 104:25.29E 2549
56 LEG7	1106 14-FEB-96 64:15.02S 104:25.76E 2774	2806	1217 64:14.53S 104:26.20E - 18.7	1349 64:13.68S 104:26.68E -
57 LEG7	1926 14-FEB-96 63:54.68S 104:26.00E 3337	3334	2053 63:54.49S 104:25.53E 3327 14.3	2221 63:54.25\$ 104:25.69E 3357
58 LEG7	0203 15-FEB-96 63:35.75S 104:25.77E 3634	3646	0331 63:35.74S 104:26.06E 3707 14.7	0514 63:35.37S 104:26.14E -
59 LEG7	0940 15-FEB-96 63:17.89S 104:26.05E 3942	3986	1111 63:18.20S 104:26.79E - 13.6	1247 63:18.09S 104:26.67E -
60 LEG7	1619 15-FEB-96 63:00.02S 104:25.99E 3901	166	1628 63:00.07\$ 104:26.01E	1643 63:00.13S 104:26.20E 3891
61 LEG7	1720 15-FEB-96 63:00.11S 104:26.67E 3901	3924	1846 63:00.29S 104:26.70E - 14.6	2028 63:00.52\$ 104:25.64E 3901
62 LEG7	0155 16-FEB-96 63:06.60S 106:11.15E 3727	3728	0318 63:06.58S 106:11.68E - 13.9	0503 63:06.78\$ 106:12.15E 3645
63 LEG7	0907 16-FEB-96 63:13.60S 107:56.52E 3327	3360	1031 63:13.90S 107:56.38E - 14.6	1208 63:14.19S 107:56.61E 3358
64 LEG7	1655 16-FEB-96 63:20.44S 109:41.33E 3716	3726	1822 63:20.52S 109:40.91E - 14.9	2004 63:20.45\$ 109:39.90E 3716
65 CAL	1604 19-FEB-96 66:15.92S 110:31.36E 56	46	1610 66:15.88S 110:31.40E 59 22.5	1616 66:15.85S 110:31.43E 59
66 LEG9	1211 23-FEB-96 65:45.43\$ 112:15.04E 438	420	1228 65:45.42S 112:15.13E - 14.6	1300 65:45.47\$ 112:15.06E 438
67 LEG9	1643 23-FEB-96 65:25.11S 112:15.84E 322	312	1659 65:25.03S 112:15.82E 328 11.0	1731 65:24.80S 112:15.32E 348
68 LEG9	1915 23-FEB-96 65:23.87\$ 112:12.45E 563	578	1940 65:23.74\$ 112:12.27E 584 33.8	2007 65:23.56\$ 112:11.93E 676
69 LEG9	2222 23-FEB-96 65:19.65\$ 112:13.81E 1014	1088	2301 65:19.52\$ 112:12.66E 1106 14.8	2347 65:19.24\$ 112:11.48E 1124
70 LEG9	0053 24-FEB-96 65:19.09S 112:14.88E 1222	1182	0144 65:18.94\$ 112:13.81E - 14.3	0234 65:18.85\$ 112:12.42E 1142
71 LEG9	0412 24-FEB-96 65:14.00\$ 112:15.24E 1587	1526	0501 65:14.20\$ 112:15.04E - 13.4	0607 65:14.51S 112:14.86E -
72 LEG9	0732 24-FEB-96 65:09.30S 112:15.00E 1843	1832	0830 65:09.45\$ 112:15.92E - 13.0	0942 65:10.55\$ 112:16.26E -

station		START	maxP	воттом	END
number	time date	latitude longitude depth(m		time latitude longitude depth(m) altimeter	time latitude longitude depth(m)
		0 1 (	, , ,	3 1 ( )	3 1 ( )
73 LEG9	1136 24-FEB-96	6 65:01.63S 112:14.83E 2211	2152	1237 65:01.42S 112:15.91E - 18.0	1351 65:01.66S 112:16.17E -
74 LEG9	1806 24-FEB-96	6 64:35.07S 112:14.99E 1873		1903 64:35.07S 112:15.45E 1893 16.0	2017 64:35.08S 112:15.76E 1873
75 LEG9	0217 25-FEB-96	6 64:04.98S 112:15.05E 2518	2542	0315 64:05.02S 112:15.63E - 16.1	0428 64:05.05S 112:15.74E 2560
76 LEG9	1017 25-FEB-96	6 63:34.98S 112:14.92E 3276	3260	1149 63:35.38S 112:15.51E - 13.0	1313 63:35.33S 112:15.87E -
77 LEG9	1944 25-FEB-96	6 62:59.97S 112:14.89E 3768	168	1953 62:59.97S 112:15.04E	2006 62:59.98S 112:15.28E 3788
78 LEG9	2034 25-FEB-96	6 62:59.97S 112:16.01E 3768	3810	2206 63:00.05S 112:17.94E - 13.1	2350 63:00.36S 112:19.50E -
79 LEG9	0548 26-FEB-96	6 63:04.54S 114:05.08E 3604	3618	0719 63:04.81S 114:05.57E - 17.0	0857 63:04.94S 114:04.63E -
80 LEG9	1314 26-FEB-96	6 63:09.20S 115:55.07E 3512	3494	1443 63:09.55S 115:56.54E - 14.7	1614 63:09.99S 115:57.56E -
81 LEG9	2113 26-FEB-96	6 63:13.79S 117:45.24E 3512	3526	2243 63:13.80S 117:47.05E - 13.2	0017 63:13.42S 117:48.53E -
82 LEG11	0532 28-FEB-96	6 65:46.56S 119:07.77E 614	598	0557 65:46.44S 119:08.35E - 13.8	0642 65:46.53S 119:08.00E 614
83 LEG11	1304 28-FEB-96	6 65:42.55S 120:18.84E 450	438	1331 65:42.75S 120:18.64E 450 15.0	1406 65:43.00S 120:18.12E 450
84 LEG11	1647 28-FEB-96	6 65:32.50S 120:18.37E 614	574	1713 65:32.56S 120:18.59E 584 19.6	1745 65:32.80S 120:18.41E 522
85 LEG11	1851 28-FEB-96	6 65:31.39S 120:18.81E 948	948	1934 65:31.53S 120:19.17E 953 13.2	2013 65:31.78S 120:19.08E 829
86 LEG11		6 65:30.72S 120:18.75E 1237		2149 65:30.76S 120:18.87E 1198 15.7	2237 65:30.80S 120:19.02E 1208
87 LEG11		6 65:29.44S 120:19.74E 1848		0030 65:29.55\$ 120:20.16E 1838 15.4	0122 65:29.74S 120:20.41E 1833
88 LEG11		6 65:28.34S 120:18.70E 2132		0337 65:28.19S 120:18.90E 2212 15.7	0454 65:28.00S 120:19.54E -
89 LEG11		6 65:23.01S 120:18.95E 2764	_	0816 65:22.89S 120:20.01E - 14.9	0936 65:22.91S 120:21.09E -
90 LEG11		6 65:14.99S 120:18.87E 3071		1225 65:15.00S 120:20.04E - 18.9	1349 65:15.12S 120:21.14E -
91 LEG11		6 64:50.88S 120:18.87E 3061		1913 64:51.31S 120:18.51E 3061 13.8	2034 64:51.91S 120:17.49E 3031
92 LEG11		6 64:26.97S 120:18.62E 3502		0154 64:27.34S 120:17.56E 3497 14.8	0545 64:28.02\$ 120:16.20E -
93 LEG11		6 64:03.13S 120:18.62E 3430		1135 64:03.67\$ 120:17.90E 3410 17.1	1303 64:04.15\$ 120:17.92E 3400
94 LEG11		6 63:38.91S 120:18.84E 3655		1818 63:39.70S 120:19.57E 3635 14.3	1947 63:39.81\$ 120:19.09E 3620
95 LEG11		6 63:14.78S 120:18.81E 3727		2336 63:14.68\$ 120:18.70E	2348 63:14.56S 120:18.59E -
96 LEG11		6 63:14.95S 120:18.93E 3737		0147 63:14.38\$ 120:19.15E - 12.2	0312 63:14.16S 120:18.67E -
97 LEG11		6 63:15.03S 122:08.91E 3839		0955 63:14.71S 122:10.09E - 14.4	1131 63:14.16S 122:09.54E -
98 LEG11		6 63:14.95S 123:58.77E 3983		1825 63:14.70S 123:59.51E - 14.2	2004 63:14.80S 123:59.78E -
99 LEG11		6 63:15.12S 125:48.76E 4116		0144 63:15.51S 125:50.90E 4111 15.6	0316 63:15.62S 125:52.38E -
100 LEG13		6 65:35.88S 128:22.35E 378	372	0757 65:35.91S 128:21.93E - 14.1	0830 65:36.12S 128:21.49E -
101 LEG13		65:15.98\$ 128:28.28E 358	352	1235 65:16.20S 128:28.26E 358 14.9	1305 65:16.54S 128:28.51E 374
102 LEG13		6 65:11.61S 128:22.11E 614	590	1632 65:11.75S 128:21.45E - 17.4	1709 65:11.69S 128:20.49E 563
103 LEG13		6 65:10.70\$ 128:22.30E 921	952	1923 65:10.69S 128:22.00E 921 16.9	2006 65:10.78S 128:21.38E 911
104 LEG13		6 65:09.93\$ 128:22.20E 1249		2217 65:09.97\$ 128:21.61E 1269 16.0	2259 65:10.09S 128:21.07E 1229
105 LEG13		6 65:08.88S 128:22.51E 1551		0039 65:09.33\$ 128:22.12E 1474 12.1	0133 65:09.57\$ 128:21.57E 1423
106 LEG13		6 65:05.07S 128:22.56E 1843		0327 65:05.18\$ 128:22.40E 1843 13.7	0430 65:05.37S 128:22.56E 1823
107 LEG13		6 64:50.01S 128:22.64E 1924		0827 64:50.10S 128:23.69E 1894 15.2	0929 64:50.10S 128:24.03E 1894
108 LEG13	1221 5-MAR-96	6 64:40.00S 128:22.53E 2539	2522	1322 64:40.12S 128:22.27E - 15.2	1448 64:40.80S 128:22.15E -

station		STA	RT	maxP	ВОТ	TOM			EN	ID
number	time date	latitude	longitude depth(m)	(dbar)	time latitude	longitude de	epth(m)	altimeter	time latitude	longitude depth(m)
				,						<u> </u>
109 LEG13	1725 5-MAR-96	64:27.249	S 128:22.50E 2682	2678	1824 64:27.55S	128:22.62E	2672	16.9	1930 64:28.06S	128:23.32E 2662
110 LEG13	2352 5-MAR-96	64:03.079	S 128:22.59E 3583	3606	0112 64:02.98S	128:23.05E	-	12.8	0244 64:02.65S	128:23.14E 3583
111 LEG13	0714 6-MAR-96	63:39.07	S 128:22.46E 3993	4010	0847 63:39.34S	128:24.88E	-	15.4	1040 63:40.08S	128:27.63E -
112 LEG13	1452 6-MAR-96	63:15.098	S 128:22.44E 4218	164	1459 63:15.18S	128:22.35E	4218	-	1512 63:15.21S	128:22.47E 4218
113 LEG13	1605 6-MAR-96	63:15.049	S 128:22.42E 4218	4266	1740 63:15.57S	128:22.62E	-	13.7	1907 63:16.00S	128:23.23E 4218
114 LEG13	0034 7-MAR-96	63:15.10	S 130:12.78E 4249	4302	0214 63:14.72S	130:15.07E	-	16.5	0402 63:14.46S	130:17.37E -
115 LEG13	0855 7-MAR-96	63:15.09	S 132:02.61E 4198	4250	1026 63:15.60S	132:04.60E	-	13.1	1203 63:16.42S	132:05.41E -
116 LEG13	1804 7-MAR-96	63:15.20	3 133:53.40E 4208	4260	1937 63:15.61S	133:53.63E	4208	9.6	2107 63:15.63S	133:53.38E 4208
117 LEG16	2231 11-MAR-96	6 63:14.91	S 136:26.24E 3993	4036	0010 63:15.17S	136:27.64E	-	15.4	0147 63:15.31S	136:29.35E -
118 LEG16	0739 12-MAR-96	6 63:22.42	S 138:08.53E 3880	3912	0909 63:22.33S	138:08.43E	-	14.7	1043 63:22.48S	138:07.48E -
119 LEG16	1733 12-MAR-96	6 63:29.97	S 139:50.98E 3788	164	1745 63:29.96S	139:50.82E	-	-	1800 63:29.91S	139:50.83E -
120 LEG16			S 139:50.64E 3788	3824	1952 63:29.55S		-	15.1		139:50.53E 3798
121 LEG16			S 139:51.13E 3727	3750	0516 63:53.62S		-	11.1	0656 63:52.78S	
122 LEG16			S 139:51.12E 3460	3456	1258 64:17.83S		-	13.1	1430 64:17.40S	
123 LEG16			S 139:50.91E 2918	2910	2026 64:42.20S		-	15.2		139:52.41E 2908
124 LEG16			S 139:50.92E 2764	2768	0451 65:05.13S		-	14.4	0624 65:05.23S	
125 LEG16			S 139:50.89E 2518	2486	1113 65:22.24S		-	14.1	1229 65:22.23S	
126 LEG16			S 139:50.95E 2150	2292	1612 65:25.09S		-	23.7		139:49.78E 2294
127 LEG16			S 139:50.79E 1843	2136	1918 65:25.87S		-	22.4	2025 65:26.20S	
128 LEG16			S 139:50.95E 1535	1480	0139 65:30.15S		-	17.4	0237 65:30.18S	
129 LEG16			S 139:51.57E 1177	1130	0426 65:32.86S		-	15.2	0515 65:32.91S	
130 LEG16	0800 16-MAR-96			910	0829 65:33.87S		932	15.1	0913 65:33.68S	
131 LEG16	1126 16-MAR-96			548	1151 65:35.11S		543	8.8	1230 65:35.49S	
132 LEG16			S 139:50.72E 296	288	1407 65:43.12S		307	16.0	1434 65:43.45S	
133 LEG18			S 144:29.99E 3906	3952	0642 63:30.17S		-	13.6	0825 63:30.88S	
134 LEG18			S 146:20.03E 3890	3926	1627 63:30.70S		-	15.2	1754 63:30.94S	
135 LEG18			S 148:09.97E 3839	3868	0015 63:29.88S		-	12.9	0144 63:29.90S	
136 LEG18			S 150:00.10E 3737	166	0645 63:30.13S		-	-	0705 63:30.20S	
137 LEG18			S 149:59.78E 3737	3762	0902 63:30.45S		-	15.9	1039 63:30.94\$	
138 LEG18			S 149:59.98E 3675	3698	1634 63:53.76S		-	12.2		150:00.05E 3675
139 LEG18	-		S 149:59.58E 3573	3600	2301 64:18.07S		-	14.9		150:01.03E 3573
140 LEG18			S 149:59.77E 3481	3490	0440 64:36.66S		-	15.4	0600 64:36.90S	
141 LEG18			S 149:59.86E 3317	3308	1345 65:00.25S		-	12.6	1516 65:00.49S	
142 LEG18			S 150:00.19E 2923	2916	2018 65:23.73\$		2918	13.8		150:00.21E 2918
143 LEG18			S 149:59.88E 2462	2448	0054 65:36.84\$			12.4		149:59.89E 2467
144 LEG18	U854 22-MAR-96	5 65:43.41	S 149:54.54E 2099	2096	0954 65:43.29S	149:54.22E	2099	10.3	1105 65:43.18S	149:54.04E -

station	START	maxP	BOTTOM	END
number	time date latitude longitude depth(m)	(dbar)	time latitude longitude depth(m) altimeter	time latitude longitude depth(m)
145 CM 146 BIO 147 BIO	0856 23-MAR-96 65:55.74\$ 145:23.86E 796 1140 23-MAR-96 65:56.28\$ 145:41.21E 573 0732 25-MAR-96 65:54.39\$ 146:56.74E 576	688 154 150	0938 65:56.01\$ 145:23.92E 676 13.1 1157 65:56.28\$ 145:41.38E 563 - 0748 65:54.45\$ 146:56.62E	1017 65:56.22S 145:23.51E 625 1220 65:56.19S 145:41.12E 573 0808 65:54.48S 146:56.63E 545

<u>Table 2.3:</u> Summary of samples drawn from Niskin bottles at each station, including salinity (sal), dissolved oxygen (do), nutrients (nut), chlorofluorocarbons (CFC), <sup>18</sup>O, primary productivity (pp), fast repitition rate fluorometry (frrf), and pigments (pig); Seacat cast information was not available. Note that 1=samples taken, 0=no samples taken, 2=surface sample only (i.e. from shallowest Niskin bottle).

station	sal	do	nut	CFC	<sup>18</sup> O	pp frrf	pig
1	1	0	0	0	0	0 0	0
2	0	0	0	0	0	0 0	0
3	1	1	1	1	1	0 0	0
4	1	0	0	0	0	0 0	0
5	1	0	0	0	0	0 0	0
6	1	1	1	1	1	0 1	1
7	1	1	1	1	1	0 1	1
8 9	1 1	1 1	1 1	0 1	1 1	1 1 0 1	1 1
9 10	1	1	1	1	1	0 1	1
11	1	1	1	1	1	0 1	1
12	1	1	1	1	1	1 1	1
13	1	1	1	1	1	0 1	1
14	1	1	1	1	1	0 1	1
15	1	1	1	1	1	0 1	1
16	0	0	0	0	0	1 1	1
17	1	1	1	1	1	0 0	0
18	1	1	1	1	1	0 1	1
19	1	1	1	1	1	0 1	1
20	1	1	1	1	1	0 1	1
21	0	0	0	0	0	1 1	1
22	1	1	1	1	1	0 0	0
23	1	1	1	1	1	0 0	0
24	1	1	1	1	1	0 0	0
25	1	1	1	1	1	0 0	0
26	1	1	1	1	1	0 0	0
27	1	1	1	1	1	0 0	0
28 29	1 0	1 0	1 0	1	1	0 0 1 1	0 1
30	1	1	1	0 1	0 1	0 0	0
31	1	1	1	1	1	0 1	1
32	1	1	1	1	1	0 1	1
33	1	1	1	1	1	0 1	1
34	1	1	1	1	1	0 1	1
35	1	1	1	1	1	1 1	1
36	1	1	1	1	1	0 1	1
37	1	1	1	1	1	0 1	1
38	1	1	1	1	1	0 1	1
39	1	1	1	1	1	0 1	1
40	1	1	1	1	1	0 1	1
41	1	1	1	1	1	0 1	1
42	1	1	1	1	1	1 1	1
43	1	0	0	0	0	0 0	0
44 45	1	1	1	1	1	0 0	0
45 46	1	1	1	1	1	0 0	0
46 47	1 1	1 1	1 1	1 1	1 1	0 0 0 0	0
4 <i>7</i> 48	1	1	1	1	1	1 1	0 1
40 49	1	1	1	1	1	0 1	1
50	1	1	1	1	1	0 1	1
50	•	'	•		•	0 1	

Table 2.3: (continued)

51         1         1         1         1         0         1         1           52         1         1         1         1         0         1         1           53         1         1         1         1         0         1         1           54         1         1         1         1         1         1         1         1         1           55         1         1         1         1         1         0         1         1         5           56         1         1         1         1         0         0         1 </th <th>station</th> <th>sal</th> <th>do</th> <th>nut</th> <th>CFC</th> <th><sup>18</sup>O</th> <th>pp frrf</th> <th>pig</th>	station	sal	do	nut	CFC	<sup>18</sup> O	pp frrf	pig
53         1								
54         1								
55         1         1         1         1         0         1         1           56         1         1         1         1         0         1         1           57         1         1         1         1         0         1         1           58         1         1         1         1         0         1         1           59         1         1         1         1         0         1         1           60         0         0         0         0         1         1         1           60         0         0         0         0         1         1         1           60         0         0         0         0         0         0         0           63         1         1         1         1         1         0         0         0           64         1 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>								
56         1								
57         1         1         1         1         0         1         1           58         1         1         1         1         0         1         1           59         1         1         1         1         0         1         1           60         0         0         0         0         1         1         1           60         0         0         0         0         1 <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>		-						
58         1         1         1         1         0         1         1           59         1         1         1         1         0         1         1           60         0         0         0         0         1         1         1           61         1         1         1         1         0 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
59         1         1         1         1         0         1								
60								
62		0	0	0				
63								
64								
65								
66								
67								
68         1         1         1         1         0         1								
69								
71         1								
72       1        1       1       1       1       1       1       1       1       1       1       1       1       1       1       1        1		1	1		1	1	0 1	
73         1         1         1         1         0         1         1           74         1         1         1         1         0         1         1           75         1         1         1         1         0         1         1           76         1         1         1         1         1         0         1         1           77         0         0         0         0         1 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
74       1       1       1       1       0       1       1         75       1       1       1       1       0       1       1         76       1       1       1       1       0       0       1       1         77       0       0       0       0       0       1       1       1         78       1       1       1       1       1       0       0       0         79       1       1       1       1       0       0       0       0         80       1       1       1       1       0       0       0       0         81       1       1       1       1       1       0       0       0         82       1       1       1       1       1       1       1       1       1         83       1       1       1       1       1       1       1       1       1         84       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1								
75         1         1         1         1         0         1         1           76         1         1         1         1         0         1         1           77         0         0         0         0         1         1         1           78         1         1         1         1         1         0         0         0           79         1         1         1         1         0         1         1         1         1         1 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
76       1       1       1       1       0       1       1         77       0       0       0       0       1       1       1         78       1       1       1       1       1       0       0       0         79       1       1       1       1       1       0       0       0         80       1       1       1       1       1       0       0       0         81       1       1       1       1       1       0       0       0         82       1       1       1       1       1       1       1       1         83       1       1       1       1       1       1       1       1         84       1								
77         0 0 0 0 0 0 1 1 1 1 1 78         1 1 1 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0								
78       1       1       1       1       0       0         79       1       1       1       1       0       0         80       1       1       1       1       0       0         81       1       1       1       1       1       0       0         82       1       1       1       1       1       1       1         83       1       1       1       1       1       1       1       1         84       1								
79       1       1       1       1       0       0       0         80       1       1       1       1       0       0       0         81       1       1       1       1       1       0       0       0         82       1       1       1       1       1       1       1       1       1         83       1								
81       1       1       1       1       1       0       0         82       1       1       1       1       1       1       1       1         83       1       1       1       1       1       1       1       1       1         84       1       1       1       1       1       0       1       1         85       1       1       1       1       1       0       1       1         86       1       1       1       1       1       0       1       1         87       1       1       1       1       1       1       1       1         88       1       1       1       1       1       1       1       1         89       1       1       1       1       1       1       1       1       1         90       1 <t< td=""><td></td><td>1</td><td>1</td><td>1</td><td>1</td><td>1</td><td></td><td></td></t<>		1	1	1	1	1		
82       1		1	1					
83       1       1       1       1       0       1       1         84       1       1       1       1       0       1       1         85       1       1       1       1       0       1       1         86       1       1       1       1       0       1       1         87       1       1       1       1       1       0       1       1         88       1       1       1       1       1       1       1       1         89       1       1       1       1       1       1       1       1       1         90       1 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
84       1       1       1       1       0       1       1         85       1       1       1       1       0       1       1         86       1       1       1       1       0       1       1         87       1       1       1       1       1       0       1       1         88       1       1       1       1       1       1       1       1       1         89       1								
85       1       1       1       1       1       0       1       1         86       1       1       1       1       0       1       1         87       1       1       1       1       1       0       1       1         88       1       1       1       1       1       1       1       1       1         89       1								
86       1       1       1       1       0       1       1         87       1       1       1       1       0       1       1         88       1       1       1       1       1       1       1       1         89       1       1       1       1       1       1       1       1       1         90       1								
87       1       1       1       1       0       1       1         88       1       1       1       1       1       1       1       1         89       1       1       1       1       1       1       1       1       1         90       1       1       1       1       1       1       1       1       1         91       1								
88       1								
90       1       1       1       1       0       1       1         91       1       1       1       1       0       1       1         92       1       1       1       1       0       1       1         93       1       1       1       1       0       1       1         94       1       1       1       1       0       1       1         95       0       0       0       0       0       1       1       1         96       1       1       1       1       1       0       0       0         97       1       1       1       1       0       0       0         98       1       1       1       1       0       0       0         99       1       1       1       1       1       1       1       1         100       1       1       1       1       1       1       1       1       1         1100       1       1       1       1       1       1       1       1       1       1         100<								
91       1       1       1       1       0       1       1         92       1       1       1       1       0       1       1         93       1       1       1       1       0       1       1         94       1       1       1       1       0       1       1         95       0       0       0       0       1       1       1         96       1       1       1       1       0       0       0         97       1       1       1       1       1       0       0       0         98       1       1       1       1       1       0       0       0         99       1       1       1       1       1       1       1       1       1         100       1       1       1       1       1       1       1       1       1       1         100       1       1       1       1       1       1       1       1       1         100       1       1       1       1       1       1       1       1								
92       1       1       1       1       0       1       1         93       1       1       1       1       0       1       1         94       1       1       1       1       0       1       1         95       0       0       0       0       1       1       1         96       1       1       1       1       0       0       0         97       1       1       1       1       0       0       0         98       1       1       1       1       1       0       0       0         99       1       1       1       1       1       1       1       1       1         100       1       1       1       1       1       1       1       1       1       1       1       1         100       1								
93       1       1       1       1       0       1       1         94       1       1       1       1       0       1       1         95       0       0       0       0       1       1       1         96       1       1       1       1       0       0       0         97       1       1       1       1       0       0       0         98       1       1       1       1       0       0       0         99       1       1       1       1       1       1       1       1         100       1       1       1       1       1       1       1       1         101       1       1       1       1       1       1       1       1       1         100       1       1       1       1       1       1       1       1       1       1         101       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1								
94       1       1       1       1       0       1       1         95       0       0       0       0       0       1       1       1         96       1       1       1       1       1       0       0       0         97       1       1       1       1       1       0       0       0         98       1       1       1       1       1       0       0       0         99       1       1       1       1       1       1       1       1       1         100       1       1       1       1       1       1       1       1       1         101       1<								
95       0       0       0       0       1       1       1         96       1       1       1       1       0       0       0         97       1       1       1       1       1       0       0       0         98       1       1       1       1       1       0       0       0         99       1       1       1       1       1       1       1       1       1         100       1       1       1       1       1       1       1       1       1         102       1       1       1       1       1       0       1       1         103       1       1       1       1       1       0       1       1								
96       1       1       1       1       0       0       0         97       1       1       1       1       0       0       0         98       1       1       1       1       0       0       0         99       1       1       1       1       1       1       1       1         100       1       1       1       1       1       1       1       1       1         101       1       1       1       1       1       0       1       1       1         102       1       1       1       1       1       0       1       1         103       1       1       1       1       0       1       1								
97       1       1       1       1       0       0       0         98       1       1       1       1       0       0       0         99       1       1       1       1       1       0       0       0         100       1       1       1       1       1       1       1       1         101       1       1       1       1       1       0       1       1         102       1       1       1       1       1       0       1       1         103       1       1       1       1       0       1       1								
98       1       1       1       1       0       0       0         99       1       1       1       1       1       0       0       0         100       1       1       1       1       1       1       1       1         101       1       1       1       1       1       1       1       1       1         102       1       1       1       1       1       0       1       1         103       1       1       1       1       0       1       1								
100       1	98	1			1	1	0 0	0
101       1       1       1       1       0       1       1         102       1       1       1       1       0       1       1         103       1       1       1       1       0       1       1								
102       1       1       1       1       0       1       1         103       1       1       1       1       0       1       1								
103	101							
	102 103							
	103	1	1	1	1	1	0 1	1

Table 2.3: (continued)

station	sal	do	nut	CFC	<sup>18</sup> O	pp frrf	pig
105	1	1	1	1	1	1 1	1
106	1	1	1	1	1	0 1	1
107	1	1	1	1	1	1 1	1
108	1	1	1	1	1	0 1	1
109	1	1	1	1	1	0 1	1
110	1	1	1	1	1	0 1	1
111	1	1	1	1	1	0 1	1
112	0	0	0	0	0	1 1	1
113	1	1	1	1	1	0 0	0
114	1	1	1	1	1	0 0	0
115	1	1	1	1	1	0 0	0
116	1	1	1	1	1	0 0	0
117	1	1	1	1	1	0 0	0
118	1	1	1	1	1	0 0	0
119	0 1	0 1	0 1	0 1	0	0 1	1
120					1	0 0	0
121 122	1 1	1 1	1 1	1 1	1 1	1 1 0 1	1 1
122	1	1	1	1	1	0 1 0 1	1
123	1	1	1	1	1	1 1	1
125	1	1	1	1	1	0 1	1
126	1	1	1	1	1	0 1	1
127	1	1	1	1	1	0 1	1
128	1	1	1	1	1	1 1	1
129	1	1	1	1	1	0 1	1
130	1	1	1	1	1	0 1	1
131	1	1	1	1	1	0 1	1
132	1	1	1	1	1	0 1	1
133	1	1	1	1	1	0 0	0
134	1	1	1	1	1	0 0	0
135	1	1	1	1	1	0 0	0
136	0	0	0	0	0	1 1	1
137	1	1	1	1	1	0 0	0
138	1	1	1	1	1	0 1	1
139	1	1	1	1	1	0 1	1
140	1	1	1	1	1	1 1	1
141	1	1	1	1	1	0 1	1
142	1	1	1	1	1	0 1	1
143	1	1	1	1	1	0 1	1
144	1	1	1	1	1	1 1	1
145	1	1	1	1	1	0 0	0
146	0	0	0	0	0	0 1	1
147	0	0	0	0	0	0 1	1

<u>Table 2.4:</u> Bottom pressure recorder, upward looking sonar, and current meter moorings deployed/recovered during cruise AU9604. Note that for current meter moorings, mooring locations and water depths are estimates only, and instrument elevations are elevations above the bottom.

deployment deployment number time (	ent/recovery	latitude	longitude	CTD station no.	bottom depth(m)
	06/01/96 16/03/96	44 <sup>o</sup> 07.019'S 65 <sup>o</sup> 33.71'S	146 <sup>0</sup> 12.744 139 <sup>0</sup> 51.26'E		998 1024
	06/01/96 15/03/96	44 <sup>0</sup> 07.18'S 65 <sup>0</sup> 33.67'S	146 <sup>0</sup> 13.134 139 <sup>0</sup> 51.147		1028 1024
unsuccessful recovery a Hobart91b 03:13,	ttempts 06/01/96	44 <sup>0</sup> 06.83'S	146 <sup>0</sup> 14.03'E	-	1024
UPWARD LOOKING SO site deployment name time (UTC)	<b>DNARS</b> latitud	e longitud	le instrumen depths (m)		bottom depth(m)
instruments deployed SO-ON 21:56, 28/01/	/96 68 <sup>0</sup> 08	.30'S 76 <sup>0</sup> 02.	.37'E 150 (ULS	S) 4	478
SOFORTH 13:15, 29/01	/96 66 <sup>0</sup> 15	.28'S 77 <sup>0</sup> 02.	.74'E 160 (ULS 210 (CM		2866
CURRENT METER MOD site recovery name time (UTC)	<b>ORINGS</b> latitude	3	current meter elevations (m)	CTD station no.	bottom depth(m)
instruments recovered CM2 08:02, 23/03/96	65 <sup>0</sup> 55.72'S	145 <sup>0</sup> 24.69'E	100 65 25 (not reco 15 2 - water le	145 vered) vel recorder (not	~740
unsuccessful recovery at CM1 24-25/03/96 CM3 24/03/96	65 <sup>0</sup> 54.11'S	146 <sup>0</sup> 55.79'E 148 <sup>0</sup> 57.93'E	<u>-</u> -	-	~600 ~515

## 2.3.2 Moorings deployed/recovered

Two bottom pressure recorders were recovered near the north and south ends of the WOCE SR3 section, and two pressure recorders were deployed as replacements. A further pressure recorder at the north end of SR3 could not be recovered. Two upward looking sonar moorings were deployed in the vicinity of Davis. One current meter mooring was recovered from the eastern end of the MARGINEX study region; two further current meter moorings in the vicinity could not be recovered. Table 2.4 summarizes all mooring locations and deployment/recovery times.

## 2.3.3 Drifters deployed

8 drifting Argos buoys, manufactured by Turo Technology, were deployed throughout the cruise in the MARGINEX study region (Table 2.5).

# 2.3.4 Principal investigators

The principal investigators for the CTD and water sample measurements are listed in Table 2.6a. Cruise participants are listed in Table 2.6b.

Table 2.5: Argos buoys deployed on cruise au9604.

Buoy id no.	deployment time (UTC)	latitude	longitude	bottom depth (m)	sea surf. temp. ( <sup>O</sup> C)	air temp. ( <sup>O</sup> C)	air pressure (hPa)
27237	12:25,12/02/96	63 <sup>0</sup> 38.78'S	101 <sup>o</sup> 37.35'E	1325	-0.51	-1.0	985.4
27239	18:48,27/02/96		117 <sup>0</sup> 44.95'E		-0.51	-5.8	992.4
27236	20:53,03/03/96		125 <sup>0</sup> 48.44'E		-0.49	-2.1	984.8
27235	14:41,08/03/96	64 <sup>0</sup> 38.55'S	135 <sup>0</sup> 52.52'E	1214	-0.32	-2.0	989.7
27240	05:03,11/03/96	64 <sup>0</sup> 59.87'S	136 <sup>0</sup> 26.32'E	1218	-0.13	-2.7	975.0
27238	09:15,18/03/96	65 <sup>0</sup> 54.01'S	144 <sup>0</sup> 29.60'E	1165	-1.62	-1.3	997.2
24669	10:34,24/03/96	66 <sup>0</sup> 02.50'S	148 <sup>0</sup> 59.31'E	645	-1.80	-3.2	980.6
24673	08:43,25/03/96	65 <sup>0</sup> 53.98'S	147 <sup>0</sup> 00.59'E	718	-1.76	-3.4	985.1

<u>Table 2.6a:</u> Principal investigators (\*=cruise participant) for rosette water sampling programmes.

name	affiliation
*Nathan Bindoff/Steve Rintoul	Antarctic CRC/CSIRO
*Mark Warner	University of Washington
Russell Frew	Otago University
John Parslow	CSIRO
*Peter Strutton(PhD student)	Flinders University
Harvey Marchant/*Simon Wright	Antarctic Division
	*Nathan Bindoff/Steve Rintoul *Mark Warner Russell Frew John Parslow *Peter Strutton(PhD student)

<u>Table 2.6b:</u> Scientific personnel (cruise participants).

name	measurement	affiliation				
Nathan Bindoff	CTD	Antarctic CRC				
Tim Gibson	CTD, weather balloons	Antarctic CRC				
Doug Gillespie	whale hydroacoustics, CTD	Oxford University				
John Hunter	CTD	CSIRO				
Ian Knott	CTD, electronics	Antarctic CRC				
Mark Rosenberg	CTD, moorings	Antarctic CRC				
Mike Williams	CTD	Antarctic CRC				
	<b>3.2</b>					
Stephen Bray	salinity, oxygen, nutrients	Antarctic CRC				
Mark Rayner	salinity, nutrients	CSIRO				
Phillip Towler	oxygen	University of Melbourne				
•	, 5					
Steve Covey	CFC	University of Washington				
Mark Warner	CFC	University of Washington				
Clive Crossley	biological sampling	Antarctic CRC				
Rick van den Enden	biological sampling	Antarctic Division				
Paul Scott	biological sampling	Antarctic Division				
Peter Strutton	biological sampling	Flinders University				
Raechel Waters	biological sampling	Antarctic Division				
Simon Wright biolo	gical sampling, deputy voyage lea	der Antarctic Division				
Toby Bolton	krill	Flinders University				
Jon Havenhand	krill	Flinders University				
Rob King	krill	Antarctic Division				
John Kitchener	krill	Antarctic Division				
Steve Nicol	krill, voyage leader	Antarctic Division				
Robin Thompson	krill	Antarctic Division				
Patti Virtue	krill	Antarctic Division				
. atti Tiitao		, interested Enviolent				
Ian Higginbottom	hydroacoustics	Antarctic Division				
Tim Pauly	hydroacoustics	Antarctic Division				
Karen Evans	whale observations	Antarctic Division				
Peter Gill	whale observations	Antarctic Division				
Jennifer Gillot	whale observations	Antarctic Division				
Deb Glasgow	whale observations	Antarctic Division				
Claire Green	whale observations	Antarctic Division				
Paul Hodda	whale observations	Antarctic Division				
Mick Mackey	whale observations	Antarctic Division				
Debbie Thiele	whale observations	Antarctic Division				
Eric Woehler	ornithology	Antarctic Division				
Stephanie Zador	ornithology	Antarctic Division				
Ctophanie Zader	5	, interested Envision				
Pamela Brodie	programmer	Antarctic Division				
Chris Boucher	electronics	Antarctic Division				
Roy Francis	doctor	Antarctic Division				
Gordon Keith	programmer	Antarctic Division				
Steve Oakley	returnee	Antarctic Division				
Tim Ryan	underway measurements	Antarctic Division				
Rob Walker	gear officer	Antarctic Division				

## 2.4 FIELD DATA COLLECTION METHODS

## 2.4.1 CTD and hydrology measurements

In this section, CTD and hydrology data collection and processing methods are discussed. Preliminary results of the CTD data calibration, along with data quality information, are presented in Section 2.6. CTD instrumentation, CTD and hydrology data collection techniques and water sampling methods are described in detail in previous data reports (Rosenberg et al. 1995a, 1995b, 1996).

Briefly, General Oceanics Mark IIIC (i.e. WOCE upgraded) CTD units were used, with a General Oceanics model 1015 pylon, and 10 litre General Oceanics Niskin bottles. A 24 bottle rosette package was used, with deep sea reversing thermometers (Gohla-Precision) mounted at rosette positions 2, 12 and 24. A Li-Cor photosynthetically active radiation (p.a.r.) sensor and Sea-Tech fluorometer were also attached to the package for some casts. Complete calibration information for the CTD pressure, platinum temperature and pressure temperature sensors are presented in Table 2.23, along with fluorometer and p.a.r. calibrations. Note that correct scaling of fluorescence data requires linkage with primary productivity data, while p.a.r. data requires recalculation using extinction coefficients for the signal strength (B. Griffiths, pers. comm.). The complete CTD conductivity and CTD dissolved oxygen calibrations, derived respectively from the in situ Niskin bottle salinity and dissolved oxygen samples, are presented in a later section.

The CTD and hydrology data processing and calibration techniques are described in detail in Appendix 2 of Rosenberg et al. (1995b) (referred to as "CTD methodology" for the remainder of the report), with the following updates to the methodology:

- (i) the 10 seconds of CTD data prior to each bottle firing are averaged to form the CTD upcast for use in calibration (5 seconds was used previously);
- (ii) in the conductivity calibration for stations 11 to 61 and stations 71 to 144, an additional term was applied to remove the pressure dependent conductivity residual.

The analytical techniques and data processing routines employed in the Hydrographic Laboratory onboard the ship are discussed in Appendix 2.1 of this report, and in Appendix 3 of Rosenberg et al. (1995b). Note the following changes to the methodology:

- (i) 150 ml sample bottles were used, and 1.0 ml of reagents 1, 2 and 3 were used; the corresponding calculated value for the total amount of oxygen added with the reagents = 0.017 ml;
- (ii) a mean volume of 147.00 ml for oxygen sample bottles was applied in the calculation of dissolved oxygen concentration;
- (iii) nutrient autoanalyser results were processed by the software package "FASPac" (Astoria-Pacific International):
- (iv) salinity substandards were measured every 12 samples typically.

# 2.4.2 Underway measurements

Underway data collection is as described in previous data reports; data files are described in Part 5. Note that a sound speed of 1498 ms<sup>-1</sup> is used for all depth calculations, and the ship's draught of 7.3 m has been accounted for in final depth values (i.e. depths are values from the surface).

#### 2.4.3 ADCP

The acoustic Doppler current profiler (ADCP) instrumentation is described in previous data reports. GPS data were collected by a Koden receiver for the entire cruise, receiving both GPS positions and velocities every 1 second. ADCP data processing is discussed in more detail in Dunn (a and b, unpublished reports). Logging parameters are summarised in Table 2.7, while data results for this cruise will be discussed in a future report.

## Table 2.7: ADCP logging parameters.

ping parameters bottom track ping parameters

no. of bins: 60 no. of bins: 128 bin length: 8 m bin length: 4 m pulse length: 8 m pulse length: 32 m

delay: 4 m

ping interval: minimum ping interval: same as profiling pings

reference layer averaging: bins 8 to 20 ensemble averaging duration: 3 min.

## 2.5 MAJOR PROBLEMS ENCOUNTERED

## 2.5.1 Logistics

On the final CTD leg 18 (Figure 2.1b), traversed north to south, the section was prematurely terminated in a depth of ~2100 m, well short of the shelf break. Heavy ice together with time and fuel limitations did not allow further ice-breaking which would have been necessary to reach the shelf break.

#### 2.5.2 CTD sensors

Following station 81, the CTD dissolved oxygen sensor was replaced. After the cruise, analysis of data collected with the replacement sensor indicated that the oxygen current response of the sensor was poor. Thus CTD dissolved oxygen data for the second half of the cruise was of low quality, and these data were not processed further.

For most of the cruise, conductivity calibrations were of a lower quality than for previous cruises. This was due to a combination of unstable salinometer performance and a significant pressure dependent response of both conductivity cells used on CTD 1103 (see section 6 for more details).

The fluorometer on the rosette package flooded during station 35, and was unusable for the remainder of the cruise.

#### 2.5.3 Moorings

Of the three current meter moorings at the eastern end of the MARGINEX study region, only one was recovered, and only partially so - a current meter and a water level recorder were lost while dragging for the recovered mooring. No precise positions or water depths were available for the moorings, and no ranging equipment was included in the moorings, making the recovery operation a difficult one.

The four year pressure recorder mooring Hobart91b (Table 2.4) failed to release from the bottom mooring weight, despite flawless communication with the acoustic release. This failure was identical with that for the two moorings Dumont92a and b, described in Rosenberg et al. 1995b.

#### 2.5.4 Other equipment

The ship's gyrocompass malfunctioned on several occasions throughout the cruise, at one stage leaving the ship with no gyro for several days. ADCP data from these times will be poor.

## 2.6 CTD RESULTS

This section details information relevant to the creation and quality of the final CTD and hydrology data set. For actual use of the data, the following is important:

```
CTD data - Tables 2.15 and 2.16, and Table 2.8; hydrology data - Tables 2.20 and 2.21.
```

Historical data comparisons are made in Part 4 of this report. Data file formats are described in Part 5.

#### 2.6.1 CTD measurements - data creation and quality

CTD data calibration and processing methods are described in detail in the CTD methodology (i.e. Appendix 2 of Rosenberg et al., 1995b, with the additions listed in section 2.4.1 of this report). Cases for cruise au9604 which vary from this methodology are detailed in this section. CTD data quality is also discussed. For conversion to WOCE data file formats, see Part 5 of this report.

The final calibration results for conductivity/salinity and dissolved oxygen, along with the performance check for temperature, are plotted in Figures 2.2 to 2.5. For temperature, salinity and dissolved oxygen, the respective residuals ( $T_{therm}$  -  $T_{cal}$ ), ( $s_{btl}$  -  $s_{cal}$ ) and ( $o_{btl}$  -  $o_{cal}$ ) are plotted. For conductivity, the ratio  $c_{btl}/c_{cal}$  is plotted.  $T_{therm}$  and  $T_{cal}$  are respectively the protected thermometer and calibrated upcast CTD burst temperature values;  $s_{btl}$ ,  $s_{cal}$ ,  $o_{btl}$ ,  $o_{cal}$ ,  $c_{btl}$  and  $c_{cal}$ , and the mean and standard deviation values in Figures 2.2 to 2.5, are as defined in the CTD methodology (with additional definitions described below for cases where a pressure dependent residual is removed from conductivity data).

# 2.6.1.1 Conductivity/salinity

The conductivity calibration for CTD 1103 (stations 3 to 144) revealed problems with the salinity measurements for both the CTD and salinometers. A larger than usual conductivity calibration scatter (Figures 2.3 and 2.4) resulting from poor salinometer performance was superimposed on a pressure dependent conductivity residual resulting from CTD conductivity cell contamination. The pressure dependent conductivity residual was found for both conductivity cells used with CTD 1103, and is assumed to result from a light fouling or contamination of both cells. An extra fit was applied to remove this residual, following the same method as described in Part 1 (section 1.6.1.1) of this report. Note that station grouping for the extra fit parameter  $\alpha$  (defined in eqn 1.1 in Part 1 of this report) was separate from and different to the initial conductivity calibration station grouping (Table 2.10). After application of the pressure dependent conductivity correction, the standard deviation of the salinity calibration scatter decreased from 0.0027 to 0.0024 (PSS78) (Figure 2.4). This standard deviation value remained high due to unstable performance of all 4 YeoKal salinometers used for salinity sample analysis on the cruise.

For the remaining stations using CTD 1193, CTD conductivity cell performance was good.

#### 2.6.1.2 Temperature

Platinum temperature sensor performance of the CTD's was stable throughout the entire cruise, with a small offset between thermometer and CTD temperature values (Figure 2.2). Note that a post cruise temperature calibration was required for CTD 1193, as the pre cruise calibration for this instrument did not appear to be applicable.

#### **2.6.1.3 Pressure**

For stations 8, 89 and 116, data logging commenced when the CTD was already in the water, so surface pressure offset values were estimated from surrounding stations. For station 68, conductivity cell freezing interfered with the automatic estimation of surface pressure offsets (see CTD methodology), while pressure spiking interfered with pressure offset values for stations 29 and 48; for these stations, surface pressure offset values were estimated from a manual inspection of the pressure data. Note that for all these stations, any resulting additional error in the CTD pressure data is judged to be small (no more than 0.2 dbar).

# 2.6.1.4 Dissolved oxygen

Usable CTD dissolved oxygen data were only obtained for half of the cruise (stations 6 to 80 and station 145). For these stations, the final standard deviation value of the dissolved oxygen residuals (Figure 2.5) are less than 1% of full scale values (where full scale is approximately equal to 250  $\mu$ mol/l for pressure > 750 dbar, and 350  $\mu$ mol/l for pressure < 750 dbar). In most cases, the best calibration was achieved using large values of the order 12.0 for the coefficient  $K_1$  (i.e. oxygen current slope), and large negative values of the order -2.0 for the coefficient  $K_3$  (i.e. oxygen current bias) (Table 2.17).

#### 2.6.1.5 Fluorescence and P.A.R. Data

Fluorescence and p.a.r. are effectively uncalibrated. These data should not be used quantitatively other than for linkage with primary productivity data.

**Table 2.8:** Summary of cautions to CTD data quality.

station no.	CTD parameter	caution			
2,3	salinity	test cast - all bottles fired at same depth; salinity accuracy reduced			
8	salinity	CTD conductivity cell behaviour for this station different to surrounding stations - stn 8 calibrated on its own (i.e. not grouped)			
8,89,116	pressure	surface pressure offset estimated from surrounding stations			
29,48,68	pressure	surface pressure offset estimated from manual inspection of data			
19,24,26	oxygen	oxygen calibration fit fairly poor			
146,147	salinity	conductivity calibration for stn 145 applied to these stations			
11-61,71-14	4 salinity	additional correction applied for pressure dependent conductivity residual			
81-144	oxygen	no CTD dissolved oxygen data due to faulty oxygen sensor			
all stns	fluorescence/p.a.r.	fluorescence and p.a.r. sensors (where active) are uncalibrated			

#### 2.6.1.6 Summary of CTD data creation

Information relevant to the creation of the calibrated CTD data is tabulated, as follows:

- \* Surface pressure offsets calculated for each station are listed in Table 2.9.
- \* CTD conductivity calibration coefficients, including the station groupings used for the conductivity calibration, are listed in Tables 2.10 and 2.11.
- \* CTD raw data scans flagged for special treatment are listed in Table 2.12.
- \* Missing 2 dbar data averages are listed in Table 2.13.
- \* 2 dbar bins which are linearly interpolated from surrounding bins are listed in Table 2.14.
- \* Suspect 2 dbar averages are listed in Tables 2.15 and 2.16.
- \* CTD dissolved oxygen calibration coefficients are listed in Table 2.17. The starting values used for the coefficients prior to iteration, and the coefficients varied during the iteration, are listed in Table 2.18.
- \* The different protected and unprotected thermometers used for the stations are listed in Table 2.22.
- \* Laboratory calibration coefficients for the CTD's are listed in Table 2.23.

# 2.6.1.7 Summary of CTD data quality

CTD data quality cautions for the various parameters are summarised in Table 2.8.

## 2.6.2 Hydrology data

Quality control information relevant to the hydrology data is tabulated, as follows:

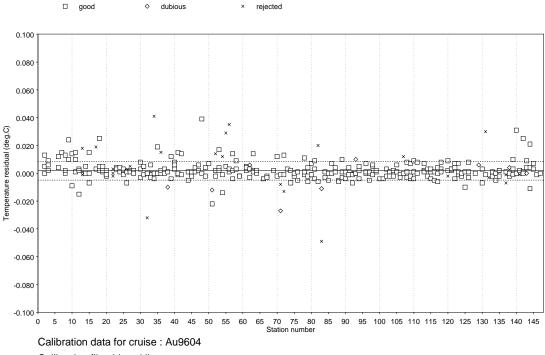
- \* Dissolved oxygen Niskin bottle samples flagged with the code -9 (rejected for CTD dissolved oxygen calibration) are listed in Table 2.19.
- \* Questionable dissolved oxygen and nutrient Niskin bottle sample values are listed in Tables 2.20 and 2.21 respectively. Note that questionable values are included in the hydrology data file, whereas bad values have been removed.

Laboratory temperature on the ship was stable, with lab temperatures at the times of nutrient analyses having a most common value of 19.6°C.

For stations 23 to 26, autoanalyser peak heights for silicate were measured manually, and a linear fit was applied to the calibration standards.

For station 22, bottle salinity values were bad, and were not used in the calibration procedure.

For stations 28 and 42, phosphate data were bad.

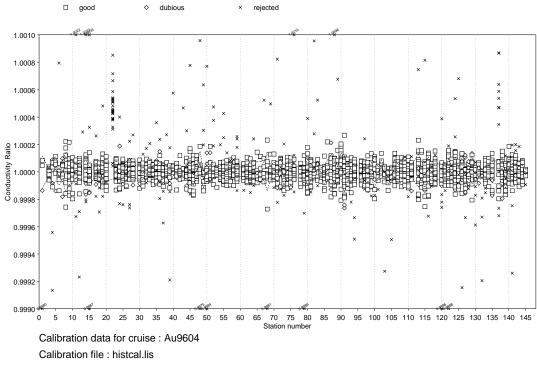


Calibration file: histcal.lis

Mean offset Temperature = 0.00190312c (s.d. = 0.0068 °c)

Number of samples used = 289 out of 326

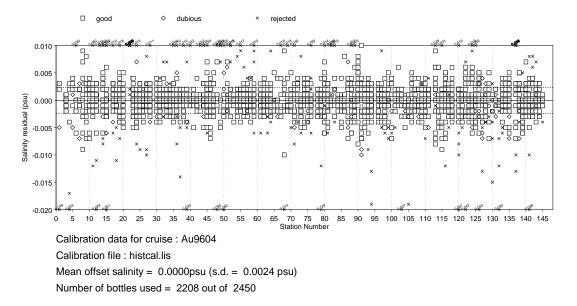
<u>Figure 2.2:</u> Temperature residual ( $T_{therm}$  -  $T_{cal}$ ) versus station number for cruise au9604. The solid line is the mean of all the residuals; the broken lines are  $\pm$  the standard deviation of all the residuals (see CTD methodology). Note that the "dubious" and "rejected" categories refer to the conductivity calibration.



Calibration file: nistcal.iis Conductivity s.d. = 0.00006

Number of bottles used = 2208 out of 2450 Mean ratio for all bottles = 1.00000

<u>Figure 2.3:</u> Conductivity ratio  $c_{btl}/c_{cal}$  versus station number for cruise au9604. The solid line follows the mean of the residuals for each station; the broken lines are  $\pm$  the standard deviation of the residuals for each station (see CTD methodology).



<u>Figure 2.4:</u> Salinity residual ( $s_{btl}$  -  $s_{cal}$ ) versus station number for cruise au9604. The solid line is the mean of all the residuals; the broken lines are  $\pm$  the standard deviation of all the residuals (see CTD methodology).

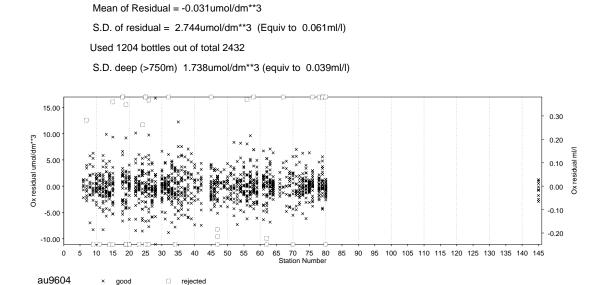


Figure 2.5: Dissolved oxygen residual (o<sub>btl</sub> - o<sub>cal</sub>) versus station number for cruise au9604.

<u>Table 2.9:</u> Surface pressure offsets (as defined in the CTD methodology). \*\* indicates that value is estimated from surrounding stations, or else determined from manual inspection of pressure data.

stn no.	surface p offset (dbar)	stn no.	surface p offset (dbar)	stn no.	surface p offset (dbar)	stn no.	surface p offset (dbar)
1	-0.25	41	-0.37	81	-0.33	121	-0.84
2	-0.61	42	-0.49	82	-0.89	122	
3	0.37	43	-0.48	83	-0.92	123	-1.01
4	0.11	44	-0.39	84	-0.56	124	-1.06
5	0.95	45	0.05	85	-0.51	125	-0.86
6	1.16	46	-0.65	86	-0.47	126	-0.84
7	1.33	47	-0.19	87	-0.35	127	
8	1.36**	48	0.00**	88	-0.75	128	
9	1.40	49	-0.40	89	-0.77**	129	-0.76
10	0.41	50	-0.15	90	-0.80	130	-0.17
11	1.61	51	-0.54	91	-0.74	131	-1.06
12	0.09	52	-0.32	92	-0.81	132	-0.27
13	0.28	53	-0.25	93	-0.88	133	-0.61
14	0.16	54	-0.99	94	-0.64	134	-0.84
15	0.04	55	-0.46	95	-0.75	135	
16	-0.06	56	-0.69	96	-0.92	136	
17	-0.03	57	-1.01	97	-0.75	137	-1.22
18	-0.24	58	-0.70	98	-0.39	138	-0.97
19	-0.22	59	-0.51	99	-0.45	139	-0.80
20	-0.36	60	-0.20	100		140	-0.87
21	0.07	61	-1.02	101		141	-0.93
22	-0.33	62	0.94	102		142	
23	-0.34	63	-0.45	103		143	
24	-0.59	64	-0.80	104		144	-0.81
25	-0.38	65	-0.26	105		145	0.09
26	-0.36	66	-0.45	106		146	0.13
27	-0.26	67	-0.35	107		147	-0.45
28	-0.46	68	-0.50**	108			
29 30	-0.20**	69 70	-0.42 -0.16	109 110			
	-1.05	70 71		111			
31 32	-0.33 -0.40	71 72	-0.27 -0.20	112			
33	-0.40 -0.53	73	-0.20 -0.14	113			
34	-0.30	74	-0.14	114			
35	-0.53	7 <del>4</del> 75	-0.69	115			
36	-0.55 -0.41	76	-0.84	116			
37	-0.68	70 77	-0.49	117			
38	-0.09	78	-0.49	118			
39	-0.08	79	-0.47	119			
40	-0.37	80	-0.47	120			
70	5.07	00	5.10	120	1.02		

<u>Table 2.10:</u> CTD conductivity calibration coefficients.  $F_1$ ,  $F_2$  and  $F_3$  are respectively conductivity bias, slope and station-dependent correction calibration terms. n is the number of samples retained for calibration in each station grouping;  $\sigma$  is the standard deviation of the conductivity residual for the n samples in the station grouping (see CTD methodology);  $\alpha$  is the correction applied to CTD conductivities due to pressure dependence of the conductivity residuals (see eqn 1.1 in Part 1 of this report).

stn grouping	g F₁	$F_2$	$F_3$	n	σ	α
001 to 001	-3.4008230	0.10266676E-02	0	3	0.004993	-
002 to 002	-3.4008230	0.10266676E-02	0	3	0.004993	-
003 to 004	0.55764682	0.99645743E-03	28960267E-05	24	0.001263	_
005 to 007	52606214E-02	0.10046804E-02	0.95765457E-07	23	0.002064	-
008 to 008	0.44036103E-01	0.10031503E-02	0	11	0.004031	-
009 to 010	79348989E-01	0.10081906E-02	41941891E-07	31	0.002407	-
011 to 017	63365640E-01	0.10072857E-02	0.92934405E-08	98	0.001785	6.30E-07
018 to 019	16941205E-01	0.10072037E 02 0.10029438E-02	0.16218103E-06	41	0.001703	6.30E-07
020 to 024	34773276E-01	0.10029430E-02 0.10062501E-02	0.27600438E-07	67	0.002006	6.30E-07(stn20)
020 10 024	.04770270L 01	0.100020012 02	0.27000+00L 07	01	0.002000	6.99E-07(stn21-24)
025 to 027	42861170E-01	0.10088248E-02	72135270E-07	65	0.001325	6.99E-07
028 to 030	38426094E-01	0.10043136E-02	0.84881449E-07	45	0.001317	6.99E-07
031 to 033	45089981E-01	0.10086500E-02	50005682E-07	67	0.001169	8.14E-07
034 to 035	16210020E-01	0.10136385E-02	22598949E-06	41	0.001225	8.14E-07
036 to 037	21369310E-01	0.10091878E-02	82466648E-07	31	0.001514	8.14E-07
038 to 040	50591527E-02	0.10050644E-02	0.20181984E-07	32	0.001201	8.14E-07
041 to 042	45224069E-01	0.10118294E-02	10457316E-06	20	0.001201	7.36E-07
043 to 044	89106026E-01	0.10309086E-02	50554005E-06	26	0.001213	7.36E-07
045 to 047	17972448E-02	0.10058200E-02	25894965E-08	69	0.001300	7.36E-07 7.36E-07
048 to 051	11278398E-02	0.10038200E-02 0.10018826E-02	0.75038871E-07	32	0.001943	7.36E-07(stn48-50)
046 (0 05)	112/0390E-02	0.10010020E-02	0.73030071E-07	32	0.002176	6.06E-07(stn51)
052 to 054	220201765 01	0.40077043E.03	29925844E-07	11	0.001056	
052 to 054	22038176E-01	0.10077813E-02		41	0.001056	6.06E-07
055 to 057	25708043E-01	0.10036519E-02	0.51001329E-07	63	0.001257	6.06E-07
058 to 060	16543813E-01	0.10067962E-02	11086368E-07	39	0.001133	6.06E-07
061 to 062	47632077E-01	0.10066633E-02	0.10413888E-07	45	0.001201	6.06E-07(stn61)
062 to 064	60785919E-02	0.404550025.02	15326305E-06	40	0.001144	- (stn62)
063 to 064		0.10155002E-02		40	0.001144	-
065 to 066	16546893E-01	0.10296772E-02	35846498E-06	14	0.001768	•
067 to 068	0.55308088E-02	0.10128742E-02	10922184E-06	13	0.003147	(-4-00.70)
069 to 074	22735305E-01	0.10084174E-02	30649004E-07	82	0.001731	- (stn69-70) 10.16E-07(stn71-74)
075 to 076	86408281E-01	0.10071895E-02	0.16918503E-07	41	0.001395	
077 to 079	19036812E-01	0.10126020E-02	82942800E-07	44		10.16E-07
080 to 081	24748542E-01	0.10069379E-02	84236957E-08	43		10.16E-07(stn80)
000 10 001	.247 40042L 01	0.100030732 02	.04200007 L 00	40	0.002002	4.09E-07(stn81)
082 to 084	35271471E-01	0.10118694E-02	62164157E-07	20	0.001201	4.09E-07
085 to 088	43779395E-01	0.10081677E-02	15567609E-07	56	0.002321	4.09E-07
089 to 091	26888057E-01	0.10126024E-02	70609756E-07	67	0.002901	4.09E-07(stn89-90)
000 10 00 1	.200000012 01	0.101200212 02	0000. 002 0.	0.	0.002001	7.45E-07(stn91)
092 to 093	25957370E-01	0.10035524E-02	0.29544867E-07	43	0.001936	7.45E-07
094 to 096	18031989E-01	0.10067845E-02	75915753E-08	46	0.001330	7.45E-07
097 to 099	0.72025201E-02	0.10007043E-02 0.10024057E-02	0.27868859E-07	65	0.001427	7.45E-07
100 to 101	53994702E-01	0.10024057E-02 0.10336150E-02	26094479E-06	15		7.45E-07(stn100)
100 10 101	5599 <del>4</del> 702E-01	0.10330130E-02	2009 <del>4</del> 479E-00	15	0.002207	9.30E-07(str100)
102 to 106	32221287E-01	0.10092370E-02	25813131E-07	54	0.001596	
107 to 108	27064708E-01	0.10092570E-02 0.10121597E-02	55131810E-07	35		9.30E-07 9.30E-07
107 to 108	41781867E-01	0.10121397E-02 0.10204373E-02	12507360E-06	44		9.30E-07 9.30E-07
111 to 116	51999880E-01	0.10204373E-02 0.10066765E-02	0.40501302E-08	96		10.39E-07
117 to 110	78123279E-01	0.10066765E-02	0.40501502E-08 0.14758557E-08			10.39E-07 10.39E-07
				62 65		10.39E-07 10.33E-07
121 to 123	30409364E-01 26783184E-01	0.10153867E-02	74014007E-07 63658094E-08	65 07		
124 to 129		0.10070376E-02		97		10.33E-07
130 to 132	99892436E-01	0.99483839E-03	0.10644714E-06	18		10.33E-07(stn130)
					(	6.37E-07(stn131-132)

## Table 2.10: (continued)

stn grouping	$F_1$	$F_2$	$F_3$	n	σ	α
		<del>-</del>				<b>-</b>
133 to 134	45705617E-01	0.10181827E-02	85306942E-07	44	0.001385	6.37E-07
135 to 137	56982632E-01	0.99366156E-03	0.10145251E-06	36	0.002465	6.37E-07
138 to 140	35961294E-01	0.10126337E-02	42141044E-07	67	0.002214	6.37E-07
141 to 142	18766667E-01	0.10120811E-02	42780742E-07	41	0.001695	6.37E-07
143 to 144	40630706E-01	0.98885825E-03	0.12512651E-06	40	0.001301	6.37E-07
145 to 145	0.90433855E-01	0.95596375E-03	0	6	0.000397	-
146 to 146	0.90433855E-01	0.95596375E-03	0	6	0.000397	-
147 to 147	0.90433855E-01	0.95596375E-03	0	6	0.000397	-

stn no.	(F <sub>2</sub> + F <sub>3</sub> . N)	stn no.	(F <sub>2</sub> + F <sub>3</sub> . N)	stn no.	(F <sub>2</sub> + F <sub>3</sub> . N)	stn no.	(F <sub>2</sub> + F <sub>3</sub> . N)
1	0.10266676E-02	41	0.10075419E-02	81	0.10062556E-02	121	0.10064310E-02
2	0.10266676E-02	42	0.10074373E-02	82	0.10067720E-02	122	0.10063570E-02
3	0.98776935E-03	43	0.10091704E-02	83	0.10067098E-02	123	0.10062829E-02
4	0.98487332E-03	44	0.10086648E-02	84	0.10066477E-02	124	0.10062482E-02
5	0.10051592E-02	45	0.10057035E-02	85	0.10068445E-02	125	0.10062418E-02
6	0.10052550E-02	46	0.10057009E-02	86	0.10068289E-02	126	0.10062355E-02
7	0.10053508E-02	47	0.10056983E-02	87	0.10068134E-02	127	0.10062291E-02
8	0.10031503E-02	48	0.10054845E-02	88	0.10067978E-02	128	0.10062227E-02
9	0.10079131E-02	49	0.10055595E-02	89	0.10063182E-02	129	0.10062164E-02
10	0.10078712E-02	50	0.10056346E-02	90	0.10062476E-02	130	0.10086765E-02
11	0.10073879E-02	51	0.10057096E-02	91	0.10061770E-02	131	0.10087830E-02
12	0.10073972E-02	52	0.10062251E-02	92	0.10062705E-02	132	0.10088894E-02
13	0.10074065E-02	53	0.10061952E-02	93	0.10063001E-02	133	0.10068369E-02
14	0.10074158E-02	54	0.10061653E-02	94	0.10060709E-02	134	0.10067516E-02
15	0.10074251E-02	55	0.10064570E-02	95	0.10060633E-02	135	0.10073576E-02
16	0.10074344E-02	56	0.10065080E-02	96	0.10060557E-02	136	0.10074591E-02
17	0.10074437E-02	57	0.10065590E-02	97	0.10051090E-02	137	0.10075606E-02
18	0.10058631E-02	58	0.10061532E-02	98	0.10051368E-02	138	0.10068183E-02
19	0.10060253E-02	59	0.10061421E-02	99	0.10051647E-02	139	0.10067761E-02
20	0.10068021E-02	60	0.10061310E-02	100	0.10075206E-02	140	0.10067340E-02
21	0.10068297E-02	61	0.10072986E-02	101	0.10072596E-02	141	0.10060490E-02
22	0.10068573E-02	62	0.10073090E-02	102	0.10066040E-02	142	0.10060063E-02
23	0.10068849E-02	63	0.10058447E-02	103	0.10065782E-02	143	0.10067513E-02
24	0.10069125E-02	64	0.10056914E-02	104	0.10065524E-02	144	0.10068765E-02
25	0.10070214E-02	65	0.10063770E-02	105	0.10065266E-02	145	0.95596375E-03
26	0.10069493E-02	66	0.10060185E-02	106	0.10065008E-02	146	0.95596375E-03
27	0.10068771E-02	67	0.10055564E-02	107	0.10062606E-02	147	0.95596375E-03
28	0.10066903E-02	68	0.10054471E-02	108	0.10062055E-02		
29	0.10067751E-02	69	0.10063026E-02	109	0.10068043E-02		
30	0.10068600E-02	70	0.10062720E-02	110	0.10066792E-02		
31	0.10070999E-02	71	0.10062413E-02	111	0.10071260E-02		
32	0.10070499E-02	72	0.10062107E-02	112	0.10071301E-02		
33	0.10069999E-02	73	0.10061800E-02	113	0.10071341E-02		
34	0.10059549E-02	74	0.10061494E-02	114	0.10071382E-02		
35	0.10057289E-02	75	0.10084584E-02	115	0.10071422E-02		
36	0.10062190E-02	76	0.10084753E-02	116	0.10071463E-02		
37	0.10061365E-02	77	0.10062154E-02	117	0.10080803E-02		
38	0.10058313E-02	78	0.10061325E-02	118	0.10080818E-02		
39	0.10058515E-02	79	0.10060495E-02	119	0.10080833E-02		
40	0.10058717E-02	80	0.10062640E-02	120	0.10080847E-02		

<u>Table 2.12:</u> CTD raw data scans flagged for special treatment (see previous data reports for explanation).

station	approximate	raw scan	action	reason
number	pressure (dbar)	numbers	taken	
4(downcas	st) 286	22602-22953	ignore	fouling of cond. cell
7(downcas	st) 146	10608-10626	ignore	bad data scans
145(upcast)		571-579,730-741,799-802	ignore	bad pressure data
145(upcast)		855-858,1137-1140,1404-140	8 ignore	bad pressure data
145(upcast)		2218-2236,2872-2879	ignore	bad pressure data
145(upcast)		5607-5612,5703-5711	ignore	bad pressure data
146(upcast)		3097-3100,3151-3155,3260-3	263 ignore	bad pressure data
146(upcast)		3286-3298,3334-3337,3388-3	390 ignore	bad pressure data
146(upcast)		3421-3425,3442-3445,3477-3	480 ignore	bad pressure data
147(upcast)		3036-3039,3142-3146,3158-3	163 ignore	bad pressure data
147(upcast)		3210-3213	ignore	bad pressure data

<u>Table 2.13:</u> Missing data points in 2 dbar-averaged files. "1" indicates missing data for the indicated parameters: T=temperature; S=salinity,  $\sigma_T$ , specific volume anomaly and geopotential anomaly; O=dissolved oxygen; PAR=photosynthetically active radiation; F=fluorescence. Note that jmin is the minimum number of data points required in a 2 dbar bin to form the 2 dbar average (see CTD methodology).

station number	pressures (dbar) where data missing	Т	S	0	PAR	F	reason
1	entire profile		4	1			no bottles for oxygen calibration
2 3	entire profile entire profile		1	1			no bottles for calibration bad oxygen data
3	3924	1	1	1	1		no. of data pts in 2 dbar bin < jmin
4,5	entire profile	'	'	1	'		no bottles for oxygen calibration
8	2	1	1	' 1	1		CTD not logging
13	618	1	1	1			no. of data pts in 2 dbar bin < jmin
16,21,29	entire profile	ı	•	1	'		no bottles for oxygen calibration
17	entire profile			1			bad oxygen data
20	2852-2864			1			bad oxygen data
26	2-58			1			bad oxygen data
35	448	1	1	1	1		no. of data pts in 2 dbar bin < jmin
38	1210	1	1	1	1		no. of data pts in 2 dbar bin < jmin
40	522	1	1	1	1		no. of data pts in 2 dbar bin < jmin
41	2-16			1			bad oxygen data
43	entire profile			1			no bottles for oxygen calibration
43	100	1	1	1	1		no. of data pts in 2 dbar bin < jmin
44	2032-2104		1				fouling of cond. cell
44	entire profile			1			bad oxygen data
60	entire profile			1			no bottles for oxygen calibration
62	2	1	1	1			bad data
62	950	1	1	1	1		no. of data pts in 2 dbar bin < jmin
62	952			1			bad oxygen data
64	932-946		1				fouling of cond. cell
65,77	entire profile			1			no bottles for oxygen calibration
72	1832	1	1	1	1		no. of data pts in 2 dbar bin < jmin
74	18-28			1			bad oxygen data
75	2542	1	1	1	1		no. of data pts in 2 dbar bin < jmin
79	2-72			1			bad oxygen data
82	2	1	1				bad data

Table 2.13: (continued)

station number	pressures (dbar) where data missing	Т	S	0	PAR	F	reason
83 89 92 97 98 123 133 134 141 81-144 145 146,147 147 1-3,14-33 35 36-147	438 2 3518 3888 2110-3106 1904-2180 3952 3926 1804 entire profile 326,374,428 entire profile 2-24 entire profile entire profile entire profile	1 1 1 1 1 1	1 1 1 1 1 1 1	1 1 1 1 1 1 1	1 1 1 1 1	1 1 1	no. of data pts in 2 dbar bin < jmin CTD not logging no. of data pts in 2 dbar bin < jmin no. of data pts in 2 dbar bin < jmin fouling of cond. cell fouling of cond. cell no. of data pts in 2 dbar bin < jmin no. of data pts in 2 dbar bin < jmin no. of data pts in 2 dbar bin < jmin no. of data pts in 2 dbar bin < jmin bad oxygen data bad oxygen data bad oxygen data no bottles for oxygen calibration fouling of cond. cell fluorometer not installed bad fluorometer data fluorometer not installed

<u>Table 2.14:</u> 2 dbar averages interpolated from surrounding 2 dbar values, for the indicated parameters.

station number	interpolated 2 dbar values	parameters interpolated
2	3320	T, PAR
133	1482	T, S, PAR
135	1986	T, S, PAR

<u>Table 2.15a:</u> Suspect 2 dbar salinity averages (+ temperature where indicated). Note: for suspect salinity values, the following are also suspect:  $\sigma_T$ , specific volume anomaly, and geopotential anomaly.

geopotential and		har valuas (dhar)	roccon
station		bar values (dbar)	reason
number	bad	questionable	
3	-	66	salinity spike in steep local gradient
4	-	64,66	salinity spike in steep local gradient
9	-	138	bad data scans
11	-	36,38	salinity spike in steep local gradient
13	-	52,54	salinity spike in steep local gradient
15	-	600	salinity spike in steep local gradient
17	_	198,200	salinity spike in steep local gradient
18	_	150,152	salinity spike in steep local gradient
20	_	2856-2870	possible fouling of conductivity cell
21	_	48	
	-		salinity spike in steep local gradient
22	-	52,54	salinity spike in steep local gradient
30	-	8,10	salinity spike in steep local gradient
32	-	170	salinity spike in steep local gradient
36	-	46	salinity spike in steep local gradient
39	-	12,14	salinity spike in steep local gradient
46	-	44,46	salinity spike in steep local gradient
59	_	42,44	salinity spike in steep local gradient
61	_	40,42	salinity spike in steep local gradient
62	_	952	possible fouling of conductivity cell
63	_	108,110	salinity spike in steep local gradient
70		14-20	
	-		salinity spike in steep local gradient
80	-	32,34	salinity spike in steep local gradient
85	-	36	salinity spike in steep local gradient
93	-	34,64,66	salinity spike in steep local gradient
94	-	34,42-52	salinity spike in steep local gradient
97	-	38,56	salinity spike in steep local gradient
98	-	34,36	salinity spike in steep local gradient
99	-	44,46	salinity spike in steep local gradient
104	-	36,38	salinity spike in steep local gradient
107	-	38	salinity spike in steep local gradient
109	_	32,34,138,168	salinity spike in steep local gradient
110	_	32	salinity spike in steep local gradient
111	_	40-44	salinity spike in steep local gradient
112	_	52-56	salinity spike in steep local gradient
	_	42	
113	-		salinity spike in steep local gradient
114	-	50-54	salinity spike in steep local gradient
117	-	54-58	salinity spike in steep local gradient
118	-	64	salinity spike in steep local gradient
119	-	56	salinity spike in steep local gradient (T also)
120	-	48-52	salinity spike in steep local gradient
129	-	696	salinity spike in steep local gradient
133	-	64,66	salinity spike in steep local gradient
137	_	62,64	salinity spike in steep local gradient
140	_	56,58,126	salinity spike in steep local gradient
142	_	34,36	salinity spike in steep local gradient
: f <b>4</b>		J=,00	daminity opinio in otoop loodi gradient

<u>Table 2.15b:</u> Suspect 2 dbar-averaged data from near the surface (applies to all parameters other than dissolved oxygen, except where noted).

stn s	uspect 2	dbar values			2dbar values
no.		questionable	no.	bad	questionable
3,4	2	4	67	2	-
5, ¬	2,4	-	68	2-60	- (T okay)
6,7	_,-	2	69	2,4	6
8	_	4	70,71		2
10	-			-	4
	-	2 (T okay)	74,75	2	
11,12	-	2	76 70	-	2-6
13	2	4	79	-	2
14	2,4	6	80	2	4
15	-	2	82	-	4
16	2	4,6	83	-	2
17	-	2,4	84,85	2	4
18,19	-	2	86	-	2
20	-	2-6	87	-	2,4
21	-	2,4	90	-	2
22	-	2	91	2	4
22	-	4 (T okay)	92	-	2,4
23	-	2	94	-	2
24	2	-	96,97	-	2
26	2	4-8	98,99	2	4
27	2	4	100,10		2
29	-	2	102	2	4,6
31	2	4	103	_	2
32,33	-	2	104	_	_ 2,4
34	_	2,4	105	_	2
34	_	6 (T okay)	106,10	7 -	2,4
35	_	2,4	108,10	2	4
35		6 (T okay)	109	2	4
36,37	_	2	110,11		2,4
30,3 <i>1</i> 39	-	2	110,11	2	4
40	-		113	2	2
	-	2,4 (T okay)		-	
41,42	-	2,4	114,11		2,4
43	2	4	116-11	0 -	2
44,45	-	2,4	119	-	2,4
46-48	-	2	120	-	2
49	-	2,4	121	2	4
50	-	2	123	-	2,4
51	-	2,4	124	-	2
52	2	-	125	-	2,4
52	-	4-14 (T okay)	126	2	4
53	2	-	127	2	-
53	-	4-14 (T okay)	128	2	4
54	2	4	129	-	2,4
55	2	-	130	2	4,6
56	2	4	131	-	2
57	-	2,4	132	-	2,4
58,59	-	2	133	2	4,6
60	-	2 (T okay)	134	-	2,4
62	4	6	135	-	2-6
63	2	4	136,13	7 -	2
64	-	2	138	-	2,4
65	2	4	139	-	2
66	-	2	140	-	_ 2,4
66	_	4-18 (T okay)	141,14	2 -	2
			143,14		4
			,		•

<u>Table 2.16:</u> Suspect 2 dbar-averaged dissolved oxygen data.

stn	suspect	2dbar values(dbar)	stn su	spect 2	dbar values(dbar)		
no.	bad	questionable	no.	no. bad questionable			
6	-	16-28	42	-	2-12		
9	-	2-12,138,228	45	-	2		
9	-	230,262,264	47	-	2,4		
11	-	2	48	-	14-56		
13	-	2-6	49	-	2-12		
14	-	2,4	51	-	2-10		
23	-	2-42	54	-	6-10		
27	-	2-16	55	-	2-14		
28	-	2-6,48-56	56	-	2		
30	-	2-6	57	-	2,4		
31	-	2-26,54-58	58	-	2-8		
32	-	2	62	-	4-8,954-960		
33	-	2-8	63	-	2-28		
34	-	4-30	64	-	932-946		
35	-	2-10	67	-	2,10-58		
38	-	2-8,54-60	68	-	2-12		
41	-	54-60	75	-	2		

<u>Table 2.17:</u> CTD dissolved oxygen calibration coefficients.  $K_1$ ,  $K_2$ ,  $K_3$ ,  $K_4$ ,  $K_5$  and  $K_6$  are respectively oxygen current slope, oxygen sensor time constant, oxygen current bias, temperature correction term, weighting factor, and pressure correction term. dox is equal to 2.8 $\sigma$  (for  $\sigma$  as defined by eqn A2.24 in the CTD methodology); n is the number of samples retained for calibration in each station or station grouping.

station number	. <b>Κ</b> <sub>1</sub>	$K_2$	K <sub>3</sub>	$K_4$	K <sub>5</sub>	K <sub>6</sub>	dox	n
1-5	-	-	-	-	-	-	-	-
6	7.418	5.00	-0.565	-0.06023	1.6962	-0.20179E-04	0.07725	7
7	6.872	5.00	-0.708	-0.13410	0.7181	0.24655E-03	0.14338	10
8	3.642	5.00	0.096	-0.12494	0.5941	-0.10229E-03	0.21158	11
9	7.093	5.00	-0.748	-0.11343	0.6713	0.89483E-04	0.23546	13
10	11.981	5.00	-1.621	-0.17472	0.9308	0.12612E-03	0.10240	17
11	6.451	5.00	-0.560	-0.14690	0.6141	0.67143E-04	0.10334	17
12	17.160	5.00	-2.450	-0.25734	1.0491	0.14873E-03	0.19673	24
13	20.289	5.00	-3.071	-0.25086	1.0967	0.17067E-03	0.19821	23
14	6.458		-0.699	-0.05269	0.2338	0.98041E-04	0.13005	23
15	14.242	5.00	-2.061	-0.16623	0.9724	0.14757E-03	0.20143	22
16-17	-	-	-	-	-	-	-	-
18	14.222	5.00	-2.049	-0.14751	1.0652	0.14078E-03	0.22139	22
19	8.206	5.00	-0.813	-0.17663	0.7010	0.61268E-04	0.21079	19
20	9.633	5.00	-1.285	-0.08468	0.7706	0.13244E-03	0.14319	20
21	-	-	-	-	-	-	-	-
22	14.502	5.00	-2.099	-0.16000	0.8689	0.14116E-03	0.22888	23
23	12.887	6.00	-1.907	-0.10053	0.8371	0.16632E-03	0.11743	22
24	13.362	5.00	-1.989	-0.11649	0.9941	0.20188E-03	0.24027	23
25	12.223	5.00	-1.746	-0.09636	0.8988	0.15115E-03	0.15767	21
26	9.611	5.00	-1.041	-0.25649	0.7004	0.80656E-04	0.25574	22
27	7.947	5.00	-0.957	-0.09613	0.6344	0.11430E-03	0.17697	24
28	12.035	5.00	-1.684	-0.15714	0.6915	0.13169E-03	0.29089	24
29	-	-	-	-	-	-	-	-

Table 2.17: (continued)

station number	<b>K</b> <sub>1</sub>	$K_2$	<b>K</b> <sub>3</sub>	K <sub>4</sub>		K <sub>5</sub>	K <sub>6</sub>	dox	n
30	11.283	5.00	-1 590	-0.11215	0	.5598	0.12912E-03	0.15112	24
31	10.148		-1.384	-0.08487		.7658	0.13585E-03	0.14159	
32	7.618		-0.916	-0.04725		.5352	0.11641E-03	0.16382	
33	35.331		-5.598	-0.38808		.0868	0.20304E-03	0.18587	
34	16.145		-2.448	-0.16724		.9970	0.18210E-03	0.18263	
35	13.675		-1.902	-0.17720		.9764	0.12958E-03	0.27098	
36	14.710			-0.19929		.9144	0.14117E-03	0.23900	
37	18.358			-0.21192		.9571	0.15181E-03	0.17370	
38	21.256		-3.387	-0.25768		.8768	0.25256E-03	0.24543	
39	10.125		-1.226	-0.12277			-0.16664E-04	0.24269	
40	8.252			-0.08883		.2829	0.22137E-03	0.20618	
41	13.477		-1.923	-0.14286		.8308	0.18302E-03	0.09454	
42	13.110		-1.792	-0.11370		.9803	0.15074E-03	0.20964	
43-44	-	-	-	-	Ū	-	-	-	-
45	8.231	5.00	-1.044	-0.09496	0	.5569	0.12043E-03	0.14826	23
46	9.107		-1.227	-0.05124		.3477	0.12590E-03	0.11759	
47	14.485		-2.190	-0.12723		.2218	0.18700E-03	0.12920	
48	2.745		1.062	0.37630			-0.12314E-03	0.13448	
49	17.719		-2.755	-0.19351		.0108	0.22516E-03	0.11148	
50	14.718		-2.083	-0.21094		.8862	0.15609E-03	0.14124	
51	12.666			-0.18490		.8430	0.73093E-04	0.13368	
52	15.079		-2.041	-0.23234		.8909	0.10585E-03	0.22428	
53	16.435		-2.359	-0.21402		.9059	0.12835E-03	0.17349	
54	8.565		-1.023	-0.09570		.5068	0.87403E-04	0.18297	
55	17.456		-2.586	-0.18771		.9519	0.14376E-03	0.14614	
56	13.541		-1.848	-0.17231		.8238	0.11222E-03	0.18034	
57	17.585		-2.693	-0.18359		.9900	0.16884E-03	0.19072	
58	8.252		-1.050	-0.04507		.2405	0.11100E-03	0.17519	
59	12.812		-1.830	-0.11619		.8256	0.13463E-03	0.15943	
60	_	-	-	-		-	-	-	-
61	15.443	8.00	-2.249	-0.15869	0	.7950	0.12621E-03	0.16280	24
62	7.552	5.00	-0.872	-0.08247	0	.3376	0.89890E-04	0.18896	21
63	7.801	5.00	-0.920	-0.07044	0	.3663	0.96123E-04	0.17730	24
64	10.588	8.00	-1.423	-0.09551	0	.4398	0.10736E-03	0.10591	24
65	-	-	-	-		-	-	-	-
66	15.627	5.00	-2.396	-0.23340	0	.7954	0.21008E-03	0.09261	8
67	10.786	5.00	-1.332	-0.12683	0	.9951	0.14226E-03	0.17909	5
68	13.291	6.00	-1.900	-0.14946	0	.8944	0.24323E-03	0.20779	8
69	25.046	5.00	-4.052	-0.26061	1	.0344	0.20912E-03	0.14930	
70	15.205	5.00	-2.163	-0.21336	0	.8850	0.12566E-03	0.20667	
71	7.230			-0.22886	0	.5820	0.37917E-04	0.21003	14
72	11.370			-0.18495	0	.7181	0.94158E-04	0.13537	
73	6.947			-0.08066		.2406	0.86378E-04	0.14414	
74	15.394			-0.20745		.9438	0.18530E-03	0.15400	
75	7.348			-0.04344		.3395	0.11707E-03	0.10340	
76	13.500	10.0	-2.049	-0.06560	1	.2992	0.19319E-03	0.11749	23
77	-	-	-	-		-	-	-	-
78	10.578			-0.04315		.8707		0.10303	
79	5.153			-0.08473		.6596	0.98564E-04	0.16396	
80	11.496		-1.606	-0.08090	0	.9995	0.14893E-03	0.07288	22
81-144		-	-	-		-	-	-	-
145	6.980		-0.716	-0.11934	0	.5563	0.12412E-03	0.10894	9
146-147	7 -	-	-	-		-	-	-	-

<u>Table 2.18:</u> Starting values for CTD dissolved oxygen calibration coefficients prior to iteration, and coefficients varied during iteration (see CTD methodology). Note that coefficients not varied during iteration are held constant at the starting value.

station number	K <sub>1</sub>	K <sub>2</sub>	<b>K</b> <sub>3</sub>	K <sub>4</sub>	K <sub>5</sub>	K <sub>6</sub>	coefficients varied
1-5 6 7 8 9 10 11 12 13 14 15	9.100 6.600 6.600 12.400 11.700 6.700 9.300 8.400 8.300 11.300	5.0000 5.0000 5.0000 5.0000 5.0000 5.0000 5.0000 5.0000 5.0000	-0.200 -0.800 -1.100 -1.700 -1.400 -0.600 1.600 0.400 -0.100 -2.400	-0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01	0.750 0.750 0.750 0.750 0.750 0.750 0.750 0.750 0.750 0.750	0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
18 19 20 21	10.500 8.200 9.550	5.0000 5.0000 5.0000	-2.500 -0.700 -1.300	-0.360E-01 -0.360E-01 -0.360E-01	0.750 0.750 0.750	0.15000E-03 0.15000E-03 0.15000E-03	K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub>
22 23 24 25 26 27 28	12.600 9.410 11.170 11.200 9.900 9.300 12.600	5.0000 6.0000 5.0000 5.0000 5.0000 5.0000 5.0000	-2.100 -2.100 -2.300 -2.000 -1.100 -0.700 -1.400	-0.360E-01 -0.360E-01 -0.300E-01 -0.360E-01 -0.360E-01 -0.360E-01	0.750 0.750 0.750 0.750 0.750 0.750 0.750	0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
29 30 31 32 33 34 35 36 37 38 39	13.600 10.100 12.000 9.100 13.330 12.000 14.400 7.500 3.900 7.900	5.0000 5.0000 5.0000 5.0000 5.0000 5.0000 5.0000 5.0000 5.0000	-0.800 -1.400 0.000 -2.300 -2.300 -2.000 -1.900 1.000 0.500 -1.300	-0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01	0.750 0.750 0.750 0.750 0.750 0.750 0.750 0.750 0.750	0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03	K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub>
40 41 42 43-44	8.900 12.400 12.700	6.0000 5.0000 5.0000	-1.000 -2.100 -1.900	-0.360E-01 -0.360E-01 -0.360E-01	0.750 0.750 0.750 -	0.15000E-03 0.15000E-03 0.15000E-03	$\begin{array}{cccc} K_1 & K_3  K_4  K_5  K_6 \\ K_1 & K_3  K_4  K_5  K_6 \\ K_1 & K_3  K_4  K_5  K_6 \\ & - \end{array}$
45 46 47 48 49 50 51 52 53 54 55 56 57	9.500 12.700 13.000 14.610 14.800 14.900 14.700 14.200 15.400 8.700 15.000 12.100	5.0000 5.0000 5.0000 8.0000 8.0000 6.0000 5.0000 5.0000 5.0000 6.0000	-0.800 -0.300 -2.100 -0.700 -2.200 -2.100 -1.000 -2.300 -1.000 -2.200 -1.900	-0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01	0.750 0.750 0.750 0.750 0.750 0.750 0.750 0.750 0.750 0.750 0.750	0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03	K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>1</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub>

Table 2.18: (continued)

station number	. K <sub>1</sub>	$K_2$	K <sub>3</sub>	K <sub>4</sub>	<b>K</b> <sub>5</sub>	K <sub>6</sub>		efficients ried
58 59 60	11.900 11.300	5.0000 5.0000	0.100 -2.100	-0.360E-01 -0.360E-01	0.750 0.750	0.15000E-03 0.15000E-03	$\mathbf{K}_1$ $\mathbf{K}_1$	$K_3 K_4 K_5 K_6 K_3 K_4 K_5 K_6$
61 62 63 64	13.750 8.400 11.000 11.200	8.0000 5.0000 5.0000 8.0000	-2.500 -0.700 -2.300 -1.300	-0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01	0.750 0.750 0.750 0.750	0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03	K <sub>1</sub> K <sub>1</sub> K <sub>1</sub>	K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub>
65 66 67	10.800 10.300	- 5.0000	-1.700 -1.500	-0.360E-01 -0.470E-01	- 0.750	- 0.15000E-03	K <sub>1</sub>	- K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub>
68 69	10.900 11.720	5.0000 6.0000 5.0000	-2.300 -2.200	-0.360E-01 -0.360E-01	0.750 0.750 0.740	0.15000E-03 0.15000E-03 0.15000E-03	K₁ K₁ K₁	$K_3 K_4 K_5 K_6$ $K_3 K_4 K_5 K_6$ $K_3 K_4 K_5 K_6$
70 71 72	13.600 15.000 11.700	5.0000 5.0000 5.0000	-2.300 -1.200 -1.300	-0.360E-01 -0.360E-01 -0.360E-01	0.750 0.750 0.750	0.15000E-03 0.15000E-03 0.15000E-03	K₁ K₁ K₁	$K_3 K_4 K_5 K_6$ $K_3 K_4 K_5 K_6$ $K_3 K_4 K_5 K_6$
73 74 75	7.300 12.800 9.900	8.0000 8.0000 5.0000	-0.700 -1.800 -0.200	-0.360E-01 -0.360E-01 -0.360E-01	0.750 0.750 0.750	0.15000E-03 0.15000E-03 0.15000E-03	K₁ K₁ K₁	K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub>
76 77	12.820	10.0000	-2.300 -	-0.400E-01 -	0.750 -	0.15000E-03 -	K <sub>1</sub>	K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub>
78 79 80	10.600 6.500 14.500	5.0000 5.0000 10.0000	-1.500 -0.300 -0.900	-0.360E-01 -0.360E-01 -0.600E-01	0.750 0.750 0.700	0.15000E-03 0.15000E-03 0.15000E-03	$egin{array}{c} K_1 \ K_1 \end{array}$	$K_3 K_4 K_5 K_6$ $K_3 K_4 K_5 K_6$ $K_3 K_4 K_5 K_6$
81-144 145 146-147	- 11.400 -	- 7.0000 -	0.000	- -0.360E-01 -	- 0.750 -	- 0.15000E-03 -	K <sub>1</sub>	- K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> -

<u>Table 2.19:</u> Dissolved oxygen Niskin bottle samples flagged as -9 for dissolved oxygen calibration. Note that this does not necessarily indicate a bad bottle sample - in many cases, flagging is due to bad CTD dissolved oxygen data.

station	rosette	station	rosette
number	position	number	position
7	4	47	21,20,19
9	5	56	17
11	11	58	20
14	22	62	21,20
15	22,21	67	17
18	21,19	70	8
19	21,20,19,1	76	23
20	22,21,20	78	22
23	24	79	24,23,22
24	22	80	23,21
25	23,21,19		
26	22,20		
32	23		
34	24		
45	21		

<u>Table 2.20:</u> Questionable dissolved oxygen Niskin bottle sample values (not deleted from hydrology data file).

stn no.	rosette position
17	14
101	5,3

Table 2.21: Questionable nutrient sample values (not deleted from hydrology data file).

PHOSPHA	ATE	NITRAT	Έ	SILICAT	E
station number	rosette position	station number	rosette position	station number	rosette position
		12	9,8	0.4	
26 34	6 22,11,7	26	6	24 26	7-17 6
40	5			47	6,3
53	20			57	whole stn
58	12				
62	7				
74	whole stn	79	9-12		
		404	4.0	96	whole stn
118	5	101 118 126 133 135	12 5 7 12 21	118	5
144	3	144	10		

<u>Table 2.22:</u> Protected and unprotected reversing thermometers used (serial numbers are listed).

protected therr	nometers		
station	rosette position 24	rosette position 12	rosette position 2
numbers	thermometers	thermometers	thermometers
1 to 144	12095,12096	12094	12119,12120
145 to 147	12095	12094,12096	12119,12120
unprotected th	ermometers		
station		rosette position 12	rosette position 2
numbers		thermometers	thermometers
1 to 92		11992	11993
93 to 147		11993	11992

<u>Table 2.23:</u> Calibration coefficients and calibration dates for CTD serial numbers 1103 and 1193 (unit nos 7 and 5 respectively) used during RSV Aurora Australis cruise AU9604. Note that an additional pressure bias term due to the station dependent surface pressure offset exists for each station (eqn A2.1 in the CTD methodology). Also note that platinum temperature calibrations are for the ITS-90 scale.

CTD serial 11 coefficient	03 (unit no. 7) value of coefficient	CTD serial 1 coefficient	193 (unit no. 5) value of coefficient
pressure calibration co CSIRO Calibration Fac pcal0 pcal1 pcal2 pcal3 pcal4		pressure calibration of CSIRO Calibration Fa pcal0 pcal1 pcal2 pcal3 pcal4	
platinum temperature of CSIRO Calibration Fac Tcal0 Tcal1 Tcal2		platinum temperature CSIRO Calibration Fa Tcal0 Tcal1 Tcal2	calibration coefficients acility - 26/06/1996 -0.46860e-01 0.49879e-03 0.27541e-11
pressure temperature CSIRO Calibration Fac Tpcal0 Tpcal1 Tpcal2 Tpcal3		pressure temperature CSIRO Calibration Fa Tpcal0 Tpcal1 Tpcal2 Tpcal3	e calibration coefficients acility - 09/11/1995 1.167581e+02 -2.450758e-03 0.0
coefficients for temper pressure CSIRO Calibration Fac T <sub>0</sub> S <sub>1</sub> S <sub>2</sub>		coefficients for temper pressure CSIRO Calibration Fa T <sub>0</sub> S <sub>1</sub> S <sub>2</sub>	
photosynthetically acti for fluorometer set to 0 f0 f1 f2	coefficients applied to fave radiation (par) (supplied to fave radiation (par) (supplied to fave radiation (par) (supplied to fave radiation (i.e. pried a.3.45252e+01 a.020700e-03 a.0.0 a.10 mg/m3 range (i.e. from a.1.115084e+01 a.402400e-04 a.0.0 a.4.499860 a.3.452156e-23	ed by manufacturer) rav ior to 02/02/96):	etic Division, January 1996) and w digitiser counts

## APPENDIX 2.1 Hydrochemistry Laboratory Report

Seawater samples were analysed for nutrient concentrations (nitrate plus nitrite, silicate, and phosphate), salinities, and dissolved oxygen concentrations. The methods used are described in Eriksen (1997). A new nutrient autoanalyser data logging system, methods of examining intra-run quality checks (tops), basic inter-run quality checks, and improved temperature control and monitoring were implemented on this cruise.

Number of samples analysed:

Nutrients (nitrate plus nitrite, silicate, phosphate): 2470

Salinities: 2500

Dissolved oxygens: 2450

## A2.1.1 NUTRIENTS

#### General

The same TACS cadmium reduction coil was used for all but the first run.

Nitrate + nitrite and phosphate were calibrated with first order curves, and silicate with second order

At the end of the cruise samples were run as part of the National Low Level Nutrient Collaborative Trials (NLLNCT).

Standards were made fresh every day. They were stored at around 4°C between runs. Tops and nitrites were made fresh every couple of days, and were also stored at around 4°C.

## New datalogging system

A new datalogging system was used for the first time, to replace the old DOS based 'DAPA' program. The system consisted of a Labtronics (Canada) 103 analogue to digital (A/D) board, and a Windows software package by Astoria-Pacific (USA), Faspac 1.2. Data was logged using both the Labtronics/Faspac system, and DAPA. The new program, while having some good points, was far from perfect, as summarised below. Many of the problems were to be fixed in later versions (1.30, 1.31).

#### Some comments on Faspac

#### - Good Points

- \* Generally, easy and quick to get to different parts of the program, and to use; especially when compared to the awkwardness of DAPA.
- \* Real time display of the trace is good. It is easy to look at earlier parts of a run while the run is still in progress.
- \* The display and calculation of calibration standards is excellent. It is real time so this aspect of machine performance can be observed before samples are opened. It is easy to delete outliers, and

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to see how that affects the correlation of the fitted curve, and the standard deviation of the residual between calculated and observed points.

- \* Real time calculation of concentrations is good, so it's possible to see if sample concentrations look reasonable.
- \* Keeps track of the baseline reasonably well.
- \* Correcting the peak height position for spikes is easy (in contrast to DAPA).

#### - Fatal Points

- \* Crashes, from a number of different areas in different circumstances. A warning box stating that Windows has become unstable generally appears. Mostly time is lost, as data processing needs to be repeated.
- \* Crashes during a run with large sample numbers. Get a 'Peak Num = 6553' error message. Have lost data this way.
- \* Does not handle interpolation of multiple standards correctly.

#### - Bad Points

- \* Problems in 'peak search':
- -peak smoothing does not function.
- -does not always find top of peaks.

These work in peak search window, but do not work on real data. This is both during a run, or doing a 'rerun' of data.

- \* Starting Faspac causes an oscillating voltage, which is seen on the chart recorder. To reduce the problem, the following steps are performed :
- Stop run, save run, exit Faspac, close 'Data logger' program, restart data logger and Faspac, 'Resume' run.
- \* Doesn't write Excel files properly. On reading, Excel crashes ('General protection error'). Excel also had difficulty reading text files. Excel 4 was used.
- \* Doesn't have a mouse driven 'Zoom' function. It is possible to zoom in on peaks, but only by inefficiently varying the horizontal and vertical scales.
- \* It is not exactly clear how the special symbol 'W' is used to define the baseline. It depends on the context of other W's nearby.

#### **Problems**

There was a problem with the A/D board (SN 35/91, 'original') at the mid-point voltage, where a 'glitch' was observed. It can be observed by looking at a ramped voltage input from a signal generator (see Figure A2.1.1). This affected a number of nitrate + nitrite values. The gain of the nitrate detector was reduced so that the maximum signal did not reach the voltage of the 'glitch'.

There was a problem with the phosphate channel. On a number of runs, high phosphate values were seen for seawater samples, but not for standards prepared in saline solution. The raw output for standards was the same for different runs, indicating that the seawater samples were being read as high. On the nitrate vs phosphate plot the phosphates were seen to be high, while the nitrates were about normal. The problem seemed to be correlated with ageing of ammonium molybdate stock solution. If fresh ammonium molybdate was used the problem seemed to be reduced. At the end of

the cruise some nutrient trial samples were run. The results from these indicated that the phosphate channel was running reasonably well. Affected samples were rerun.

On the silicate channel, a precipitate in the ammonium molybdate reagent was observed a few days after preparation of fresh reagent. Generally the solution was replaced to reduce the risk of particles travelling through the system.

After a pump tube change there was no response from the nitrate channel. This was traced to a faulty blocked Bran and Luebe tube.

On run 7 Faspac crashed. No reliable results were produced for silicates, and only some results from the early part of the run for nitrates and phosphates. The nitrate and phosphate samples were rerun. Silicate, which does not store well, was calculated by hand from the chart. To verify that the hand and Faspac methods of calculation produced similar results, some of the usable nitrate results from Faspac were compared to hand calculated ones, with an average difference of around 0.6% (hand calculations larger).

## **Tops**

'Tops' are used as a check of changes in instrument responsiveness during a run. They are the same concentration as the top standard, but are made separately. They are placed at the start of a run and after every block of 12 samples.

The tops macro within A9604.XLM was used to extract tops from each \*.XLS run file, calculate statistics, and collate these statistics. The rsd % and range % for the nitrate + nitrite, silicate, and phosphate channels are shown in Figure A2.1.3.

The nitrate and phosphate channels had average ranges of 2.7% and 1.8% respectively. Variations in silicate were greater, with an average range of 4.2%. The silicates had about 20 runs with tops ranges greater than 5%. These 20 were examined, and some had obvious outliers, some appeared random, and about 7 had a time dependent drift. Examples of the worst cases of tops variations for the three channels are shown in Figure A2.1.4.

In general, correcting for tops variations could affect results by up to 1 - 4%. Corrections were not applied though, as the current method of placing tops does not allow for rigorous corrections to be made. The method of correcting for tops variation would have been to assume the first set of tops gives the correct value, and variation later in the run can be referenced to these. However, the first set of tops may not be correct, and false corrections could be made.

A better method would be to use the same solution for the top standard and for tops, and to run reference tops soon after the calibration curve. Thus an absolute concentration could reliably be placed on the tops, and corrections made by comparing tops to the nominal top value. Corrections would only be made once the error in the tops exceeded some set amount. This is because applying a correction between two points is likely to introduce a new source of error.

To get an idea of the sources of error, the error in the calibration curve was looked at for two randomly selected runs, 4 and 60. A total of four calibrations were looked at for nitrate + nitrite and phosphate. Second order calculations for silicate were not looked at. Of these four curves, for nitrate and phosphate, the maximum standard error of the slope was 0.6%, and the maximum standard error of the intercept was 1.9%. It was decided not to calculate the calibration errors for every run, thus they are not included in the total error of the samples for this cruise.

#### Quality checks

Batches of 30-40 deep seawater samples were taken to be used as quality checks to give an indication of instrument responsiveness between runs (Figure A2.1.5). Some were run fresh and the

others stored frozen (Table A2.1.2). Once the value of a batch was established it could be used to see if a run and its calibration appeared normal. The QC macro in A9604.XLM was used to sort through the run \*.XLS files and extract the QC's. The QC names were prefixed by an 's'. As different batches were used this method could not effectively be used to compare runs throughout the cruise. Values could be normalised to the batch averages, but this is not likely to be reliable. Later cruises have used larger batches (~500 10ml tubes) of surface seawater.

## Nutrient data handling

The files produced by Faspac are \*.ACF. These contain the traces for all channels, settings information, calibration curves, and calculated concentrations. The original Faspac files were backed up as \*.NEW. This was important, as occasionally when Faspac crashed the previously saved copy of the file could not be worked on as it would soon crash, so it was necessary to start from original data.

Faspac produced a 'report', a spreadsheet format of nutrient concentrations. It is supposed to produce a format that can be read directly by Excel, however this format caused Excel to crash. The text format could not easily be parsed by Excel. Eventually, data was output as Lotus \*.WKS format, imported by Excel, and a macro used to convert the Lotus format to Excel format. Thus for every run there is an \*.ACF file, and a corresponding \*.XLS file containing the run sequence with concentrations calculated by Faspac.

The "Hydro" program was changed to process Faspac runs by reading \*.FAS files, extracting the sample number and concentration information, and calling the processed file \*.ACM. The information is stored in \*.DAT files, along with other data. Thus any \*.XLS files to be processed need to be copied as \*.FAS files. If only one station in a run is required for processing, then the data needs to be cut and pasted from the \*.XLS file into the \*.ACM file.

Which runs a particular station was run on is shown in Table A2.1.3. This also summarises the reason a station was repeated, and if the original or repeat run was used in the final data.

An attempt was made to observe the nutrient content of the saline solution in which standards were made up in. This was done only for the phosphate channel as it has the highest gain. A rise in the baseline was observed when switching from phosphate 'background' solution to phosphate 'colour' solution. This was attributed to phosphate in the saline solution from impurities in the original solid salt, although more work is needed to confirm it is due only to this, and not due to other contributions such as refractive index change. The value was around 0.006 µM. This value was assigned to the 'blank' in the calibration curve. It made very little impact on the final concentrations.

## A2.1.2 DISSOLVED OXYGEN

The dissolved oxygen (D.O.) titration instrument was fairly reliable and determinations were generally within World Ocean Circulation Experiment (WOCE) guidelines. Exceptions are given below. Standardisations of sodium thiosulfate solution were within WOCE guidelines but improvements could be made by the addition of a second Dosimat unit. Blanks were not measured within WOCE guidelines.

#### Standardisations

The object of the standardisation procedure is to obtain "4 successive titres concordant to within 0.003 mL (of thiosulfate)." This was always achieved but was hampered by continual changing of the Dosimat exchange units. Often 7 or 8 titrations were required. This was time consuming and frustrating. Variations in the sodium thiosulphate titre were often due to bubble formation in the tubing of the exchange units. These are formed by the movement of the burette syringe on removal and replacement of the unit. A second Dosimat would make the standardisation simpler and faster. One

unit would be used for the preparation of the standard solution while a titration was carried out on the second unit. Other advantages include:

- \* elimination of the need to continually exchange units reducing wear on the units, reducing the chance of dropping the unit in rough seas and preventing the formation of bubbles in the tubing;
- \* method may still be used on the cruise if one unit breaks down;
- \* stirring rate would remain the same for each titration (currently, the rate must be changed between preparation of the standard solution and the titration).

Potassium biiodate was added to the standard solution with the dV/dt knob set to 7.5. The rate is not specified in the current instruction manual. The rate could be set in the "DODO" software.

#### Blank Determinations

After concordant standardisation titres were obtained 5 blank determinations were made. These were not within WOCE guidelines. The blanks varied by 0.007 mL (of thiosulfate) for any set of 5 titrations. If 50 mL of water was used for the blank determination the titration did not work. This was increased to 60 mL and the titrations were successful. The measured variation in the blanks leads to an approximate error of 0.1% in the final results.

#### Samples

D.O. measurements in the samples were straightforward. Two or three repeats were measured for each crate of D.O. samples. The titre of the second determination was generally 0.003 - 0.006 mL (of thiosulfate) lower than the first. The greater the titre the greater the loss of volatile iodine.

After the addition of 1 mL of sulfuric acid to the sample the bottle required about 1 minute of shaking.

## Instrumentation

The Dosimat seized up on two occasions. The first happened during the addition of 15 ml of potassium biiodate to the standard solution. This was a "time-out" error as the Dosimat was delivering the solution while the computer was trying to communicate with it. This was fixed by increasing the time the computer allowed for the addition from 20 to 40 seconds and by setting dV/Dt to 7.5. The second time the Dosimat seized up was when it was switched on when the computer was switched on. If the Dosimat was switched on after the "DODO" program was started this was not a problem.

The hydraulic ram was not used. It was more convenient to hold the sample bottles so the pipette tip was just off the bottom.

Standardisations are shown in Figure A2.1.6.

## A2.1.3 LABORATORIES

A number of work spaces were used. Nutrient and salinity analyses were performed in lab 3. The autoanalyser was set up on the forward bench, while the salinometer was set up on the outboard bench near the fume cupboard. Dissolved oxygen analysis and water purification took place in the photolab.

## A2.1.4 TEMPERATURE MONITORING AND CONTROL

Laboratory temperature was recorded by two Tinytalk units, and measured by two mercury thermometers, an electronic thermometer, and the temperature monitor of the PID controller. An 'indoor/outdoor' electronic thermometer was used to measure fridge and freezer temperatures. One Tinytalk was positioned above the salinity crates for the duration of analysis, the other was moved around for shorter checks. One mercury thermometer was positioned above the salinity crates, the other with the DO instrumentation. An electronic thermometer was also used for spot checks. All the temperature measuring devices were placed together at the start of the cruise. The PID temperature was calibrated, and the devices agreed to within 0.5°C.

The long term Tinytalk recorded 1800 temperature points at 48 minute intervals. The file is A9604L.DTF, and the numbers have been exported to A9604L.XLS. The average temperature was 19.6 +/- 0.4 °C. See Figure A2.1.2 and Table A2.1.1. Spatial variations in laboratory temperatures were observed. Among the instrument locations in the nutrient/salinity lab, from bench top to about one metre above the bench, the temperature had a range of 3-4°C.

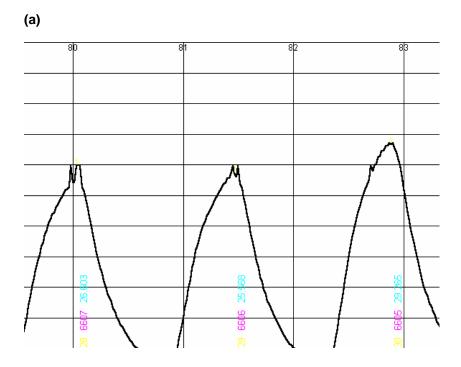
<u>Table A2.1.1:</u> Laboratory temperature recorder statistics.

Temperature Tinytalk	statistics	from
average	19.6 °C	
stdev	0.4 °C	
%rsd	1.9	
min	18.5 °C	
max	20.7 °C	
range	2.2 °C	
% range	11.3	

### Temperature control

Temperature in the nutrient/salinity laboratory was controlled with the ship's air conditioning and with a heating device. The lab was cooled with 16°C air from the ships air conditioning, with the lab reheaters turned off. Heating was provided by a 'Cal control 9900' proportional, integral, and derivative (PID) controller/sensor controlling two simple fan heaters. The sensor was placed near the salinometer, at the height of the top of the salinometer. The setpoint was 19.6°C.

There was no temperature control in the dissolved oxygen lab besides the ship's air conditioning.



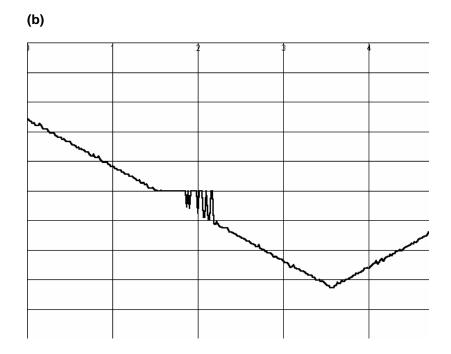
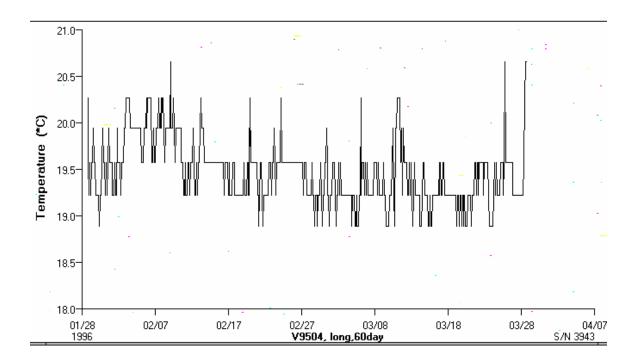
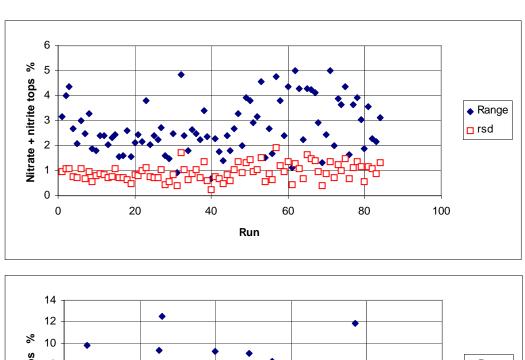
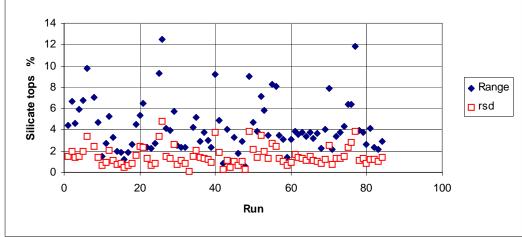


Figure A2.1.1a and b: 'Glitch' in nutrient A/D board: (a) real data, and (b) ramped voltage.



<u>Figure A2.1.2:</u> 'Tinytalk' temperature plot, 28/01/96 to 28/03/96, 48 minute time resolution; logger in film canister punctured to allow air flow, and positioned on middle of bottom shelf opposite fume cupboard in nutrient/salinity lab (lab 3).





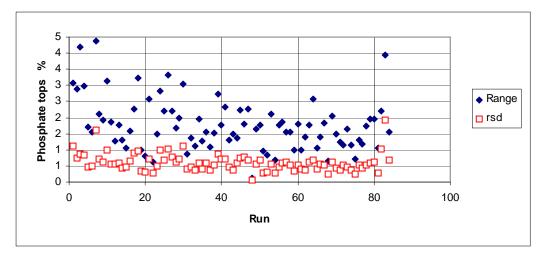


Figure A2.1.3: Statistics for tops used in nutrient analyses.

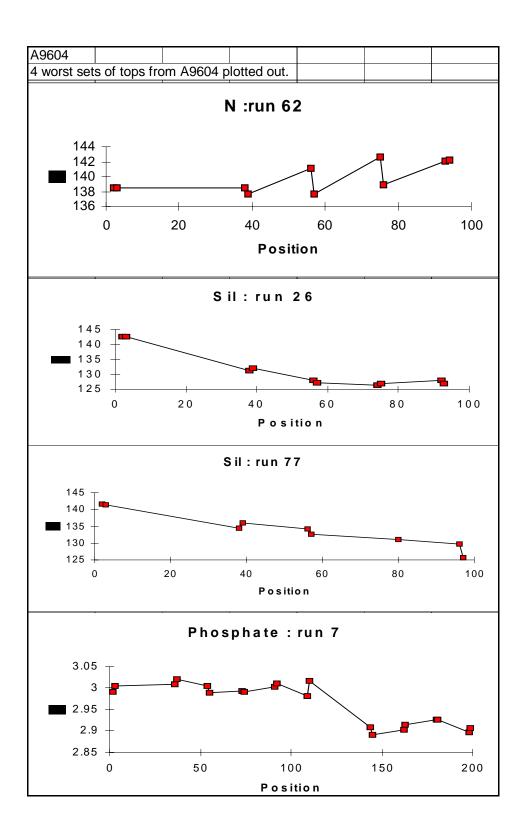


Figure A2.1.4: Worst cases of tops variations for the 3 nutrient channels.

<u>Table A2.1.2:</u> Nutrient samples run as quality checks.

Output from QC.XLS, with							
loop OC magra in A0604	n labels I.XLM to extract QC's (with	a profix in name)					
racio in A9604		ı ə prenx in name)			1		<del>                                     </del>
ïle	Run	Cup	QC name	QC batch	N	S	Р
			4.0		uM	uM	uM
9604017.XLS	17	5	s6101	61	32.3	118.1	2.
9604018.XLS	18		S6101	61	32.1	121.1	2
9604019.XLS	19	5	s6101	61	32.3	118.8	2
9604020.XLS	20	5	S6101	61	32.7	118.5	2
9604021.XLS	21		s6101	61	32.2	99.3	2
9604022.XLS	22	5	s6101	61	32.7	117.3	2
9604022.XLS	22	47		61	32.8	115.8	2
9604022.XLS	22		S6101new	61	32.8	50.6	2
9604023.XLS	23		s6101	61	32.6	119.7	2
9604024.XLS	24		s6101fridge	61	32.8	120.1	2
9604024.XLS	24		s6101freezer	61	32.7	96.6	2
9604025.XLS	25		S6101	61	32.8	79.1	2
9604026.XLS	26		S6101	61	33.3	113.4	2
9604027.XLS 9604027.XLS	27		s6101 s6101	61 61	32.5 32.5	108.2 114.0	2
9604028.XLS	27		s7102fresh	71	32.8	117.5	2
.9604029.XLS	28		s710211es11	71	33.0	115.8	2
9604030.XLS	29		s7102	71	32.7	121.5	2
9604030.XLS	30		s7102	71	32.7	116.4	2
9604030.XLS	30		s7102	71	33.1	112.6	2
9604030.XLS	30	97		71	33.1	118.4	2
9604030.XLS	30		s7102	71	33.2	118.2	
9604031.XLS	30		s7102	71	33.3	119.4	
9604032.XLS	31		s7102	71	32.4	117.6	2
9604033.XLS	32		s7102	71	32.7	117.8	2
9604034.XLS	33		s7102	71	33.3	117.3	2
9604034.XLS	34		s7102	71	32.7	110.5	2
9604035.XLS	35		s7102_fg thaw	71	32.1	87.3	2
9604036.XLS	36		s7102 fridge thaw	71	32.9	109.5	2
9604037.XLS	37		s7102 frdg thaw	71	32.6	115.3	2
9604038.XLS	38		s7102	71	33.1	115.0	2
9604039.XLS	39		s7102	71	33.0	106.5	
9604040.XLS	40		s7102	71	32.7	113.7	2
9604041.XLS	41		s7102	71	32.0	116.2	2
9604042.XLS	42		s7102	71	33.0	116.8	2
9604043.XLS	43		s7102	71 71	32.8	116.6	2
9604044.XLS 9604044.XLS	44		s7102 air24h s7102 frid	71	32.4 32.7	119.2 116.9	2
9604045.XLS	45		s7102 iiid	71	32.4	115.7	2
19604045.XLS	45		s7102	71	32.4	116.0	2
9604047.XLS	47		s7102	71	32.8	118.5	2
9604048.XLS	48		s7102 fdg,days	71	32.2	114.4	2
9604048.XLS	49		s7102 air	71	33.4	127.5	2
9604049.XLS	50		s7102,frd	71	32.6	100.5	2
9604049.XLS	51		s7102	71	32.8	106.8	2
9604049.XLS	48		s11603 fresh,fdg	116	32.7	126.2	:
9604050.XLS	49		s11603	116	32.5	125.2	
9604050.XLS	49	87	s11603 frsh, fdg	116	32.9	136.7	2
9604051.XLS	50	5	s11603,air	116	32.2	121.6	2
9604051.XLS	51	6	s11603	116	33.2	119.3	2
9604051.XLS	51		s11603	116	33.3	125.0	
9604052.XLS	52		s11603	116	32.8		
9604052.XLS	52		s11603	116	32.7	122.7	2
9604053.XLS	53		s11603	116	32.4	96.6	
9604053.XLS	53		s11603	116	33.0	115.5	
9604053.XLS	53		s11603	116	32.3	113.2	
9604054.XLS	54		s11603	116	33.2	113.9	
9604054.XLS	54		s11603	116	33.1	122.2	
9604055.XLS	55		s11603	116	32.3	124.0	
9604055.XLS 9604055.XLS	55 55		s11603 s11603	116 116	32.2 32.6	118.3 122.3	:
9604055.XLS	55		s11603	116	32.6		
9604056.XLS	56		s11603	116	32.8	110.0 122.6	
9604057.XLS	57		s11603	116	33.0	87.1	
9604058.XLS	58		s11603	116	32.6	129.2	
9604058.XLS	58		s11603	116	33.7	124.4	
9604059.XLS	59		s11603	116	32.0	125.2	
9604059.XLS	60		s11603	116	32.0	124.5	
9604059.XLS	60		s11603	116	32.5	125.1	
9604059.XLS	62		s11603	116	31.5	89.2	2
9604060.XLS	62		s11603	116	32.6	86.3	
	O.	30			5	55.0	

A9604060.XLS	59	5	s13002 fresh	130	31.4	90.7	2.22
A9604060.XLS	59		s13002 fsh	130	31.2	92.7	2.20
A9604060.XLS	59	63	s13002 fsh	130	31.5	92.6	2.20
A9604060.XLS	60		s13002	130	31.4	90.8	2.22
A9604061.XLS	60		s13002	130	31.9	90.8	2.23
A9604061.XLS	60		s13002	130	32.0	90.8	2.20
A9604062.XLS	61		s13002	130	32.8	88.4	2.20
A9604062.XLS	61		s13002	130	32.5	89.9	2.21
A9604062.XLS	62		s13002	130	32.1	90.5	2.25
A9604063.XLS	63		s13002	130	31.8	89.3	2.24
A9604063.XLS	63		s13002	130	32.1	86.4	2.23
A9604064.XLS	64		s13002	130	32.3	85.4	2.24
A9604064.XLS	64		s13002	130	31.7	89.0	2.21
A9604065.XLS	65		s13002	130	33.5	72.5	2.24
A9604066.XLS	66		s13002 s13002 4h	130	32.2	85.4	2.24
			s13002 4ff			89.4	
A9604066.XLS	66			130	31.1		2.24
A9604067.XLS	67		s13002 4h	130	32.6	83.8	2.26
A9604067.XLS	67		s13002	130	32.1	87.7	2.21
A9604067.XLS	67		s13002	130	31.8	88.2	2.22
A9604068.XLS	68		s13002	130	32.3	86.8	2.24
A9604068.XLS	68		s13002	130	32.0	91.3	2.23
A9604069.XLS	69		s13002 R	130	32.2	90.5	2.24
A9604069.XLS	69		s13002 '139'	130	31.8	86.6	2.23
A9604069.XLS	69		s13002 '139'	130	32.1	87.5	2.17
A9604070.XLS	70		s13002	130	31.4	81.8	2.24
A9604070.XLS	70		s13002 4h	130	31.5	85.1	2.22
A9604071.XLS	71	5	s13002	130	31.2	64.2	2.22
A9604071.XLS	71	96	s13002	130	32.0	90.4	2.20
A9604071.XLS	73	5	s13002	130	31.7	86.8	2.28
A9604071.XLS	73	59	s13002	130	31.4	88.4	2.27
A9604071.XLS	71	6	s14102	141	31.7	101.3	2.21
A9604071.XLS	71	97	s14102	141	32.1	101.6	2.22
A9604071.XLS	71	98	s14102	141	32.1	101.1	2.25
A9604073.XLS	71	100	s14102	141	32.6	101.4	2.18
A9604073.XLS	71	101	s14102	141	31.9	100.7	2.21
A9604073.XLS	73	6	s14102	141	32.3	96.2	2.33
A9604073.XLS	73	60	s14102	141	31.7	100.0	2.32
A9604073.XLS	73	97	s14102	141	31.9	101.0	2.28
A9604074.XLS	74		s14102	141	32.4	89.8	2.30
A9604074.XLS	74		s14102	141	32.3	97.3	2.25
A9604075.XLS	75		s14102 2h	141	32.0	84.8	2.45
A9604075.XLS	75		s14102	141	32.8	101.5	2.47
A9604076.XLS	76		s14102 1h	141	32.1	61.5	2.26
A9604076.XLS	76		s14102 1h	141	32.2	100.9	2.28
A9604077.XLS	77		s14102 211	141	33.0	76.3	2.28
A9604077.XLS	77		s14102	141	31.7	87.4	2.31
A9604078.XLS	78		s14102	141	31.9	99.4	2.28
A9604078.XLS	78		s14102	141	32.6	96.9	2.30
A9604078.XLS	78		s14102 s14102	141	32.0	98.2	2.30
A9604079.XLS	79		s14102	141	31.7	88.4	2.23
A9604079.XLS	79			141	32.6	101.6	
			s14102				2.23
A9604080.XLS	80		s14102	141	32.4	63.5	2.24
A9604080.XLS	80		s14102	141	32.7	91.6	2.17
A9604081.XLS	81		s14102	141	32.3	93.9	2.24
A9604081.XLS	81 82		s14102 s14102	141	32.5 30.1	97.4 96.7	2.21 2.26
A9604082.XLS							

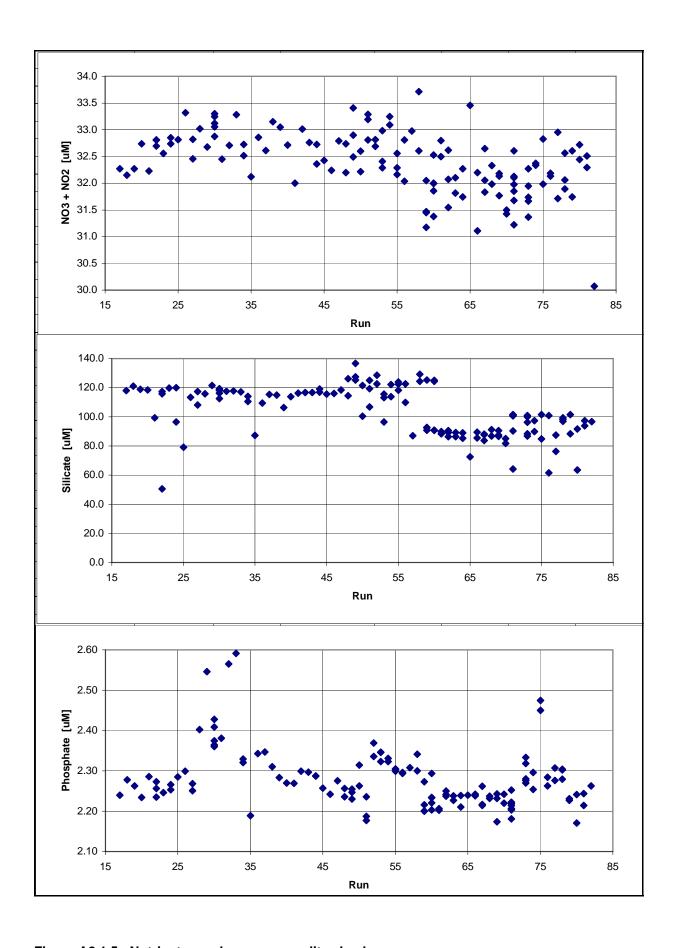


Figure A2.1.5: Nutrient samples run as quality checks.

<u>Table A2.1.3:</u> Nutrient analysis run numbers on which stations were run.

A0604				1	1					1	1
A9604 nuts											
run vs stn Shows proble	ms					-	<b> </b>			1	1
Silows proble	1115										
Stn	Run	Run	Probs	Stn	Run	Run	Probs	Stn	Run	Run	Probs
	first	repeat	11003	Otti	first	repeat	11003	Otti	first	repeat	11003
	iliot	repeat			mot	гереас			mat	repeat	
1	ns			61	23			120	55		
	ns			62	17			121	52		
3	1		Ph	63	18			122	56		
	ns			64	24			123	57		
	ns				ns			124	54		
6	2			66	24			125	56		
7	2			67	28	82	Ph	126	60		
8	2			68	28		Ph	127	60		
9	2			69	28	77	Ph	128	59		
10	2			70	28	77	Ph	129	60		
11	2			71	27			130	59		
12	3	61	Ph	72	27			131	60		
13	3	62	Ph	73	29	79	Ph	132	60		
14	3		Ph	74	31		Ph	133	63		
15	3		Ph	75	30		Ph	134	64		
16	ns			76	30		Ph	135	65		
17	4	64	Ph	77	ns			136			
18	4		Ph	78	34	81	Ph	137	67		
19	4	67	Ph	79	32		Ph	138	68		
20	4	70	Ph	80	33	58	S Ph	139	69		
21	ns			81	35			140	69		
22	5	70	P?	82	34			141	71		
23	7	25	Sx Ph	83	35			142	73		
24	7	25	Sx Ph	84	37			143	72		
25	7	26	Sx Ph	85	37			144	74		
26	7	26	Sx Ph	86	39			145	75	81	Ph
27	8	71	Ph N	87	39			146	ns		
28	8	75	Ph	88	36			147	ns		
29	ns			89	37						
30	9	73	Ph N	90	41			N	Nitrate + nit	trite	
31	9	74	Ph N	91	43	58	S	S	Silicate		
32	5			92	38			Р	Phosphate	ā.	
33	11	81	Ph N	93	39			h	high		
34	12	78	Ph	94	43			X	Lost data		
35	6			95				ns	No sample		
36	14			96	40			Bold	indicates ch		
37	6			97	41				of repeated		
38	6			98	43				station used	d in final data.	
39	18			99	42						
40	18			100	45						
41	19			101	47						
42	7	29	Sx Ph	102	47						
43				103	48						
44	19			104	48						
45	20			105	49						
46	21			106	49						
47	21	77	Di	107	49					-	
48	10	77	Ph	108	50		-			-	
49	11		Ph	109	51		-			-	
50	11		Ph N	110						-	
51	11		Ph N	111	45					-	
52	12	79	Ph	112			-			-	
53	22			113							
54	13			114			-			-	
55	13			115			-			-	
56	14			116							
57	23			117							
58	15			118							
59	16			119	ris						-
60	115				l	l	<u> </u>			l	l

		. ml of thios	ulfate titrate	ed against b	iiodate.				
values co	pied from lo	y sileets.							
Cruise	Number	Sheet	Stn	Std	Blank	Date	Biiodate ba	atch	
			1st stn app						
49604	1		3	4.334		22-Jan-96			
A9604	2		6	4.438	0.0063	30-Jan-96			
A9604	3		13	4.436		1-Feb-96			
49604 49604	5		19 26	4.439 4.435	0.0053 0.0068	3-Feb-96 7-Feb-96			
49604 49604	6		34	4.433	0.0068	9-Feb-96			
49604 49604	7		40	4.431	0.0060	10-Feb-96			
49604	8		44	4.432	-0.0058	12-Feb-96			
A9604	9		47	4.434		13-Feb-96			
A9604	10		54	4.431	-0.0067	15-Feb-96			
A9604	11	53	62	4.428		17-Feb-96			
49604	12	56	66	4.437	0.0022	24-Feb-96			
49604	13	65	75	4.435	0.0050	26-Feb-96			
A9604	14		82	4.433		29-Feb-96			
49604	15		93	4.440	0.0044	2-Mar-96			
A9604	16		98	4.437	0.0040	4-Mar-96			
A9604	17		104	4.436					
A9604	18		111	4.428	0.0042	7-Mar-96			
A9604	19		117	4.427	0.0078	13-Mar-96			
A9604	20		124	4.423	0.0028	15-Mar-96	hali far	ht 110	
49604 49604	21		128 133	4.424 4.424		17-Mar-96 20-Mar-96	bnk from s	nt 110	
49604 49604	23		133	4.424	0.0053		bnk from sl	ht 110	
49604 49604	24		145	4.423		24-Mar-96	DIIK HOIH S	11119	
49601	25		143	4.357	0.0050		sqb 18-8-9	6 no1	
49601	26		4	4.366		28-Aug-96		01101	
A9601	27		5			31-Aug-96			
A9601	28		7	4.374		1-Sep-96			
A9601	29		13	4.382				18-8-96 no1	
A9601	30		18	4.384				18-8-96 no2	
A9601	31	26	20	4.370	-0.0010	7-Sep-96	top up sgb	18-8-96 no2	
A9601	32	32	25	4.373	0.0050	8-Sep-96	new Nal/Na	aOH dispensor	
49601	33	38	31	4.367	0.0020	10-Sep-96			
A9601	34	44	36	4.370	0.0030	11-Sep-96			
A9601	35		41	4.402		13-Sep-96	top up sgb	no 3	
A9601	36		47	4.416		15-Sep-96			
A9601	37		53	4.411		17-Sep-96			
A9601	38		59	4.418		20-Sep-96			
A9601	39	76	66	4.432	-0.0010	22-Sep-96			
4.44									
4.44 - 4.42 -		• • • • •	***	••	• •		•		
Thiosulfate m - 98.4									
4.38 -					4.4	• • • •			
.9 4.36 -					♦ Å9601				
<b>-</b> 4.34 -	◆ A9604								
4.32 -					-	-			
C	5	10	15	20	25	30 3	5 40		
				Number				<u> </u>	
0.01	ı <del>,</del>		T		1 1		$\neg$		
0.000		••	. •	•	•				
<b>E</b> 0.005		<b>-</b>	* ***	• • • • • • • • • • • • • • • • • • • •	•	***			
Blank ml	-			<u> </u>	•	* * * * * * * * * * * * * * * * * * * *			
<u>-0.005</u>	5								
	· [	* * <b>.</b> *			1				
0.000	. —	<del></del>	<del> </del>	_			→		_
-0.00	0 5	10	15	20 :	25 30	35	40		_

Figure A2.1.6: Dissolved oxygen standardisations.

85

## Part 3

# Aurora Australis Marine Science Cruise AU9601 - Oceanographic Field Measurements and Analysis

#### **ABSTRACT**

Oceanographic measurements were conducted along WOCE Southern Ocean meridional section SR3 between Tasmania and Antarctica from August to September 1996. A total of 71 CTD vertical profile stations were taken, most to near bottom. Over 1500 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients, dissolved inorganic carbon, alkalinity, carbon isotopes, primary productivity, and biological parameters, using a 24 bottle rosette sampler. Near surface current data were collected using a ship mounted ADCP. Measurement and data processing techniques are summarised, and a summary of the data is presented in graphical and tabular form.

#### 3.1 INTRODUCTION

Marine science cruise AU9601, the sixth oceanographic cruise of the Cooperative Research Centre for the Antarctic and Southern Ocean Environment (Antarctic CRC), was conducted aboard the RSV Aurora Australis from August to September 1996. The major constituent of the cruise was the collection of oceanographic data relevant to the Australian Southern Ocean WOCE Hydrographic Program, along WOCE section SR3 (Figure 3.1). This was the seventh occupation of section SR3 (and the last by the Aurora Australis under the WOCE program), and the second during a southern winter. Previous occupations of SR3 are summarised in Part 1 of this report. A further occupation of the northern half of SR3 took place in March to April of 1997 by the SCRIPPS ship R.V. Melville (principal investigators R.Watts, S. Rintoul, J. Richman, B. Petit, D. Luther, J. Filloux, J. Church, A. Chave).

This report describes the collection of oceanographic data from the SR3 section, and summarises the chemical analysis and data processing methods employed. All information required for use of the data set is presented in tabular and graphical form.

## 3.2 CRUISE ITINERARY

En route to Macquarie Island at the start of the cruise, the ship steamed in a straight line over the Tasmanian continental shelf for calibration tests of the ADCP. Three test CTD casts were also taken en route. Following cargo operations at Macquarie Island, the ship steamed southwest towards the southern end of the SR3 transect, taking a deep and a shallow test CTD cast on the way. A full day was spent penetrating southward into the ice before commencing the SR3 transect at the Antarctic shelf break east of Dumont D'Urville (Figure 3.1). The transect was then completed on the northward journey back to Hobart. Station spacing was decreased in the region of the Subantarctic Front, with casts taken over a series of inverted echo sounder and current meter moorings. The transect proper was interrupted briefly here for completion of several CTD casts over the eastern group of moorings in the larger mooring array (Figure 3.1) (Table 3.4). Further north, the SR3 station at latitude ~47.15°S was shifted ~5 nautical miles west of the transect line to avoid the pronounced steep bathymetry encountered at this latitude on previous cruises. Following completion of the SR3 transect, two further casts were taken to test another CTD before returning to Hobart.

## 3.3 CRUISE SUMMARY

In the course of the cruise, 71 CTD casts were completed along the SR3 section (Figure 3.1) (Table 3.2), plus additional test locations, with most casts reaching to within 20 m of the sea floor (Table 3.2). Over 1500 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients (orthophosphate, nitrate plus nitrite, and reactive silicate), dissolved inorganic carbon, alkalinity, carbon isotopes (<sup>14</sup>C and <sup>13</sup>C), primary productivity, and biological parameters, using a 24 bottle rosette sampler. Table 3.3 summarises samples drawn at each station. For all stations, the different samples were drawn in a fixed sequence (see previous data reports). Casts taken over mooring locations are summarised in Table 3.4. Principal investigators for the various water sampling programmes and cruise participants are listed in Tables 3.5a and b.

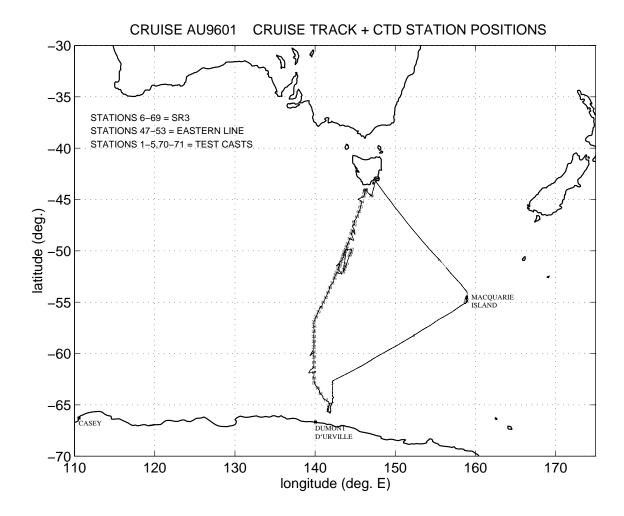


Figure 3.1: Cruise track and CTD station positions for RSV Aurora Australis cruise AU9601.

## Table 3.1: Summary of cruise itinerary.

Expedition Designation
Cruise AU9601 (cruise acronym WASTE), encompassing WOCE section SR3

Chief Scientist Steve Rintoul, CSIRO

Ship RSV Aurora Australis

Ports of Call Macquarie Island

Cruise Dates
August 22 to September 22 1996

Table 3.2 (following 2 pages): Summary of station information for RSV Aurora Australis cruise AU9601. The information shown includes time, date, position and ocean depth for the start of the cast, at the bottom of the cast, and for the end of the cast. The maximum pressure reached for each cast, and the altimeter reading at the bottom of each cast (i.e. elevation above the sea bed) are also included. Missing ocean depth values are due to noise from the ship's bow thrusters interfering with the echo sounder. For casts which do not reach to within 100 m of the bed (i.e. the altimeter range), or for which the altimeter was not functioning, there is no altimeter value. For station names, TEST is a test cast and EL is the eastern line (the meridional section over the eastern part of the mooring array). Note that all times are UTC (i.e. GMT). CTD unit 7 (serial no. 1103) was used for stations 4 to 69; CTD unit 5 (serial no. 1193) was used for stations 1 to 2 and 70 to 71; CTD unit 6 (serial no. 2568) was used for station 3.

station		STA	RT		maxP		В	ОТТС	M				EN	D	
number	time date	latitude	longitude	depth(m)	(dbar)	time	latitude		ngitude d	epth(m)	altimeter	time	latitude	longitude	depth(m)
			<u></u>		( /				<b>J</b>	-1 - ( /				<u> </u>	
1 TEST	0715 24-AUG-96 5	50:48.64S	155:26.04E	4597	1026	0757	50:49.31	1S 15	5:27.15E	4604	_	0829	50:49.72S	155:27.89E	4589
2 TEST	0903 25-AUG-96 5	54:47.52S	159:02.91E	4607	154	0912	54:47.62	2S 159	9:03.13E	-	_	0917	54:47.67S	159:03.19E	4607
3 TEST	1048 25-AUG-96 5	54:56.43S	158:56.37E	3071	840	1137	54:56.48	8S 158	8:57.54E	-	_	1156	54:56.43S	158:57.67E	_
4 TEST	0536 27-AUG-96 5	58:14.95S	152:18.29E	2355	2564	0702	58:15.12	2S 152	2:17.62E	-	30.1	0814	58:15.03S	152:17.35E	_
5 TEST	0230 29-AUG-96 6	32:50.62S	142:10.90E	3993	344	0252	62:50.62	2S 142	2:11.17E	-	_	0304	62:50.67S	142:11.37E	_
6 SR3	0726 30-AUG-96 6	65:44.59S	141:51.94E	761	764	0812	65:44.37	7S 14	1:51.07E	773	8.7	0904	65:44.04S	141:50.28E	768
7 SR3	0554 31-AUG-96 6	55:34.50S	141:34.66E	1019	970	0636	65:34.30	OS 14	1:34.24E	973	7.5	0727	65:34.09S	141:33.73E	951
8 SR3	0922 31-AUG-96 6	55:30.25S	141:35.62E	1491	1486	1017	65:30.10	OS 14	1:35.08E	1505	9.4	1114	65:29.89S	141:34.48E	1494
9 SR3	1252 31-AUG-96 6	55:25.68S	141:37.33E	2125	2100	1402	65:25.45	5S 14°	1:36.58E	2099	8.8	1521	65:25.15S	141:35.43E	2077
10 SR3	1844 31-AUG-96 6	55:10.53S	141:41.76E	2594	2544	2001	65:10.37	7S 141	1:40.14E	2529	10.3	2115	65:10.20S	141:38.34E	2551
11 SR3	0106 1-SEP-96 6			2965	2950	0241	64:52.77	7S 141	1:48.58E	-	10.0	0414	64:52.54S	141:45.55E	2920
12 SR3	0949 1-SEP-96 6	64:30.67S	141:20.56E	3506	3518	1136	64:30.10	OS 141	1:16.15E	3481	4.6	1329	64:29.44S	141:11.59E	
13 SR3	2219 1-SEP-96 6	3:53.74S	140:39.16E	3716	3746	2356	63:52.72	2S 140	0:38.22E	3732	11.6	0127	63:51.87S	140:38.40E	3726
14 SR3	0622 2-SEP-96 6	3:22.44S	140:18.76E	3801	3836	0757	63:21.22	2S 140	0:21.04E	3801	13.1	0944	63:20.08S	140:22.33E	3801
15 SR3	1442 2-SEP-96 6	32:51.01S	139:52.91E	3225	3262	1613	62:50.88	BS 139	9:53.65E	3246	11.7	1729	62:50.76S	139:54.28E	3251
16 SR3	2115 2-SEP-96 6	32:21.73S	139:50.56E	3952	3988	2254	62:21.45	5S 139	9:49.95E	-	9.9	0032	62:21.81S	139:49.38E	3963
17 SR3	0403 3-SEP-96 6	31:50.89S	139:51.19E	4300	4344	0543	61:51.33	3S 139	9:50.61E	-	11.0	0731	61:52.07S	139:50.25E	-
18 SR3	2101 3-SEP-96 6			4336	4392		-		9:49.39E	-	15.5			139:49.42E	
19 SR3	0348 4-SEP-96 6			4392	4460				9:49.81E	-	3.6			139:49.78E	
20 SR3	0956 4-SEP-96 6			4443	4488	_			9:51.04E	-	18.0			139:51.30E	
21 SR3	1847 4-SEP-96 5				4534				9:51.84E	-	15.3			139:52.74E	
22 SR3	1547 5-SEP-96 5			4146	4174				9:51.21E	-	15.3			139:51.51E	
23 SR3	2254 5-SEP-96 5			3911	3962				9:50.50E	-	15.4			139:51.24E	
24 SR3	1247 6-SEP-96 5			3942	4084				9:51.25E	-	18.8			139:50.38E	
25 SR3	1901 6-SEP-96 5			4090	4168				9:51.69E	-	15.3			139:52.12E	
26 SR3	0714 7-SEP-96 5			4100	4212		-		9:52.35E	-	16.9	_		139:51.26E	
27 SR3	1328 7-SEP-96 5			4100	4272	_			9:52.32E	-	19.5	_		139:52.98E	
28 SR3	2324 7-SEP-96 5			3910	3950				0:07.06E	-	15.3			140:07.39E	
29 SR3	0602 8-SEP-96 5			3730	3640				0:25.27E	-	16.5			140:25.78E	
30 SR3	1738 8-SEP-96 5			3890	3900			_	0:44.95E	-	16.1			140:45.64E	
31 SR3	0004 9-SEP-96 5			3225	3238				1:01.78E	-	12.4			141:01.88E	
32 SR3	0603 9-SEP-96 5			2815	2896				1:19.04E	-	14.5			141:19.33E	
33 SR3	1207 9-SEP-96 5			2559	2666			_	1:36.06E	-	16.9	_		141:36.90E	
34 SR3	1736 9-SEP-96 5			2503	2672				1:49.77E	-	18.3			141:48.66E	
35 SR3	2308 9-SEP-96 5				3244				2:10.83E	-	23.5			142:12.03E	
36 SR3	0510 10-SEP-96 5	2:40.03S	142:23.22E	3378	3396	0641	52:40.15	5S 142	2:24.16E	-	16.8	0807	52:40.16S	142:24.31E	-

station	START	maxP	BOTTOM	END
number	time date latitude longitude depth(m)	(dbar)	time latitude longitude depth(m) altimeter	time latitude longitude depth(m)
	<u> </u>		<b>5</b> 1 ( )	
37 SR3	1010 10-SEP-96 52:21.93S 142:31.92E 3481	3608	1146 52:21.93S 142:32.61E - 20.4	1308 52:22.36\$ 142:33.11E -
38 SR3	1521 10-SEP-96 52:04.98S 142:42.34E 3481	3544	1652 52:05.62S 142:42.69E - 15.2	1814 52:05.89S 142:43.00E -
39 SR3	0344 11-SEP-96 51:48.52S 142:50.68E 3686	3782	0530 51:48.49S 142:50.71E - 16.0	0655 51:48.60S 142:51.04E -
40 SR3	0843 11-SEP-96 51:32.14S 142:59.19E 3686	3834	1035 51:32.07S 142:59.26E - 18.8	1214 51:32.16S 142:59.35E -
41 SR3	1422 11-SEP-96 51:15.70S 143:07.74E 3737	3832	1548 51:15.76S 143:07.71E - 16.2	1713 51:15.76S 143:07.93E -
42 SR3	0348 12-SEP-96 51:00.49S 143:16.03E 3870	3884	0517 50:59.68S 143:16.84E - 18.1	0643 50:58.99S 143:17.54E -
43 SR3	0904 12-SEP-96 50:40.89S 143:25.14E 3583	3556	1048 50:40.16S 143:29.77E - 16.7	1219 50:39.58\$ 143:32.34E -
44 SR3	2111 12-SEP-96 50:23.87S 143:32.09E 3580	3580	2258 50:23.71S 143:33.09E - 16.5	0022 50:23.82\$ 143:33.30E -
45 SR3	0253 13-SEP-96 50:09.63S 143:40.07E 3563	3740	0436 50:09.18S 143:40.57E - 17.9	0602 50:08.77S 143:40.54E -
46 SR3	0827 13-SEP-96 49:53.17S 143:48.27E 3768	3788	1010 49:53.08S 143:48.40E - 23.1	1130 49:52.99S 143:47.92E -
47 EL	1443 13-SEP-96 49:53.16S 144:33.90E 3768	3888	1610 49:53.13S 144:34.54E - 18.5	1735 49:53.32S 144:34.66E -
48 EL	2037 13-SEP-96 50:08.79S 144:27.34E 3730	3884	2233 50:08.76S 144:27.33E - 15.9	0002 50:08.72S 144:27.38E -
49 EL	0344 14-SEP-96 50:26.09S 144:17.95E 3420	3198	0515 50:25.96S 144:18.28E - 13.0	0633 50:25.56S 144:19.02E -
50 EL	1400 14-SEP-96 51:15.87S 143:54.24E 3737	3794	1532 51:15.82S 143:54.22E - 17.2	1654 51:15.81S 143:54.34E -
51 EL	1855 14-SEP-96 51:32.25S 143:46.65E 3686	3780	2040 51:32.29S 143:46.60E - 17.9	2211 51:32.25S 143:46.75E -
52 EL	0028 15-SEP-96 51:48.85S 143:37.95E 3481	3646	0159 51:48.82S 143:37.89E - 5.8	0319 51:48.84S 143:38.16E -
53 EL	0552 15-SEP-96 52:05.55S 143:29.43E 3532	3564	0726 52:05.52S 143:29.52E - 16.9	0847 52:05.38\$ 143:29.52E -
54 SR3	0507 16-SEP-96 49:36.47S 143:55.95E 3665	3730	0645 49:36.56S 143:55.93E - 18.9	0808 49:36.61S 143:56.02E -
55 SR3	1046 16-SEP-96 49:16.03S 144:06.03E 4382	4422	1256 49:16.99S 144:05.71E - 18.5	1430 49:17.44S 144:06.22E -
56 SR3	1822 16-SEP-96 48:47.05S 144:18.94E 4180	4148	1959 48:48.15S 144:19.39E - 15.0	2126 48:48.75S 144:19.74E -
57 SR3	0829 17-SEP-96 48:19.01S 144:32.00E 4000	4126	1001 48:19.79S 144:32.23E - 15.1	1143 48:20.58\$ 144:32.43E -
58 SR3	1414 17-SEP-96 47:59.94S 144:40.33E 4116	4412	1621 47:59.79S 144:40.25E - 17.3	1750 47:59.94S 144:40.45E -
59 SR3	1058 18-SEP-96 47:28.12S 144:53.80E 4440	4384	1302 47:28.05S 144:52.12E - 25.6	1438 47:28.18S 144:50.88E -
60 SR3	1704 18-SEP-96 47:09.25S 144:54.19E 4790	4882	1904 47:09.67S 144:53.08E - 20.8	2053 47:09.91S 144:52.51E -
61 SR3	0034 19-SEP-96 46:39.04S 145:15.19E 3378	3434	0219 46:39.61S 145:15.01E - 21.1	0341 46:39.75S 145:14.89E -
62 SR3	0701 19-SEP-96 46:10.00S 145:28.15E 2723	2754	1016 46:11.83S 145:28.41E - 14.6	1134 46:12.61S 145:28.57E -
63 SR3	1833 19-SEP-96 45:42.01S 145:39.82E 2017	2098	1945 45:42.55S 145:39.82E - 15.6	2045 45:42.93S 145:39.93E -
64 SR3	2355 19-SEP-96 45:13.02S 145:50.89E 2851	2892	0120 45:12.70S 145:49.78E 2887 14.7	0232 45:12.76S 145:49.69E -
65 SR3	1141 20-SEP-96 44:42.99S 146:03.04E 3195	3222	1323 44:42.73\$ 146:03.82E 3195 17.0	1441 44:42.43S 146:04.75E 3220
66 SR3	1649 20-SEP-96 44:22.99S 146:11.37E 2333	2348	1800 44:23.05\$ 146:11.82E 2333 17.1	1907 44:23.13S 146:11.95E 2333
67 SR3	2106 20-SEP-96 44:07.05S 146:13.33E 1003	1000	2145 44:06.94S 146:13.29E 1003 17.5	2219 44:06.90S 146:13.39E 1003
68 SR3	2312 20-SEP-96 44:03.21S 146:17.21E 522	478	2347 44:03.24S 146:18.09E 481 17.4	0016 44:03.40S 146:18.52E 481
69 SR3	0105 21-SEP-96 44:00.04S 146:19.17E 236	190	0124 44:00.03\$ 146:19.48E 200 12.0	0142 44:00.01S 146:19.83E 179
70 TEST	1004 21-SEP-96 44:39.59S 147:00.22E 2457	318	1014 44:39.59S 147:00.37E	1024 44:39.57S 147:00.47E -
71 TEST	1248 21-SEP-96 44:37.02S 147:00.21E 2559	2564	1415 44:37.13S 147:00.82E - 28.5	1534 44:37.41S 147:00.97E -

<u>Table 3.3:</u> Summary of samples drawn from Niskin bottles at each station, including salinity (sal), dissolved oxygen (do), nutrients (nut), dissolved inorganic carbon (dic), alkalinity (alk), carbon isotopes (Ctope), fluorometry (fl), and pigments (pig); Seacat casts are also listed. Note that 1=samples taken, 0=no samples taken, 2=surface sample only (i.e. from shallowest Niskin bottle or from seawater outlet).

station	sal	do	nut	dic	alk	Ctope	fl	pig	SEACAT
1 2 3	1 0 0	1 0 0	1 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0
4	1	1	1	0	0	0	0	0	1
5 6	1 1	1 1	1 1	0 1	0 1	0 1	0 1	0 1	0 1
7	1	1	1	1	1	2	1	1	1
8	1	1	1	1	1	2	1	1	1
9	1	1	1	1	1	2	0	0	0
10 11	1 1	1 1	1 1	2 1	2	2 1	1	1 1	1 1
12	1	1	1	1	1	2	1	1	1
13	1	1	1	1	1	2	1	1	1
14	1	1	1	1	1	2	1	1	1
15 16	1 1	1 1	1 1	1 1	1 1	1 2	0 1	1 1	1 1
17	1	1	1	1	1	2	1	1	1
18	1	1	1	1	1	1	1	1	0
19	1	1	1	1	2	2	1	1	1
20 21	1 1	1 1	1 1	1 1	1 1	0 1	0 1	1 1	1 1
22	1	1	1	1	1	2	0	1	1
23	1	1	1	1	1	2	1	1	1
24	1	1	1	1	1	1	0	1	1
25	1 1	1 1	1 1	2 1	2 1	2	1 1	1 1	1 1
26 27	1	1	1	1	1	2	0	1	1
28	1	1	1	1	1	2	1	1	1
29	1	1	1	1	1	2	1	1	1
30	1 1	1 1	1 1	1 2	1 2	1 2	0 1	1 1	1 1
31 32	1	1	1	1	1	2	1	1	1
33	1	1	1	2	2	2	0	1	1
34	1	1	1	1	1	1	0	1	1
35	1 1	1 1	1	2 1	2	2 2	1	1	1
36 37	1	1	1 1	1	1	2	1	1 1	1 1
38	1	1	1		2		0	1	1
39	1	1	1	2 1	1	2 1	1	1	1
40	1	1	1	1	1	2 2 2	1	1	1
41 42	1 1	1 1	1 1	1 1	1 1	2	0 1	1 1	1 0
43	1	1	1	1	1	0	1	1	0
44	1	1	1	1	1	0	1	1	0
45	1	1	1	1	1	2	1	1	0
46 47	1 1	1 1	1 1	1 2	1	0 0	1 0	0	0 0
48	1	1	1	2	2	0	0	0	0
49	1	1	1	2 2	2	0	0	0	0
50	1	1	1	2	2	0	0	0	0

Table 3.3: (continued)

station	sal	do	nut	dic	alk	Ctope	fl	pig	SEACAT
51 52	1 1	1 1	1 1	2 2	2	0	0	0 0	0 0
53	1	1	1	2	2	0	0	0	0
54	1	1	1	1	1	0	1	1	1
55	1	1	1	1	1	1	0	1	1
56	1	1	1	2	2	0	0	1	1
57	1	1	1	1	1	2	1	1	1
58	1	1	1	1	1	0	0	1	1
59	1	1	1	1	1	1	0	1	0
60	1	1	1	1	1	0	1	1	0
61	1	1	1	1	1	2	1	1	1
62	1	1	1	1	1	0	1	1	1
63	1	1	1	1	1	0	1	1	1
64	1	1	1	2	2	2	1	1	1
65	1	1	1	1	1	1	0	1	1
66	1	1	1	2	2	0	0	1	1
67	1	1	1	1	1	0	1	1	1
68	1	1	1	0	0	0	1	1	1
69	1	1	1	1	1	0	0	0	0
70	0	0	0	0	0	0	0	0	1
71	1	0	0	0	0	0	0	0	0

<u>Table 3.4:</u> CTD stations over current meter (CM) and inverted echo sounder (IES) moorings along SR3 transect in the vicinity of the Subantarctic Front. Note that bottom depths (at the start of each CTD cast) are calculated using a sound speed of 1498 ms<sup>-1</sup>. For CTD station positions, see Table 3.2.

CTD station no.	start time	bottom depth (m)	mooring number
station no.		deptii (iii)	Humber
38	15:21, 10/09/96	3481	I18 (IES)
39	03:44, 11/09/96	3686	I16 (IES)
40	08:43, 11/09/96	3686	114 (IES)
41	14:22, 11/09/96	3737	I12 (IES)
42	03:48, 12/09/96	3870	I10 (CM+IES)
43	09:04, 12/09/96	3583	I9 (CM+IES)
44	21:11, 12/09/96	3580	I8 (CM+IES)
45	02:53, 13/09/96	3563	16 (IES)
46	08:27, 13/09/96	3768	14 (IES)
47	14:43, 13/09/96	3768	I3 (IES)
48	20:37, 13/09/96	3730	I5 (IES)
49	03:44, 14/09/96	3420	17 (IES)
50	14:00, 14/09/96	3737	I11 (IES)
51	18:55, 14/09/96	3686	113 (IES)
52	00:28, 15/09/96	3481	115 (IES)
53	05:52, 15/09/96	3532	I17 (IES)
54	05:07, 16/09/96	3665	I2 (IES)
58	14:14, 17/09/96	4116	I1 (IES)

<u>Table 3.5a:</u> Principal investigators (\*=cruise participant) for rosette water sampling programmes.

measurement name affiliation

CTD, salinity, O<sub>2</sub>, nutrients \*Steve Rintoul/Nathan Bindoff CSIRO/Antarctic CRC

D.I.C., alkalinity, carbon isotopes \*Bronte Tilbrook CSIRO

fluorometry \*Peter Strutton(PhD student) Flinders University biological sampling Harvey Marchant/\*Simon Wright Antarctic Division

Table 3.5b: Scientific personnel (cruise participants).

name	measurement	affiliation
Muhammad Evri Helen Phillips Steve Rintoul Marie Robert Mark Rosenberg Serguei Sokolov Annie Wong Fadli Syamsudin	CTD CTD CTD CTD CTD CTD CTD CTD CTD	BPPT (Indonesia) Antarctic CRC CSIRO Antarctic CRC Antarctic CRC CSIRO Antarctic CRC BPPT (Indonesia)
Stephen Bray Ana Costalunga Neale Johnston	salinity, oxygen, nutrients oxygen salinity, oxygen, nutrients	Antarctic CRC Antarctic CRC Antarctic CRC
Rebecca Esmay Mark Pretty Bronte Tilbrook Alison Walker	D.I.C., alkalinity, C isotopes D.I.C., alkalinity, C isotopes D.I.C., alkalinity, C isotopes D.I.C., alkalinity, C isotopes	CSIRO CSIRO CSIRO CSIRO
Raechel Waters Simon Wright	biological sampling biological sampling, voyage leader	Antarctic Division Antarctic Division
Simon Evans Robert Geier Stewart Graham Alan Poole Sandra Potter Peter Strutton Andrew Tabor Wojciech Wierzbicki Karen Wilson	programmer programmer doctor electronics deputy voyage leader, fishing underway data, fluorometry gear officer, fishing electronics fishing	Antarctic Division Antarctic Division Antarctic Division CSIRO Antarctic Division Antarctic Division/Flinders University Antarctic Division Antarctic Division Marine Studies Centre (Tasmania)
Steve Oakley	returnee	Antarctic Division

## 3.4 FIELD DATA COLLECTION METHODS

# 3.4.1 CTD and hydrology measurements

CTD and hydrology instrumentation, data collection and processing methods are as described in Part 2 of this report. The hydrology laboratory report for this cruise can be found in Appendix 3.1. Preliminary results of the CTD data calibration, along with data quality information, are presented in Section 3.6. Calibration information for CTD sensors are presented in Table 3.22. Note that no photosynthetically active radiation (p.a.r.) sensor or fluorometer were attached to the rosette package for this cruise. P.a.r. and fluorescence data were collected by a Seabird "Seacat" CTD, which was deployed separately (Table 3.3) (these data are not discussed further in this report).

The following updates apply to the CTD data processing and hydrology analytical techniques:

- (i) in the conductivity calibration for stations 10 to 21, an additional term was applied to remove the pressure dependent conductivity residual;
- (ii) salinity bottle samples were analysed using a Guildline Autosal model 8400B (YeoKal salinometers had been used on all previous cruises); substandard measurements were not required, owing to the stability of the Autosal; international seawater standards were measured at the start and end of each day's analysis.

## 3.4.2 Underway measurements

Underway data collection is as described in previous data reports; data files are described in Part 5. Note that a sound speed of 1498 ms<sup>-1</sup> is used for all depth calculations.

## 3.4.3 ADCP

The acoustic Doppler current profiler (ADCP) instrumentation is described in previous data reports. Logging parameters are summarised in Table 3.6, while data results for this cruise will be discussed in a future report.

## Table 3.6: ADCP logging parameters.

ping parameters bottom track ping parameters

no. of bins: 60 no. of bins: 128 bin length: 8 m bin length: 4 m pulse length: 8 m pulse length: 32 m

delay: 4 m

ping interval: minimum ping interval: same as profiling pings

reference layer averaging: bins 8 to 13 ensemble averaging duration: 3 min.

## 3.5 MAJOR PROBLEMS ENCOUNTERED

After completion of station 6 at the southernmost end of the SR3 transect, the ship encountered thick pack ice while attempting to head northward. At one point the ship became stuck on top of an ice pressure ridge. Ballast waters were shifted and the vessel was freed after a total delay of 15 hours. No major logistical problems were encountered for the remainder of the voyage, with all scheduled work being completed.

The only significant problem with the instrumentation was the large amount of unusable CTD dissolved oxygen data. These bad data often occurred near the bottom of casts. Figure 3.2 summarises the spatial coverage of good CTD dissolved oxygen data (note that bottle dissolved oxygen data is good for the entire transect).

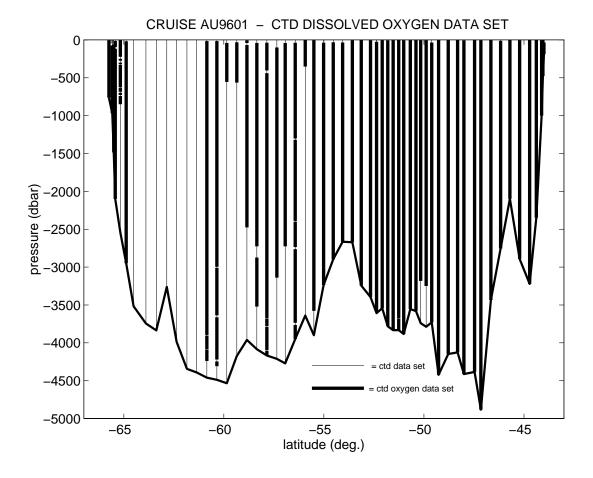


Figure 3.2: CTD dissolved oxygen data coverage along SR3 transect for cruise AU9601.

## 3.6 CTD RESULTS

This section details information relevant to the creation and quality of the final CTD and hydrology data set. For actual use of the data, the following is important:

```
CTD data - Tables 3.14 and 3.15, and Table 3.7; hydrology data - Tables 3.19 and 3.20.
```

Historical data comparisons are made in Part 4 of this report. Data file formats are described in Part 5.

#### 3.6.1 CTD measurements - data creation and quality

The final calibration results for conductivity/salinity and dissolved oxygen, along with the performance check for temperature, are plotted in Figures 3.3 to 3.6 (see Part 1 of this report for further details of the parameters plotted). For conversion to WOCE data file formats, see Part 5 of this report.

## 3.6.1.1 Conductivity/salinity

The conductivity calibration for CTD 1103 (stations 4 to 69) was of high quality (Figures 3.4 and 3.5), due in part to stable performance of the new Guildline salinometer. Note that for stations 10 to 21, the CTD conductivity cell was slightly fouled (the fouling was not discovered until after completion of station 21). This fouling resulted in a pressure dependent conductivity residual after initial calibration. An extra fit (Table 3.9) was applied to remove this residual, following the same method as described in Part 1 (section 1.6.1.1) of this report.

A small discontinuity of the order 0.0018 (PSS78) may exist in the CTD salinity data between stations 1-23 and stations 24-69 due to differences in International Standard Seawater batches, as described in section 3.6.2 below.

For test stations 1 and 2 using CTD 1193, CTD salinity accuracy is diminished (accurate to ~0.01 (PSS78)) as the only salinity samples available for calibration were collected from a single depth at station 1. For the test stations 3, 70 and 71, no bottle data are available for calibration of the CTD.

At ~580 dbar on the downcast of station 62, the ship's engine shutdown and all power was lost, leaving the ship adrift. The downcast was resumed approximately 2 hours later without retrieving the CTD. A small discontinuity at ~580 dbar may therefore be present in all parameters due to any local horizontal gradients.

#### 3.6.1.2 Temperature

Platinum temperature sensor performance of the CTD's was stable throughout the cruise, with a moderate mean offset between thermometer and CTD temperature values (Figure 3.3).

## 3.6.1.3 Dissolved oxygen

The final standard deviation value of the dissolved oxygen residuals (Figure 3.6) is less than 1% of full scale values (where full scale is approximately equal to 250  $\mu$ mol/l for pressure > 750 dbar, and 350  $\mu$ mol/l for pressure < 750 dbar). Unusual calibration coefficient values were found for some stations (Table 3.17), in particular for station 30 where the coefficient K<sub>5</sub> >> 1. CTD dissolved oxygen calibration for this station was of a lower quality than for other stations.

## 3.6.1.4 Summary of CTD data creation

Information relevant to the creation of the calibrated CTD data is tabulated, as follows:

- \* Surface pressure offsets calculated for each station are listed in Table 3.8.
- \* CTD conductivity calibration coefficients, including the station groupings used for the conductivity calibration, are listed in Tables 3.9 and 3.10.
- \* CTD raw data scans flagged for special treatment are listed in Table 3.11.
- \* Missing 2 dbar data averages are listed in Table 3.12.
- \* 2 dbar bins which are linearly interpolated from surrounding bins are listed in Table 3.13.
- \* Suspect 2 dbar averages are listed in Tables 3.14 and 3.15.
- \* CTD dissolved oxygen calibration coefficients are listed in Table 3.16. The starting values used for the coefficients prior to iteration, and the coefficients varied during the iteration, are listed in Table 3.17.
- \* The different protected and unprotected thermometers used for the stations are listed in Table 3.21.
- \* The pressure and temperature laboratory calibration coefficients for the CTD's used are listed in Table 3.22.

# 3.6.1.5 Summary of CTD data quality

CTD data quality cautions for the various parameters are summarised in Table 3.7.

<u>Table 3.7:</u> Summary of cautions to CTD data quality.

station no. 1,2 10-21	CTD parameter salinity salinity	caution test cast - all bottles fired at same depth; salinity accuracy reduced additional correction applied for pressure dependent conductivity
30	oxygen	residual oxygen calibration fit fairly poor
62	all	ship broke down - will be a discontinuity in downcast due to horizontal drift
1-23/24-69	salinity	discontinuity in salinity data of 0.0018 (PSS78) between the 2 station groups due to ISS batch difference
1-40	oxygen	values larger than for remaining stations by ~4μmol/l

# 3.6.2 Hydrology data

Quality control information relevant to the hydrology data is tabulated, as follows:

\* Dissolved oxygen Niskin bottle samples flagged with the code -9 (rejected for CTD dissolved oxygen calibration) are listed in Table 3.18.

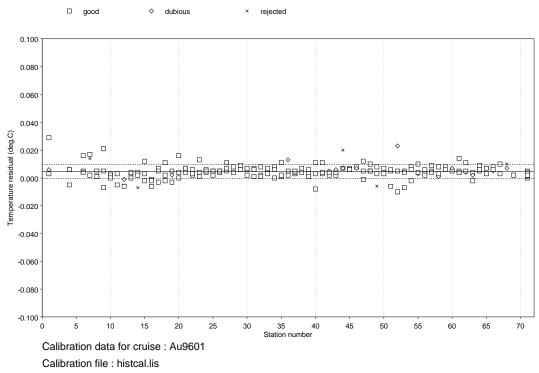
\* Questionable dissolved oxygen and nutrient Niskin bottle sample values are listed in Tables 3.19 and 3.20 respectively. Note that questionable values are included in the hydrology data file, whereas bad values have been removed.

Laboratory temperature on the ship was stable, with lab temperatures at the times of nutrient analyses having a most common value of 20°C.

International Standard Seawater (ISS) batch P128 (18th July 1995)) was used for salinity sample analyses of stations 1-23, while batch P130 (21st March 1996) was used for stations 24-69. Standardisation values on the salinometer were consistently different for these two ISS batches, indicating a problem with one of the batches. A discontinuity is therefore present in salinity bottle values, with station 24-69 values higher than station 1-23 values by 0.0018 ±0.0003 (PSS78). It is not known which ISS batch is at fault.

For dissoved oxygen data, stations 1 to 40 bottle values (and therefore CTD values also) are  $\sim 4\mu$ mol/l larger than for the remaining stations 41 to 69. Note that a jump in standardisation values for the laboratory analyses occurred between stations 40 and 41, accounting for the two groups of dissolved oxygen data. See Part 4 of this report for a more detailed discussion.

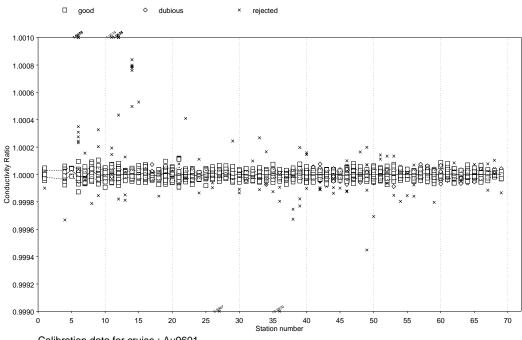
For stations 16 and 17 nutrient data, autoanalyser peak heights were measured manually.



Mean offset Temperature = 0.00463312c (s.d. = 0.0050  $^{\circ}c$ )

Number of samples used = 187 out of 193

<u>Figure 3.3:</u> Temperature residual ( $T_{therm}$  -  $T_{cal}$ ) versus station number for cruise au9601. The solid line is the mean of all the residuals; the broken lines are  $\pm$  the standard deviation of all the residuals (see CTD methodology). Note that the "dubious" and "rejected" categories refer to the conductivity calibration.

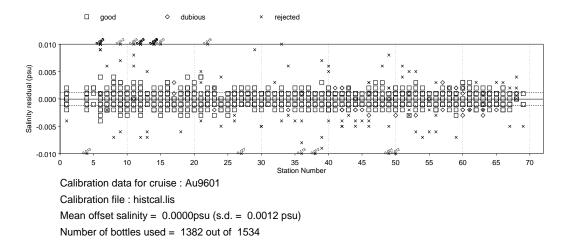


Calibration data for cruise: Au9601

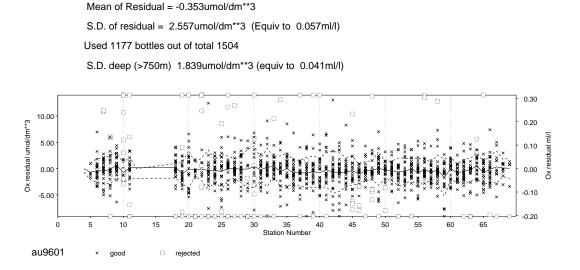
Calibration file: histcal.lis Conductivity s.d. = 0.00003

Number of bottles used = 1382 out of 1534 Mean ratio for all bottles = 1.00000

Figure 3.4: Conductivity ratio c<sub>btl</sub>/c<sub>cal</sub> versus station number for cruise au9601. The solid line follows the mean of the residuals for each station; the broken lines are  $\pm$  the standard deviation of the residuals for each station (see CTD methodology).



<u>Figure 3.5:</u> Salinity residual ( $s_{btl}$  -  $s_{cal}$ ) versus station number for cruise au9601. The solid line is the mean of all the residuals; the broken lines are  $\pm$  the standard deviation of all the residuals (see CTD methodology).



<u>Figure 3.6:</u> Dissolved oxygen residual ( $o_{btl}$  -  $o_{cal}$ ) versus station number for cruise au9601. The solid line follows the mean residual for each station; the broken lines are  $\pm$  the standard deviation of the residuals for each station (see CTD methodology).

Table 3.8: Surface pressure offsets (as defined in the CTD methodology).

stn no.	surface p offset (dbar)	stn no.	surface p offset (dbar)	stn no.	surface p offset (dbar)		surface p offset (dbar)
1	0.78	19	-2.68	37	-2.92	55	-2.66
2	0.61	20	-3.07	38	-2.84	56	-2.70
3	0.77	21	-2.73	39	-2.42	57	-3.18
4	-2.55	22	-2.20	40	-2.50	58	-3.08
5	-2.06	23	-2.71	41	-3.00	59	-2.69
6	-2.41	24	-2.60	42	-2.03	60	-2.77
7	-2.31	25	-2.65	43	-2.61	61	-3.19
8	-2.16	26	-2.85	44	-2.95	62	-2.81
9	-2.27	27	-2.69	45	-2.78	63	-3.15
10	-2.67	28	-2.52	46	-2.64	64	-3.01
11	-2.57	29	-2.99	47	-2.96	65	-3.02
12	-2.83	30	-2.89	48	-2.68	66	-3.13
13	-2.71	31	-3.25	49	-3.11	67	-3.13
14	-2.68	32	-2.88	50	-2.59	68	-3.35
15	-2.80	33	-3.28	51	-2.74	69	-3.15
16	-2.54	34	-2.59	52	-3.07	70	0.89
17	-2.70	35	-3.05	53	-3.31	71	0.41
18	-2.67	36	-2.69	54	-2.47		

<u>Table 3.9:</u> CTD conductivity calibration coefficients.  $F_1$ ,  $F_2$  and  $F_3$  are respectively conductivity bias, slope and station-dependent correction calibration terms. n is the number of samples retained for calibration in each station grouping;  $\sigma$  is the standard deviation of the conductivity residual for the n samples in the station grouping (see CTD methodology);  $\alpha$  is the correction applied to CTD conductivities due to pressure dependence of the conductivity residuals (see eqn 1.1 in Part 1 of this report).

stn grouping	F <sub>1</sub>	$F_2$	F <sub>3</sub>	n	σ	α
001 to 001	74396631	0.98848575E-03	0	19	0.000758	-
002 to 002	74396631	0.98848575E-03	0	19	0.000758	-
003 to 003	-	-	-	-	-	-
004 to 009	0.38105131E-01	0.10026968E-02	17129059E-07	109	0.001151	-
010 to 012	0.29464364E-01	0.10029643E-02	42023366E-07	63	0.001082	-1.72220E-06
013 to 014	0.22334088E-01	0.10031561E-02	28439980E-07	38	0.000808	-2.89414E-06
015 to 017	0.25912709E-01	0.10022619E-02	0.54122684E-07	71	0.000975	-3.23843E-06
018 to 021	0.17743922E-01	0.10042234E-02	38849067E-07	89	0.001224	-1.25810E-06
022 to 023	0.10979836E-02	0.10062176E-02	14796191E-07	45	0.000810	-
024 to 033	12532344E-01	0.10063905E-02	61267260E-10	224	0.000741	-
034 to 037	0.20512016E-02	0.10060457E-02	32684513E-08	83	0.000750	-
038 to 040	27578964E-01	0.10069364E-02	12822740E-08	60	0.000879	-
041 to 042	24668828E-01	0.10063144E-02	0.13021786E-07	41	0.000940	-
043 to 047	19096958E-01	0.10068804E-02	42245725E-08	106	0.000944	-
048 to 049	20424480E-01	0.10065386E-02	0.38684723E-08	40	0.000814	-
050 to 053	34297624E-01	0.10072630E-02	15337700E-08	86	0.001002	-
054 to 056	18440140E-01	0.10073180E-02	11331976E-07	61	0.000756	-
057 to 059	19465081E-01	0.10061536E-02	0.94647529E-08	68	0.000993	-
060 to 061	17832191E-01	0.10045096E-02	0.35861141E-07	45	0.001197	-
062 to 065	18907083E-01	0.10069848E-02	42532668E-08	89	0.000932	-
066 to 069	19880267E-01	0.10067129E-02	0.65647745E-09	45	0.001026	-
070 to 070	74396631	0.98848575E-03	0	19	0.000758	-
071 to 071	74396631	0.98848575E-03	0	19	0.000758	-

<u>Table 3.10:</u> Station-dependent-corrected conductivity slope term ( $F_2 + F_3$ . N), for station number N, and  $F_2$  and  $F_3$  the conductivity slope and station-dependent correction calibration terms respectively.

stn no.	$(F_2 + F_3 . N)$						
1	0.98848575E-03	19	0.10034853E-02	37	0.10059247E-02	55	0.10066947E-02
2	0.98848575E-03	20	0.10034465E-02	38	0.10068877E-02	56	0.10066834E-02
3	-	21	0.10034076E-02	39	0.10068864E-02	57	0.10066931E-02
4	0.10026283E-02	22	0.10058920E-02	40	0.10068851E-02	58	0.10067025E-02
5	0.10026112E-02	23	0.10058772E-02	41	0.10068483E-02	59	0.10067120E-02
6	0.10025940E-02	24	0.10063891E-02	42	0.10068613E-02	60	0.10066612E-02
7	0.10025769E-02	25	0.10063890E-02	43	0.10066988E-02	61	0.10066971E-02
8	0.10025598E-02	26	0.10063890E-02	44	0.10066946E-02	62	0.10067211E-02
9	0.10025426E-02	27	0.10063889E-02	45	0.10066903E-02	63	0.10067169E-02
10	0.10025441E-02	28	0.10063888E-02	46	0.10066861E-02	64	0.10067126E-02
11	0.10025021E-02	29	0.10063888E-02	47	0.10066819E-02	65	0.10067084E-02
12	0.10024601E-02	30	0.10063887E-02	48	0.10067243E-02	66	0.10067563E-02
13	0.10027864E-02	31	0.10063886E-02	49	0.10067281E-02	67	0.10067569E-02
14	0.10027579E-02	32	0.10063886E-02	50	0.10071863E-02	68	0.10067576E-02
15	0.10030737E-02	33	0.10063885E-02	51	0.10071848E-02	69	0.10067582E-02
16	0.10031278E-02	34	0.10059345E-02	52	0.10071833E-02	70	0.98848575E-03
17	0.10031819E-02	35	0.10059313E-02	53	0.10071817E-02	71	0.98848575E-03
18	0.10035242E-02	36	0.10059280E-02	54	0.10067060E-02		

<u>Table 3.11:</u> CTD raw data scans flagged for special treatment (see previous data reports for explanation).

station	approximate	raw scan	action	reason
number	pressure (dbar)	numbers	taken	
4	00	44044 44000 44000 44400		l. affact in atom and linet
4	98	14011-14220,14392-14422	. •	wake effect in steep gradient
4	106	15123-15275	ignore	wake effect in steep gradient
5	6-41	8352-13559	ignore	preliminary dip to 41 dbar
5	110	17848-18017	ignore	wake effect in steep gradient
6	3-30	2605-8552	ignore	preliminary dip to 30 dbar
6	11-16	2633-9148	ignore	fouling of cond. cell
7	8-22	2313-6115	ignore	preliminary dip to 22 dbar
8	9-28	1534-5118	ignore	preliminary dip to 28 dbar
9	9-40	6951-13639	ignore	preliminary dip to 40 dbar
11	10-158	11617-31172	ignore	preliminary dip to 158 dbar
12	9-31	3185-8956	ignore	preliminary dip to 31 dbar
14	9-25	1987-6352	ignore	preliminary dip to 25 dbar
17	9-33	3939-9105	ignore	preliminary dip to 33 dbar
19	7-39	4544-9809	ignore	preliminary dip to 39 dbar
20	8-35	3049-7411	ignore	preliminary dip to 35 dbar
28	1302-1354	74227-76421	ignore	fouling of cond. cell
29	8-30	5451-9404	ignore	preliminary dip to 30 dbar
34	576	57543-57686	ignore	fouling of cond. cell
58	329	30437-30772	ignore	fouling of cond. cell
62	199	19731-19995	ignore	fouling of cond. cell
66	226	22795-22871	ignore	fouling of cond. cell
71		81471-7,81548-81620,8168		
71		81780-2,81753-81768	ignore	bad data
71		125721-3,126067-126114	ignore	bad data
, ,		120121 0,120001 120114	ignore	שמע ממומ

<u>Table 3.12:</u> Missing data points in 2 dbar-averaged files. "1" indicates missing data for the indicated parameters: T=temperature; S=salinity,  $\sigma_T$ , specific volume anomaly and geopotential anomaly; O=dissolved oxygen. Note that jmin is the minimum number of data points required in a 2 dbar bin to form the 2 dbar average (see CTD methodology).

station number	pressures (dbar) where data missing	Т	s	0	reason
1,2	entire profile			1	no bottles for oxygen calibration
3	entire profile	1	1	1	no calibration data
4	2	1	1		bad data
4	entire profile			1	CTD oxygen hardware fault
5	2,4	1	1		bad data
5	2-14			1	bad data
6	2	1	1		bad data
7	2-8	1	1		bad data
7	2,22-32,46-72			1	bad data
8	2-58			1	bad data
9	2-8	1	1		bad data
9	2-12,98-116			1	bad data
10	226-248,278-298,324-328			1	bad data
10	626-630,688-696,730-738			1	bad data
10	852-bottom			1	bad data
11	2	1	1		bad data
11	2-16			1	bad data
12	2,4	1	1		bad data
14	2,4	1	1		bad data
15-18	2	1	1		bad data
12-18	entire profile			1	bad data
19	2-14,3898-3902,4090-4092			1	bad data
19	4242-bottom			1	bad data
20	2	1	1		bad data
20	2-14,2998-3008,3640-3660			1	bad data
20	4222-4244,4310-bottom			1	bad data
21	2	1	1		bad data
21	2-38,558-bottom			1	bad data
22	2	1	1		bad data
22	2-30,566-bottom			1	bad data
23	2,4	1	1		bad data
23	2,44-66,2478-bottom			1	bad data
24	2,4	1	1		bad data
24	2-38,2728-2872,3524-bottom			1	bad data
25	2-36,406-438,3680-3682			1	bad data
25	3780-3786,4096-4102,4162-41	68		1	bad data
26	2-98,3142-bottom			1	bad data
27	2-38,2728-bottom			1	bad data
28	2	1	1		bad data
28	1304-1318	1	1		fouling of conductivity cell
28	2-36,1304-1318,3738-3762			1	bad data
28	2392-2398,2738-2762			1	bad data
29	354-bottom			1	bad data
30	2	1	1		bad data
30	2,3580-bottom			1	bad data
31	2,4	1	1		bad data
31	2-36			1	bad data
32	2	1	1		bad data
32	2-30			1	bad data
33	2-32			1	bad data

Table 3.12: (continued)

station number	pressures (dbar) where data missing	Т	S	0	reason
34	2	1	1	1	bad data
36	2	1	1	1	bad data
37	4-24,3588-bottom			1	bad data
38	2	1	1	1	bad data
39	2,4			1	bad data
39	3782	1	1	1	no. of data pts in 2dbar bin < jmin
40	2	1	1	1	bad data
41	3678			1	bad data
42	2	1	1	1	bad data
45	2	1	1		bad data
45	2,3184-bottom			1	bad data
46	2,3252-bottom			1	bad data
47,48	2	1	1		bad data
48	3400-bottom			1	bad data
49	2,4	1	1		bad data
50	2	1	1		bad data
50	2,3352-bottom			1	bad data
52-54	2	1	1		bad data
52	2,4			1	bad data
53	2			1	bad data
54	2-34			1	bad data
58	2	1	1		bad data
58	2,4			1	bad data
60	2			1	bad data
62	2	1	1		bad data
62	2-10			1	bad data
64	2	1	1	1	bad data
67	2	1	1		bad data
69	2	1	1		bad data
69	2-32			1	bad data
70	entire profile	1	1	1	no calibration data
71	entire profile	1	1	1	no calibration data

<u>Table 3.13:</u> 2 dbar averages interpolated from surrounding 2 dbar values, for the indicated parameters.

station	interpolated	parameters
number	2 dbar values	interpolated
20	3692	T. S

<u>Table 3.14a:</u> Suspect 2 dbar salinity averages (+ temperature where indicated). Note: for suspect salinity values, the following are also suspect:  $\sigma_T$ , specific volume anomaly, and geopotential anomaly.

number  4	station	suspect 2 dl	bar values (dbar)	reason
5 - 98,100,106 salinity spike in steep local gradient 5 - 114,116,120 salinity spike in steep local gradient 6 - 6-10 possible fouling of conductivity cell 7 - 800-804,820,828 salinity spike in steep local gradient 7 826 - salinity spike in steep local gradient 14 70 - salinity spike in steep local gradient 15 76 - salinity spike in steep local gradient 16 - 78,80 salinity spike in steep local gradient 17 110 - salinity spike in steep local gradient 18 - 136-142 salinity spike in steep local gradient 19 - 136-142 salinity spike in steep local gradient 20 - 100-106,114 salinity spike in steep local gradient 20 - 128,130,136 salinity spike in steep local gradient 20 - 150,152,162,164 salinity spike in steep local gradient 21 - 150,152,162,164 salinity spike in steep local gradient 22 - 178,292 salinity spike in steep local gradient 23 salinity spike in steep local gradient 24 salinity spike in steep local gradient 25 salinity spike in steep local gradient 26 salinity spike in steep local gradient 27 salinity spike in steep local gradient 28 salinity spike in steep local gradient 29 salinity spike in steep local gradient 20 salinity spike in steep local gradient	number	bad	questionable	
5 - 114,116,120 salinity spike in steep local gradient 6 - 6-10 possible fouling of conductivity cell 7 - 800-804,820,828 salinity spike in steep local gradient 7 826 - salinity spike in steep local gradient 14 70 - salinity spike in steep local gradient 15 76 - salinity spike in steep local gradient 16 - 78,80 salinity spike in steep local gradient 17 110 - salinity spike in steep local gradient 19 - 136-142 salinity spike in steep local gradient 20 - 100-106,114 salinity spike in steep local gradient 20 - 128,130,136 salinity spike in steep local gradient 20 - 150,152,162,164 salinity spike in steep local gradient 21 - 150,152,162,164 salinity spike in steep local gradient 22 - 150,152,162,164 salinity spike in steep local gradient 23 salinity spike in steep local gradient 24 salinity spike in steep local gradient 25 salinity spike in steep local gradient 26 salinity spike in steep local gradient 27 salinity spike in steep local gradient 28 salinity spike in steep local gradient 29 salinity spike in steep local gradient 20 salinity spike in steep local gradient	4	-	90,92	salinity spike in steep local gradient
6 - 6-10 possible fouling of conductivity cell 7 - 800-804,820,828 salinity spike in steep local gradient 7 826 - salinity spike in steep local gradient 14 70 - salinity spike in steep local gradient 15 76 - salinity spike in steep local gradient 16 - 78,80 salinity spike in steep local gradient 17 110 - salinity spike in steep local gradient 18 - 136-142 salinity spike in steep local gradient 19 - 136-142 salinity spike in steep local gradient 20 - 100-106,114 salinity spike in steep local gradient 20 - 128,130,136 salinity spike in steep local gradient 20 - 150,152,162,164 salinity spike in steep local gradient 21 - 150,152,162,164 salinity spike in steep local gradient 22 - salinity spike in steep local gradient 23 salinity spike in steep local gradient 24 salinity spike in steep local gradient 25 salinity spike in steep local gradient 26 salinity spike in steep local gradient 27 salinity spike in steep local gradient 28 salinity spike in steep local gradient 29 salinity spike in steep local gradient 29 salinity spike in steep local gradient 20 salinity spike in steep local gradient		-	98,100,106	salinity spike in steep local gradient
7 - 800-804,820,828 salinity spike in steep local gradient 7 826 - salinity spike in steep local gradient 14 70 - salinity spike in steep local gradient 15 76 - salinity spike in steep local gradient 16 - 78,80 salinity spike in steep local gradient 17 110 - salinity spike in steep local gradient 19 - 136-142 salinity spike in steep local gradient 20 - 100-106,114 salinity spike in steep local gradient 20 - 128,130,136 salinity spike in steep local gradient 20 - 150,152,162,164 salinity spike in steep local gradient 21 - 150,152,162,164 salinity spike in steep local gradient 22 - 178,292 salinity spike in steep local gradient 23 - 178,292 salinity spike in steep local gradient 24 salinity spike in steep local gradient 25 - 178,292 salinity spike in steep local gradient 26 salinity spike in steep local gradient 27 salinity spike in steep local gradient 28 salinity spike in steep local gradient 29 salinity spike in steep local gradient 29 salinity spike in steep local gradient 29 salinity spike in steep local gradient 20 salinity spike in steep local gradient	5	-	114,116,120	salinity spike in steep local gradient
7826-salinity spike in steep local gradient1470-salinity spike in steep local gradient1576-salinity spike in steep local gradient15-78,80salinity spike in steep local gradient17110-salinity spike in steep local gradient19-136-142salinity spike in steep local gradient20-100-106,114salinity spike in steep local gradient20-128,130,136salinity spike in steep local gradient22-150,152,162,164salinity spike in steep local gradient39144-salinity spike in steep local gradient43656,692-salinity spike in steep local gradient52-178,292salinity spike in steep local gradient60-1160,1276-1280salinity spike in steep local gradient60-1322-1326salinity spike in steep local gradient60-13122-1326salinity spike in steep local gradient65-1010,1014salinity spike in steep local gradient	6	-	6-10	possible fouling of conductivity cell
1470-salinity spike in steep local gradient1576-salinity spike in steep local gradient15-78,80salinity spike in steep local gradient17110-salinity spike in steep local gradient19-136-142salinity spike in steep local gradient20-100-106,114salinity spike in steep local gradient20-128,130,136salinity spike in steep local gradient22-150,152,162,164salinity spike in steep local gradient39144-salinity spike in steep local gradient43656,692salinity spike in steep local gradient52-178,292salinity spike in steep local gradient60-1160,1276-1280salinity spike in steep local gradient60-1322-1326salinity spike in steep local gradient65-1010,1014salinity spike in steep local gradient	7	-	800-804,820,828	salinity spike in steep local gradient
1576-salinity spike in steep local gradient15-78,80salinity spike in steep local gradient17110-salinity spike in steep local gradient19-136-142salinity spike in steep local gradient20-100-106,114salinity spike in steep local gradient20-128,130,136salinity spike in steep local gradient22-150,152,162,164salinity spike in steep local gradient39144-salinity spike in steep local gradient43656,692salinity spike in steep local gradient52-178,292salinity spike in steep local gradient60-1160,1276-1280salinity spike in steep local gradient60-1322-1326salinity spike in steep local gradient65-1010,1014salinity spike in steep local gradient	7	826	-	salinity spike in steep local gradient
15 - 78,80 salinity spike in steep local gradient 17 110 - salinity spike in steep local gradient 19 - 136-142 salinity spike in steep local gradient 20 - 100-106,114 salinity spike in steep local gradient 20 - 128,130,136 salinity spike in steep local gradient 22 - 150,152,162,164 salinity spike in steep local gradient 39 144 - salinity spike in steep local gradient 43 656,692 - salinity spike in steep local gradient 43 656,692 - salinity spike in steep local gradient 52 - 178,292 salinity spike in steep local gradient 60 - 1160,1276-1280 salinity spike in steep local gradient 60 - 322-1326 salinity spike in steep local gradient 65 - 1010,1014 salinity spike in steep local gradient	14	70	-	salinity spike in steep local gradient
17 110 - salinity spike in steep local gradient salinity	15	76	-	salinity spike in steep local gradient
19 - 136-142 salinity spike in steep local gradient 20 - 100-106,114 salinity spike in steep local gradient 20 - 128,130,136 salinity spike in steep local gradient 22 - 150,152,162,164 salinity spike in steep local gradient 39 144 - salinity spike in steep local gradient 43 656,692 - salinity spike in steep local gradient 52 - 178,292 salinity spike in steep local gradient 52 salinity spike in steep local gradient 55 - 1322-1326 salinity spike in steep local gradient 56 - 1010,1014 salinity spike in steep local gradient 57 salinity spike in steep local gradient 58 salinity spike in steep local gradient 59 salinity spike in steep local gradient 59 salinity spike in steep local gradient 50 salinity spike in steep local gradient 50 salinity spike in steep local gradient 59 salinity spike in steep local gradient 50 salinity spike in 50 salinity spike	15	-	78,80	salinity spike in steep local gradient
20 - 100-106,114 salinity spike in steep local gradient 20 - 128,130,136 salinity spike in steep local gradient 22 - 150,152,162,164 salinity spike in steep local gradient 39 144 - salinity spike in steep local gradient 43 656,692 - salinity spike in steep local gradient 52 - 178,292 salinity spike in steep local gradient 60 - 1160,1276-1280 salinity spike in steep local gradient 60 - 1322-1326 salinity spike in steep local gradient 65 - 1010,1014 salinity spike in steep local gradient	17	110	-	salinity spike in steep local gradient
20 - 128,130,136 salinity spike in steep local gradient 22 - 150,152,162,164 salinity spike in steep local gradient 39 144 - salinity spike in steep local gradient 43 656,692 - salinity spike in steep local gradient 52 - 178,292 salinity spike in steep local gradient 60 - 1160,1276-1280 salinity spike in steep local gradient 60 - 1322-1326 salinity spike in steep local gradient 65 - 1010,1014 salinity spike in steep local gradient	19	-	136-142	salinity spike in steep local gradient
22 - 150,152,162,164 salinity spike in steep local gradient 39 144 - salinity spike in steep local gradient 43 656,692 - salinity spike in steep local gradient 52 - 178,292 salinity spike in steep local gradient 60 - 1160,1276-1280 salinity spike in steep local gradient 60 - 1322-1326 salinity spike in steep local gradient 65 - 1010,1014 salinity spike in steep local gradient	20	-	100-106,114	salinity spike in steep local gradient
39 144 - salinity spike in steep local gradient 43 656,692 - salinity spike in steep local gradient 52 - 178,292 salinity spike in steep local gradient 60 - 1160,1276-1280 salinity spike in steep local gradient 60 - 1322-1326 salinity spike in steep local gradient 65 - 1010,1014 salinity spike in steep local gradient	20	-	128,130,136	salinity spike in steep local gradient
43 656,692 - salinity spike in steep local gradient 52 - 178,292 salinity spike in steep local gradient 60 - 1160,1276-1280 salinity spike in steep local gradient 60 - 1322-1326 salinity spike in steep local gradient 65 - 1010,1014 salinity spike in steep local gradient	22	-	150,152,162,164	salinity spike in steep local gradient
52 - 178,292 salinity spike in steep local gradient 60 - 1160,1276-1280 salinity spike in steep local gradient 60 - 1322-1326 salinity spike in steep local gradient 65 - 1010,1014 salinity spike in steep local gradient	39	144	-	salinity spike in steep local gradient
60 - 1160,1276-1280 salinity spike in steep local gradient 60 - 1322-1326 salinity spike in steep local gradient 65 - 1010,1014 salinity spike in steep local gradient	43	656,69	2 -	salinity spike in steep local gradient
60 - 1322-1326 salinity spike in steep local gradient 65 - 1010,1014 salinity spike in steep local gradient	52	-	178,292	salinity spike in steep local gradient
65 - 1010,1014 salinity spike in steep local gradient	60	-	1160,1276-1280	salinity spike in steep local gradient
, , , , , , , , , , , , , , , , , , , ,	60	-	1322-1326	salinity spike in steep local gradient
65 1012 - salinity spike in steep local gradient	65	-	1010,1014	salinity spike in steep local gradient
	65	1012	-	salinity spike in steep local gradient

<u>Table 3.14b:</u> Suspect 2 dbar-averaged data from near the surface (applies to all parameters other than dissolved oxygen, except where noted).

0	or triair a		, oxoopt			
stn		2dbar values		stn		t 2dbar values
no.	bad	<u>questionable</u>		no.	bad	questionable
4	-	4-10		52	4	-
5	-	6		53	-	4
6	-	6-10		54	-	4
8	2	-		56	2	-
11	-	4		58	-	4
12	-	6,8		59	2	-
16	-	4 (T okay)		60	-	2 (T okay)
18	-	4,6		61	-	2
19	2-6	-		62	-	4
20	4,6	-		63	-	2 2
21	4-8	10-14		65	-	2
22	4	-		66	2	4
24	6	-		67	-	4
25	-	2		68	-	2,4
26	-	2,4		69	-	4
27	-	2				
29	2	-				
35	2	4,6				
37	-	2-6				
41	-	2				
42	4	6-10				
44	-	2				
46	2	-				
47	-	4				
48	4	-				
50	4	-				

Table 3.15: Suspect 2 dbar-averaged dissolved oxygen data.

stn suspect 2dbar values(dbar)			stn su	spect 2	dbar values(dbar)
no.	bad o	questionable	no.	bad o	questionable
6	-	4	41	-	2
20	-	58-62,80-82	42	-	4,6,12-34
23	6-18	-	43	-	2
29	-	2-8	44	2-10	-
30	-	4-56,2176-3578	46	-	4-10
34	-	4-8	50	-	12-32
35	-	38,40,52,54,68	51	-	2-6
36	-	4	56	-	2
37	-	34,36	57	-	2-34
38	-	14-18	60	-	4-10
39	-	12-24			
40	-	4,6			

<u>Table 3.16:</u> CTD dissolved oxygen calibration coefficients.  $K_1$ ,  $K_2$ ,  $K_3$ ,  $K_4$ ,  $K_5$  and  $K_6$  are respectively oxygen current slope, oxygen sensor time constant, oxygen current bias, temperature correction term, weighting factor, and pressure correction term. dox is equal to 2.8 $\sigma$  (for  $\sigma$  as defined by eqn A2.24 in the CTD methodology); n is the number of samples retained for calibration in each station or station grouping.

station	$K_1$	$K_2$	$K_3$	$K_4$	$K_5$	$K_6$	dox	n
numbe	r							
1-4	_	_	-	-	-	-	_	_
5	7.977	5.00	-0.903	-0.15206	0.65057	0.19386E-03	0.08607	4
6	2.216	5.00	0.250	-0.13008	0.25629	0.53099E-04	0.14567	24
7	0.922	5.00	0.502	-0.12390	0.11961	0.12705E-04	0.14944	22
8	0.942	5.00	0.632	-0.22443	0.48146	0.19279E-04	0.16980	19
9	3.650	8.00	0.315	-0.31208	0.74841	0.45625E-04	0.14580	24
10	1.181	5.00	0.484	-0.10030	0.20991	-0.46710E-04	0.11310	10
11	7.372	8.00	-0.984	-0.03645	0.12896	0.13085E-03	0.13112	18
12-18	-	-	-	-	-	-	-	-
19	9.970	5.00	-1.309	-0.13446	0.71125	0.10492E-03	0.12424	20
20	10.893	5.00	-1.574	-0.10461	0.68169	0.10988E-03	0.22049	20
21	8.782	7.00	-1.164	-0.10375	0.27859	0.23859E-03	0.07780	8
22	10.780	8.00	-1.159	-0.18501	0.74659	-0.30282E-03	0.13646	8
23	13.095	5.00	-1.881	-0.14275	0.71999	0.12092E-03	0.24383	18
24	13.788	8.00	-2.059	-0.15753	0.45006	0.11444E-03	0.12085	21
25	15.839	8.50	-2.414	-0.17273	0.61228	0.12524E-03	0.21887	
26	10.964	6.00	-1.593	-0.08905	0.50065	0.13016E-03	0.14554	-
27	14.482	6.00	-2.076	-0.17650	0.51565	0.63161E-04	0.11809	
28	11.079	6.00	-1.659	-0.04909	1.23120	0.15427E-03	0.15871	-
29	11.232	8.00	-1.723	-0.02111	0.71090	0.28299E-03	0.23383	7
30	12.399	5.00	-1.917	-0.04067	3.41140	0.21041E-03	0.24999	-
31	13.137	5.00	-1.984	-0.09521	0.92360	0.14840E-03	0.13421	_
32	12.151	5.00	-1.818	-0.07098	0.31861	0.12694E-03	0.22956	
33	11.447	5.00	-1.684	-0.06222	0.20779	0.12393E-03	0.10320	
34	14.974	7.00	-2.250	-0.14137	0.93157	0.14922E-03	0.19063	
35	13.503	5.00	-2.034	-0.10348	1.55730	0.18499E-03	0.18944	
36	13.167	5.00	-1.952	-0.11089	0.93079	0.14698E-03	0.15666	
37	12.810	5.00	-1.897	-0.09934	0.92874	0.14852E-03	0.14493	
38	13.964	5.00	-2.049	-0.14110	1.10950	0.14467E-03	0.18674	
39	12.315	5.00	-1.779	-0.11737	1.15650	0.14835E-03	0.18201	
40	12.799	5.00	-1.872	-0.10613	0.84008	0.12872E-03	0.17978	
41	13.666	5.00	-2.016	-0.12765	0.92883	0.13385E-03	0.20248	23

Table 3.16: (continued)

station number	<b>Κ</b> <sub>1</sub>	$K_2$	<b>K</b> <sub>3</sub>	K <sub>4</sub>	K <sub>5</sub>	5	$K_6$	dox	n
42	13.239	5.00	-1.985	-0.11293	0.8	38499	0.15201E-03	0.25177	24
43	12.990	5.00	-1.931	-0.11076		91703	0.15071E-03	0.23118	24
44	12.650	8.00	-1.860	-0.10660	0.9	91335	0.13240E-03	0.17877	23
45	11.968	5.00	-1.835	-0.05606	0.3	39845	0.16464E-03	0.17434	20
46	11.624	5.00	-1.703	-0.08886	0.9	93062	0.15078E-03	0.11577	20
47	11.238	5.00	-1.651	-0.07039	0.7	76785	0.14245E-03	0.11352	23
48	10.654	5.00	-1.527	-0.07438	0.8	39526	0.14189E-03	0.11396	20
49	10.460	5.00	-1.513	-0.06562	1.0	00040	0.15150E-03	0.20295	22
50	13.487	5.00	-2.003	-0.13628	1.1	12640	0.16671E-03	0.09998	22
51	11.429	5.00	-1.674	-0.07639	0.0	37000	0.14268E-03	0.11557	24
52	13.893	5.00	-2.011	-0.16381	1.2	21440	0.15485E-03	0.16197	22
53	11.973	5.00	-1.723	-0.09890	0.9	99061	0.13249E-03	0.16167	24
54	8.123	5.00	-1.096	-0.03568	0.0	97237	0.12951E-03	0.12116	22
55	10.257	5.00	-1.441	-0.07503	0.9	92291	0.12490E-03	0.18500	24
56	13.329	5.00	-2.015	-0.10473	0.0	30404	0.14212E-03	0.12378	22
57	11.954	5.00	-1.764	-0.09596	0.9	91435	0.14067E-03	0.12476	24
58	14.906	5.00	-2.207	-0.15879	1.0	00730	0.13214E-03	0.17453	23
59	12.717	8.00	-1.914	-0.09111	0.7	77570	0.14559E-03	0.21816	
60	14.505	5.00	-2.192	-0.13230	0.9	92839	0.14503E-03	0.13844	
61	11.118	5.00	-1.613	-0.08351	0.9	90790	0.14216E-03	0.11000	
62	10.148	5.00	-1.437	-0.08017	1.0	05690	0.15153E-03	0.14261	23
63	9.048	5.00	-1.232	-0.06994	1.1	18910	0.11739E-03	0.13847	19
64	11.613	8.00	-1.851	-0.05570	0.7	79147	0.15911E-03	0.15317	
65	10.876	5.00	-1.562	-0.07559	0.9	92785	0.14065E-03	0.13997	23
66	10.325	5.00	-1.345	-0.11909		18150	0.10524E-03	0.15732	_
67	10.556	5.00	-1.583	-0.05825		93328	0.18770E-03	0.19300	
68-69	5.606	5.00	-0.384	-0.03367	0.9	95645	0.57658E-04	0.11008	15

<u>Table 3.17:</u> Starting values for CTD dissolved oxygen calibration coefficients prior to iteration, and coefficients varied during iteration (see CTD methodology). Note that coefficients not varied during iteration are held constant at the starting value.

station numbe	K <sub>1</sub>	K <sub>2</sub>	K <sub>3</sub>	K <sub>4</sub>	$K_5$	K <sub>6</sub>		efficients ried
1-4	-	-	_	_	_	-		_
5	8.900	5.0000	-0.700	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
6	5.200	5.0000	1.000	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
7	4.000	5.0000	1.300	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
8	3.600	5.0000	1.300	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
9	3.400	8.0000	0.900	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
10	2.100	5.0000	0.700	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
11	7.420	8.0000	-0.960	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
12-18	-	-	-	-	-	-		-
19	10.240	5.0000	-1.100	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
20	12.500	5.0000	-1.300	-0.400E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
21	10.800	7.0000	-0.800	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
22	9.800	8.0000	-0.900	-0.450E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
23	12.700	5.0000	-1.500	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
24	8.300	8.0000	-0.350	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$

Table 3.17: (continued)

station numbe		$K_2$	<b>K</b> <sub>3</sub>	$K_4$	<b>K</b> <sub>5</sub>	K <sub>6</sub>		efficients ied
25	15.600	8.5000	-2.200	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
26	11.900	6.0000	-1.400	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
27	13.900	6.0000	-1.900	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
28	11.200	6.0000	-1.600	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
29	11.200	8.0000	-1.700	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
30	12.150	5.0000	-1.800	-0.370E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
31	14.100	5.0000	-1.700	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
32	13.800	5.0000	-1.400	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
33	12.900	5.0000	-1.300	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
34	14.000	7.0000	-1.700	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
35	14.900	5.0000	-1.700	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
36	13.800	5.0000	-1.700	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
37	14.100	5.0000	-1.700	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
38	14.900	5.0000	-2.100	-0.360E-01	0.900	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
39	13.500	5.0000	-1.900	-0.380E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
40	13.110	5.0000	-1.600	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
41	14.100	5.0000	-2.000	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
42	13.700	5.0000	-1.800	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
43	13.600	5.0000	-1.800	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
44	13.550	8.0000	-1.850	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
45	12.300	5.0000	-1.800	-0.400E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
46	12.900	5.0000	-1.450	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
47	12.500	5.0000	-1.200	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
48	12.000	5.0000	-1.050	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
49 50	12.600	5.0000 5.0000	-1.400	-0.360E-01	0.770	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
50 51	14.400 12.900	5.0000	-2.100 -1.400	-0.550E-01 -0.360E-01	0.750 0.750	0.15000E-03 0.15000E-03	$K_1$ $K_1$	$K_3 K_4 K_5 K_6$
52	14.500	5.0000	-2.000	-0.300E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6 K_3 K_4 K_5 K_6$
53	12.800	5.0000	-1.500	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
54	8.000	5.0000	-1.100	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
55	11.700	5.0000	-1.200	-0.360E-01	0.750	0.15000E-03	Κ <sub>1</sub>	$K_3 K_4 K_5 K_6$
56	13.800	5.0000	-2.000	-0.360E-01	0.550	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
57	13.000	5.0000	-1.700	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
58	16.200	5.0000	-2.350	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
59	14.300	8.0000	-1.800	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
60	14.500	5.0000	-2.100	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
61	12.300	5.0000	-1.300	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
62	11.600	5.0000	-1.100	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
63	10.700	5.0000	-1.100	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
64	11.400	8.0000	-1.900	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
65	12.500	5.0000	-1.200	-0.360E-01	0.740	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
66	11.400	5.0000	-1.200	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
67	10.000	5.0000	-1.800	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
68-69	5.600	5.0000	-0.400	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$

<u>Table 3.18:</u> Dissolved oxygen Niskin bottle samples flagged as -9 for dissolved oxygen calibration. Note that this does not necessarily indicate a bad bottle sample - in many cases, flagging is due to bad CTD dissolved oxygen data.

station	rosette	station	rosette
number	position	number	position
7	21,9	38	8
8	24,23,22,21,20	39	21,19
10	24,21,13,11-1	40	17
11	24,21,20,19,18,6	41	18
18	24,20	45	18,3,2,1
19	24,5,2,1	46	15,3,2,1
20	24,21,2,1	47	12
21	24,15-1	48	19,3,2,1
22	20,15-1	49	20
23	6,5,4,3,2,1	50	2,1
24	24,2,1	52	21,20
25	24,20,18	54	24,19
26	24,23,22,21,2,1	56	19,18
27	24,1	58	23
28	24	62	24
29	17-1	63	5,4,3,2,1
30	23,19,7,5,4,3,2,1	64	7,4
31	24	65	18
32	24	66	19
33	24,19	67	14
34	18	69	12
37	24,1		

<u>Table 3.19:</u> Questionable dissolved oxygen Niskin bottle sample values (not deleted from hydrology data file).

stn no.	rosette position
11	6
13	23
19	5
38	8
64	7,4

<u>Table 3.20:</u> Questionable nutrient sample values (not deleted from hydrology data file).

PHOSP	HATE	NITR	ATE	SILICATE		
station	rosette	station	rosette	station	rosette	
number	position	<u>number</u>	position	<u>number</u>	position	
6	15,14,13	6	8		-	
		7	7,5			
				10	6	
13	23	13	23	13	23	
24	3	24	3			
26	2					
27	9	27	9			
29	22	29	22			
31	4	31	4			
32	4					
		35	2			
		38	9			
		60	4			

<u>Table 3.21:</u> Protected and unprotected reversing thermometers used (serial numbers are listed).

protected thermometers

station rosette position 24 rosette position 12 rosette position 2 numbers thermometers thermometers 1 to 70 12095,12096 12094 rosette position 12 rosette position 2 thermometers 12119,12120

71 12095 (pos. 24); 12096 (pos.17); 12094 (pos.12); 12120 (pos. 7); 12119 (pos. 2)

unprotected thermometers

station rosette position 12 rosette position 2 numbers thermometers thermometers 1 to 27 11993 11992 11993

<u>Table 3.22:</u> Calibration coefficients and calibration dates for CTD serial numbers 1103 and 1193 (unit nos 7 and 5 respectively) used during RSV Aurora Australis cruise AU9601. Note that an additional pressure bias term due to the station dependent surface pressure offset exists for each station (eqn A2.1 in the CTD methodology). Also note that platinum temperature calibrations are for the ITS-90 scale.

	CTD serial 110 coefficient	3 (unit no. 7) value of coefficient		CTD serial 119 coefficient	93 (unit no. 5) value of coefficient
	re calibration coe Calibration Fact pcal0 pcal1 pcal2 pcal3 pcal4			re calibration cod Calibration Fact pcal0 pcal1 pcal2 pcal3 pcal4	efficients ility - 05/07/1996 -1.107604e+01 1.008327e-01 0.0 0.0
	m temperature ca Calibration Faci Tcal0 Tcal1 Tcal2	alibration coefficients ility - 27/06/1996 0.28797e-01 0.49988e-03 0.35049e-11			alibration coefficients ility - 26/06/1996 -0.46860e-01 0.49879e-03 0.27541e-11
	rre temperature c Calibration Faci Tpcal0 Tpcal1 Tpcal2 Tpcal3	alibration coefficients fility - 10/07/1996 1.713678e+02 -4.239208e-03 1.481513e-08 0.0			ralibration coefficients ility - 05/07/1996 1.299013e+02 -2.541029e-03 -7.814892e-09 0.0
press	•	ture correction to ility - 10/07/1996 20.00 -9.196843e-06 -7.818015e-02	press	ure .	ility - 05/07/1996 20.00 -1.578863e-05 -6.349700e-02

# **APPENDIX 3.1** Hydrochemistry Laboratory Report

Seawater samples were analysed for nutrient concentrations (nitrate plus nitrite, silicate, and phosphate), salinities, and dissolved oxygen concentrations. The methods used are described in Eriksen (1997). A new type of salinometer, improvements to nutrient autoanalyser chemistries, improvements to inter-run quality checks, and improvements to dissolved oxygen methods were implemented on this cruise.

Number of samples analysed:

Nutrients (nitrate plus nitrite, silicate, phosphate): 1520

Salinities: 1560

Dissolved oxygens: 1610

## A3.1.1 NUTRIENTS

The Alpkem auto-analyser performed well on this cruise as did the new version (1.31) of Faspac software. Phosphate, silicate and nitrate + nitrite were analysed for all sites. Nitrate and nitrite were not analysed separately as only three channels could be run concurrently.

A 20 L carbuoy of seawater was filtered through a GFF filter, mixed and sub sampled into 10 ml tubes, then frozen immediately. At least two of these samples were run with each run and used as an in-house quality control. It was found that this sample was stable for the duration of the trip. See Figure A3.1.2 and Table A3.1.2.

The sample racks were covered with aluminium foil when in the sampler, making sure that it was not in contact with the sample. This served to reduce splashing, sample carryover and the possibility of airborne contamination.

On a couple of occasions there was a shift in the baseline on one or more of the channels. This was generally due to either foreign matter or a bubble becoming lodged in the flow cell. For these runs the affected peaks were either measured manually from the chart or repeated.

The temperature of the laboratory near the Auto-analyser was stable, remaining in the range of 19.5° to 20.5° for the voyage.

All channels were run without the colour reagent for at least six sites (approximately 150 samples) to calculate an average background matrix correction. For both nitrate + nitrite and silicate channels there was no significant background matrix, but for phosphate a background matrix of 0.088  $\mu$ mol/l was measured. There has been no correction applied to the phosphate results: this facilitates comparisons with previous cruise results as no corrections have been applied in the past (see Part 4 of this report).

Some modifications were made to the methodology used in previous cruises, as follows.

# Nitrate + Nitrite

The nitrate + nitrite channel was unstable for the first ten runs, with the bubble pattern breaking down in the cadmium tube. This resulted in poor peak shape and inconsistent results for the QC (quality check) and duplicate samples. The cadmium tube was replaced with a new tube and the duplicate samples were run for the nitrate + nitrite results only. The new cadmium tube resulted in a much better flow pattern with no problems with either duplicate or QC samples.

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Sample :-Flow rate 0.32 ml/min Nitrogen :-Flow rate 0.23 ml/min

Reagent 1:-Imidazole (4.25 g/L) + Hydrochloric acid (1.15 ml/L) + Brij (0.5 ml/L)

Flow rate 0.32 ml/min

Reagent 2:-Sulphanilamide (3.12 g/L) + Hydrochloric acid (31 ml/L) + Brij (0.5 ml/L)

Flow rate 0.16 ml/min

Reagent 3:-N-1 Naphthylethylene di-amine di-hydrochloride (0.31 g/L) + Brij (0.5 ml/L)

Flow rate 0.16 ml/min

**Debubbler:-** Flow rate 0.42 ml/min

## **Phosphate**

The reagent for the phosphate was changed from a single mixed reagent to two reagents. The ammonium molybdate and sulphuric acid were in reagent one and the ascorbic acid and antimony potassium tartrate were in reagent two. This was done to prolong the working life of the reagents from about 8 hours to at least 24 hours. It also made it easier to do the background matrix correction run. The pH of the system was lowered slightly from what had been used in the past because the buffering effect of the seawater resulted in the pH of the system being raised to a level where the silicate may have interfered with the phosphate chemistry.

On the first couple of runs there was a great deal of peak diffusion, with the trace not coming back to baseline between samples. The system was rebuilt with all tubing connections being checked and redone if necessary. This did not fix the problem to any degree. It was noticed that the heating coil being used was for a silicate channel. This was changed for a phosphate module, which fixed the problem. Although it seems that the heating coils are constructed of the same type of tubing (PEEK) with the phosphate coil being of greater length (which would not account for the problem), and although the sales rep advised that there was no difference that he was aware of, it appears to be the source of the problem.

It was noticed that while there was a need for wetting agent to be used for the system to run smoothly, an excess of the wetting agent caused the baseline both to become noisy and to gradually shift. The wetting agent currently in use is dowfax, which is lauryl sulphate based. It may be worth using straight lauryl sulphate which is in use in other laboratories - it has been noted to depress the sensitivity if in excess, but not to affect the baseline.

On one occasion the Eppendorf syringe used to add the sulphuric acid appeared to have affected the baseline noise level, possibly by plasticisers or contamination being introduced to the reagent. After replacing the syringe the baseline noise returned to its previous level.

Sample :- Flow rate 0. 80 ml/min Air :- Flow rate 0.23 ml/min Reagent 1:- Dowfax (2 ml/L)

Flow rate 0.80 ml/min

Reagent 2:- Ammonium molybdate (5.04 g/L) + Sulphuric acid (56 ml/L)

Flow rate 0.23 ml/min

Reagent 3:- Ascorbic acid (4.56 g/L) + Antimony potassium tartrate (0.1275 g/L)

Flow rate 0.23 ml/min

Flow rate 0. 42 ml/min Debubbler :-

#### Silicate

The silicate channel did not give any problems for the duration of the cruise, the only modification to the system being that no acetone was used in the reagent. The silicate channel is currently being heated to 37°C to stabilise the baseline and improve the duplicate and replicate results. Some more work needs to be done to rule out interferences, such as from phosphate, or other possible errors.

**Sample** :- Flow rate 0.23 ml/min Flow rate 0.23 ml/min

Reagent 1:- Ammonium molybdate (10 g/L) + Sulphuric acid (2.8 ml/L) + Dowfax (1 ml/L)

Flow rate 0.42 ml/min

Reagent 2:- Oxalic acid (50 g/L) + Dowfax (0.5 ml/L)

Flow rate 0.32 ml/min

Reagent 3:- Ascorbic acid (17.6 g/L)

Flow rate 0.42 ml/min

**Debubbler:-** Flow rate 0.60 ml/min

**Sampler :-** Total pumping rate of artificial seawater into the sampler = 3.39 ml/min

Total pumping rate of artificial seawater out of the sampler 5.78 ml/min

Artificial Seawater :- Sodium Chloride (39 g/L)

The oscillating baseline problem which occurs when Faspac is started is still present. Some work was done looking at grounding of detectors and computers, looking at the wiring of ground to the A/D board, and at further shielding, with no success.

The 'glitch' problem with the A/D board at the mid-point voltage was fixed by purchasing a new A/D board from Labtronics. Although the 'glitch' is still present, it is now negligible.

The version of data logging software used, Faspac 1.31, was an improvement on that used on cruise AU9604 (Faspac 1.2). It did not crash, and produced Excel files which did not cause Excel to crash. The Excel files had a text format, which the output from Faspac 1.2 did not have, so Hydro was modified to convert the cells to numbers, using the 'VALUE' command.

The method of making tops was improved. Previously, standards were made up in six 100 ml volumetric flasks, and tops were made up in a 500 ml volumetric flask. The top standard and the 'tops' were nominally the same concentration, but small differences were possible since they were made up separately. Now all the standards but the top standard are made up as previously. The top standard is made in a 500 ml volumetric flask, and this is also used to make the 'tops'. Thus the 'tops' and top standard have the same source, and the only variation should be due to the process of pouring into 10 ml sample tubes. A comparison was made between the top standard made in a 100 ml flask and a 500 ml flask. No difference was seen. The advantage of making the top standard and 'tops' together is that if a run is found to be unstable, corrections can be made by equating 'tops' values with the top standard.

As usual 'tops' were used to monitor intra-run stability of the system. All the tops for all three channels were examined manually by the operator and found to be satisfactory.

A variation from normal data processing was used. As usual Faspac produced .ACF files, and exported data as .XLS files. Normally the .XLS files represent runs, and can have tops extracted to examine run stability, or have the error in the calibration curve. However on this cruise data was cut and pasted from these .XLS files, thus destroying the integrity of run information. If further examination of the data were required it would be necessary to repeat the export process from Faspac. Care would be needed to separate the new intact .XLS files from the old fragmented .XLS files.

## A3.1.2 SALINITIES

A Guildline 'Autosal' salinometer, SN 62549, was used. This was the first time the CRC had used this instrument. The reliability of the instrument was excellent, in contrast to experience with Yeo-Kal

salinometers. The instrument was stable enough so that a secondary 'substandard' was not necessary.

A peristaltic pump from Ocean Scientific was used to pump in samples. Pump speeds 1, 2, or 3 were used. There was no difference to the result between these pump speeds if the samples were temperature equilibrated.

The salinometer has a capability of logging data directly to a computer, but this was not used as an interface was not built in time.

The "Hydro" program was modified so that the double conductivity ratio given by the Guildline salinometer could be entered and converted to salinity.

The biggest problem was with bubbles forming on the electrodes of the conductivity cell. These collected mostly in the first and last electrodes. We had been advised by Guildline that the bubbles had no effect, and by Ocean Scientific that a few bubbles would have no effect, but that a lot of bubbles might. Causes of error would be restricting electrical current flow, and changing the volume of seawater within the cell. A quick test showed that a few bubbles made no difference, and CSIRO users have also found this. However, it is not clear to what extent bubbles may eventually affect results, and the cell was debubbled after every crate of 24 samples, and before every standardisation. The cell was debubbled by rinsing with ethanol or ethanol with Brij. Both were equally effective. The ethanol was found to corrode the inlet and outlet tubes of the peristaltic pump, so the inbuilt air pump was used for pumping ethanol. Methanol was also tried, but was not as effective as ethanol.

Two sets of standards were used, P128 and P130. The standards were compared by standardising the instrument with one standard, measuring the other standard, and comparing it with its nominal value. It was found that P128 read 0.0018 +/- 0.0003 (PSS78) higher than P130. The cause of this difference is not known. If the cause is that P128 is more concentrated than its nominal value, then any samples measured with the salinometer standardised with P128 would appear lower than they really are. It is also assumed that any errors in standardisation will result in an offset across the range of measured salinities. If this is also true, then any samples measured with the salinometer standardised with P128 would appear 0.0018 (PSS78) lower than they really are. This would mean a correction of 0.0018 (PSS78) would need to be added on (no correction was applied to the data).

The standardisation values are in Figure A3.1.3. The comparison of P128 and P130 is in Table A3.1.3.

A crate of 24 samples were analysed for calibration of the underway thermosalinograph. This was entered into Hydro as station 300.

# A3.1.3 DISSOLVED OXYGEN

Dissolved oxygen analyses generally went well. Problems are described below.

By using the READVOLT.BAS program the factors which most affected the current across the electrodes could be observed. It was seen that the position of the beaker and the stirring rate had profound effects, whereas the addition of sodium thiosulfate or potassium biiodate had only moderate effects. This indicated that effort was needed to keep the stirring rate and position of electrodes in the beaker constant.

The magnetic stirrer which had previously been used for the salinity substandard was used for stirring during preparation of the biiodate standard. This meant that the stirring rate control knob on the Dosimat could be left at the same value. Previously stirring of the biiodate standard had been done with the Dosimat magnetic stirrer, so that the actual titration speed always varied slightly, as the stirring rate of standards and samples is different.

The "Newwink" program was modified so that blanks could be done entirely with the single Dosimat base unit. Previously, the 1 mL of biiodate had been added using a manual dispenser. "Hydro" was modified in the handling of sample repeats. It now has the first value as the default value.

As with other cruises there were problems with standardising to WOCE precision. One of the Optifix dispensers had had some extra tubing placed on the end of the tip. Taking this off seemed to improve precision. As has been noted previously, a second Dosimat base unit for dispensing standards would improve the procedure.

Standardisations are shown in Figure A2.1.6 of Appendix 2.1.

## A3.1.4 LABORATORIES

Nutrients, salinities, and dissolved oxygens were analysed in the wet lab, with water purification in the 'photolab.' Nutrients and salinities were performed on the aft bench, on the inboard and outboard sides respectively. Dissolved oxygens were performed over the inboard sink.

# A3.1.5 TEMPERATURE CONTROL AND MEASUREMENT

There were two temperature control units. The first was the lab air conditioner. This was set at around 19°C. The second was the PID temperature controller, which had a set point of 20.1°C. The temperature sensor was placed above the salinity crates. The ships air conditioning outlets above the instruments were taped closed. The sea door access to the trawl deck was kept shut. Laboratory temperature was recorded by two Tinytalk units, and measured by two mercury thermometers, an electronic thermometer, and the temperature monitor of the PID controller. An 'indoor/outdoor' electronic thermometer was used to measure fridge and freezer temperatures. One Tinytalk was positioned above the salinity crates for the duration of analysis, the other was moved around for shorter checks. One mercury thermometer was positioned above the salinity crates, the other with the DO instrumentation. An electronic thermometer was also used for spot checks. All the temperature measuring devices were placed together at the start of the cruise. The PID temperature was calibrated, and the devices agreed to within 0.5°C.

The mercury thermometer with the DO instrumentation was in the range of 19.5 to 20.5°C.

The long term Tinytalk recorded 1342 temperature points at 24 minute intervals. The average temperature was 20.9 +/- 0.4  $^{\circ}$ C. See Figure A3.1.1 and Table A3.1.1. There was some spatial variation, which had a range of +/-  $2^{\circ}$ C among the instrument locations. This was from the bench top to the height of the top of the salinometer.

<u>Table A3.1.1:</u> Laboratory temperature recorder statistics.

Temperature statistics from Tinytalk						
average	20.9					
stdev	0.4					
%rsd	1.7					
Min	19.6					
Max	22.0					
range	2.4					
% range	11.5					

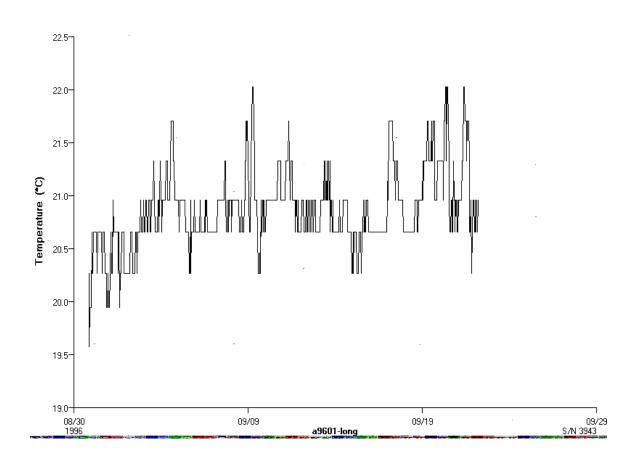


Figure A3.1.1: 'Tinytalk' temperature plot, 24 minute time resolution.

<u>Table A3.1.2:</u> Nutrient samples run as quality checks.

A9601					1	1	
QC's extracted					-		
QC S extracted	Run	NO3+NO2	_	Sil	_	Phos	
	Kuli		uM	Volts	uM		uM
	-	Volts	uivi	VOIIS	uivi	Volts	uivi
	_		20.52	_	20.22		1.07
average	_		30.52	_	39.32		1.97
stdev			0.54		0.70		0.05
%rsd		+	1.8		1.8	_	2.7
			00.47		37.57		4.00
min		+	29.47			_	1.88
max			31.94		40.91	-	2.11
range			2.46		3.33	-	0.23
Range%			8.1		8.5		11.6
A9601004.ACM	4	2.62	31.0	2.66	39.9	2.49	1.98
	4						
A9601004.ACM A9601005.ACM	5	2.59	30.6	2.66	40.0 39.8	2.49	1.97
			30.9	2.66			1.96
A9601005.ACM	5	2.47	30.1	2.66	39.8	2.48	1.96
A9601006.ACM	6	2.55	31.0	2.59	40.3		1.93
A9601006.ACM	6	2.49	30.1	2.58	40.0	0.40	1.92
A9601007.ACM	7	5.31	30.8	2.58	38.9	2.42	1.98
A9601007.ACM	7	5.22	30.2	2.60	39.2	2.47	2.04
A9601008.ACM	8	5.21	30.2	2.58	38.5	2.42	1.97
A9601008.ACM	8	5.45	31.9	2.62	39.5	2.44	2.00
A9601010.ACM	10	5.57	30.7	2.51	39.0	2.47	2.05
A9601010.ACM	10	5.65	31.2	2.55	40.0	2.52	2.10
A9601015.ACM	15	5.84	31.4	2.67	39.3	2.78	2.11
A9601015.ACM	15	5.76	31.0	2.65	39.7	2.78	1.94
A9601015.ACM	15	5.74	30.8	2.69	40.5	2.79	1.95
A9601016.ACM	16	5.71	30.2	2.56	38.8	2.62	1.94
A9601016.ACM	16	5.87	31.2	2.60	39.9	2.71	2.03
A9601016.ACM	16	5.66	29.9	2.58	39.3	2.58	1.89
A9601016.ACM	16	5.79	30.7	2.65	40.9	2.67	2.00
A9601017.ACM	17	5.57	31.4	2.51	38.1	2.69	1.97
A9601017.ACM	17	5.55	31.3	2.49	37.6	2.67	1.95
A9601019.ACM	19	5.57	29.5	2.33	38.9	2.61	1.91
A9601019.ACM	19	5.71	30.4	2.32	38.6	2.66	1.97
A9601021.ACM	21	5.63	30.4	2.51	38.8	2.56	1.89
A9601021.ACM	21	5.59	30.1	2.50	38.6	2.56	1.89
A9601022.ACM	22	5.71	30.4	2.44	39.1	2.57	1.90
A9601022.ACM	22	5.68	30.2	2.43	38.8	2.54	1.88
A9601023.ACM	23	5.40	30.2	2.52	38.4	2.64	1.95
A9601023.ACM	23	5.34	29.8	2.53	38.6	2.62	1.93
A9601051.ACM	51	5.66	30.0	2.71	39.2	2.67	2.00
A9601051.ACM	51	5.66	30.0	2.71	39.2	2.66	1.99
A9601051.ACM	51	5.65	30.0	2.66	39.9	2.49	1.98
A9601051.ACM	51	5.62	29.8	2.66	40.0	2.49	1.97
A9601052.ACM	52	5.67	30.5	2.66	39.9	2.80	2.01
A9601052.ACM	52	5.72	30.8	2.66	40.0	2.82	2.03
A9601053.ACM	53	5.68	30.4	2.58	38.9	2.75	2.01
A9601053.ACM	53	5.68	30.4	2.60	39.2	2.74	1.99
A9601053.ACM	53	5.70	30.5	2.62	39.5	2.78	1.97
A9601053.ACM	53	5.69	30.5	2.60	39.1	2.76	1.94

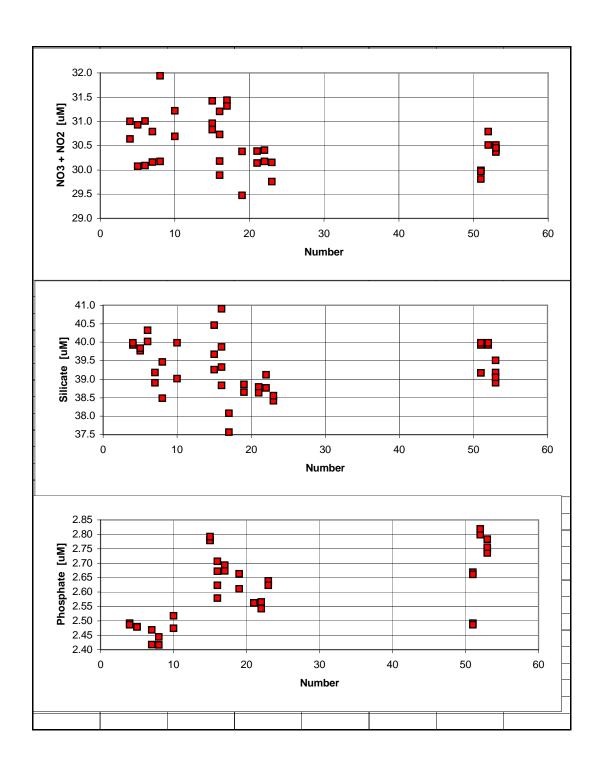


Figure A3.1.2: Nutrient samples run as quality checks.

Calibration of	Guildline s	alinometer					
SN 62 549							
0.01 = 1-2  co	unts on std	dial=0.002-	0.004 psu				
			<b>-</b>				
Date	Std	Lab	Sal	IAPSO	Nom	Nom	Location
		temp	temp	batch	Sal	Sal	
		p			1R	2R	
13-Aug-96	4.49	19		P126	0.99987	1.99974	CSIRO
24-Aug-96		18		P126	0.99987		
25-Aug-96			21	P128	0.99986	1.99972	
29-Aug-96				P128	0.99986		
1-Sep-96			21	P128	0.99986		
2-Sep-96	4.58			P128	0.99986	1.99972	
3-Sep-96	4.57			P128	0.99986	1.99972	
4-Sep-96	4.49	20.1	21	P128	0.99986	1.99972	
7-Sep-96	4.44	20.1	21	P128	0.99986	1.99972	
9-Sep-96	4.52	20.1	21	P128	0.99986	1.99972	
9-Sep-96	4.61	20.1	21	P130	0.99997	1.99994	
10-Sep-96	4.61	20.1	21	P130	0.99997	1.99994	
11-Sep-96	4.603	20.1	21	P130	0.99997	1.99994	
12-Sep-96	4.55	20.1	21	P130	0.99997	1.99994	
13-Sep-96	4.55	20.1	21	P130	0.99997	1.99994	
14-Sep-96	4.57	20.1	21	P130	0.99997	1.99994	
15-Sep-96	4.59	20.1		P130	0.99997	1.99994	
17-Sep-96	4.49	20.1	21	P130 0.999		1.99994	
18-Sep-96	4.525	20.1		P130 0.99997		1.99994	
20-Sep-96	4.525	20.1	21	P130 0.99997		1.99994	
21-Sep-96	4.525	20.1	21	P130 0.99997		1.99994	
4.65							
4.6					···		
4.55					<del>_</del> +		
4.5 🙀 🤆	SIRO						
4.45		■ A9	601				<u> </u>
4.4				<del>- T</del>			<u> </u>
13-	18-	23- 2		o- 7-Sep-	12-	17- 22-	
		Aug-96 Aug		•	Sep-96 Se		

Figure A3.1.3: Salinometer standardisation values.

		, , ,		y c. uc	uble conductiv	,								
Looks at standardisations on A9601. Sal standardised with one std, and the other one then measured.														
Sal star	dardise	ed with or	ne std, and th	e other or	e then measu	red.								
Sheet	Std.	Std	Measured	Stdise	Measured val	ue		Nominal value			Diff (meas-n	om)	Diff, abs	
	num.			value	R	2R	Т	R	2R	psu	2R	psu	psu	
16	1	P128	P130	4.44	0.99993	1.99985	21	0.99997	1.99994	34.999	-0.00009	-34.9988	34.9988	
16		P128	P130	4.44		1.99985	21	0.99997	1.99994		-0.00009	-34.9988		
21	3	P128	p130	4.44	0.99993	1.99985	21	0.99997	1.99994	34.999	-0.00009	-34.9988	34.9988	
22	3	P128	p130	4.52	0.99993	1.99986	21	0.99997	1.99994	34.999	-0.00008	-34.9988	34.9988	
25	3	P130	p128	4.61	0.99990	1.99979	21	0.99986	1.99972	34.994	0.00007	-34.9945	34.9945	
	4	p130	p128	4.61	0.99992	1.99983	21	0.99986	1.99972	34.994	0.00011	-34.9945	34.9945	
29	3	p130	p128	4.61	0.99992	1.99983	21	0.99986	1.99972	34.994	0.00011	-34.9945	34.9945	
29	4	p130	p128	4.61	0.99991	1.99982	21	0.99986	1.99972	34.994	0.00010	-34.9945	34.9945	
												av	34.9967	•
P128 is	0.0018	+/- 0.000	3 psu higher	than P13	0							stdev	0.0023	
	1											%rsd	0	%

Table A3.1.3: Comparison of ISS batches P128 and P130.

## Part 4

# Aurora Australis Southern Ocean Oceanographic Cruises, 1991 to 1996 - Inter-cruise Comparisons and Data Quality Notes

## 4.1 INTRODUCTION

Marine science cruise AU9601 aboard the RSV Aurora Australis was the seventh and last in a series of oceanographic cruises from 1991 to 1996, taking CTD measurements along Southern Ocean transects, mostly under the WOCE program (Table 4.1). In this part of the report, brief data comparisons are made between the cruises, and data quality notes relevant to the cruise set are discussed.

<u>Table 4.1:</u> RSV Aurora Australis Southern Ocean oceanographic cruises, 1991 to 1996. Note the following: PET=Princess Elizabeth Trough section, FORMEX=Formation Experiment, MARGINEX=Antarctic Margin Experiment; au9309 and au9391 were part of the same cruise; the southern end of SR3 was occupied as part of MARGINEX.

cruise	transect	occupation date	direction of occupation
au9101 au9309 au9391 au9407 au9407 au9404 au9404 au9501 au9501 au9604 au9601	SR3 (WOCE) SR3 (WOCE) P11 (WOCE) SR3 (WOCE) PET S4 (WOCE) SR3 (WOCE) SR3 (WOCE) FORMEX MARGINEX SR3 (WOCE)	October 1991 March 1993 April 1993 January 1994 January 1994 Dec. 1994 - Jan. 1 January-February July-August 1995 August 1995 January-March 19	1995 south to north north to south  - 96 -
ausoul	SINS (WOCL)	August-Septembe	300011010111

# 4.2 INTER-CRUISE DATA COMPARISONS

In this section, a brief comparison of salinity, dissolved oxygen and nutrient data is made between the seven cruises. Most of the discussion refers to data from the SR3 section. The primary aim of the comparison is to assess the inter-cruise compatibility of measurements and data quality for the entire data set. Comparisons with earlier data sets are discussed in Rosenberg et al. (1995a).

## 4.2.1 Salinity

## Inter-cruise comparisons

Inter-cruise salinity comparisons in earlier data reports (Rosenberg et al., 1995a, 1995b and 1996) revealed significant variation in salinity measurements for the different cruises. The YeoKal salinometers used (Table 4.2) were identified as the most likely source of error. For cruise AU9601, the last cruise in the series, a Guildline salinometer was used for the first time, with a manufacturer-quoted salinity accuracy of 0.001 (PSS78) as compared to 0.003 (PSS78) for the YeoKal instruments. As a result, high quality CTD salinity data were obtained for this cruise (see Part 3 of this report). To assess inter-cruise errors in salinity measurements, salinity data from each cruise are compared to

data from AU9601. Specifically, the meridional variation of the salinity maximum (i.e. for Lower Circumpolar Deep Water as defined by Gordon, 1967) along the SR3 section for each cruise is compared to the equivalent values for AU9601 (Figures 4.1a and b). For the comparison, 2 dbaraveraged CTD data are used i.e. CTD salinity at the nearest 2 dbar bin to the salinity maximum for each station. Note that in the Figure 4.1 comparison of cruises au9601 and au9101, au9601 data are linearly interpolated to the au9101 station positions. For the other cruises in the figure, salinity differences are only formed between station pairs which are separated by less than 1.5 nautical miles of latitude.

<u>Table 4.2:</u> Summary of International Standard Seawater (ISS) batches and salinometers used for salinity sample analyses on cruises, including RV Melville cruise me9706.

cruise	ISS batch number (+ date)	station numbers
au9101	P115 (6th Feb. 1991)	1-35
au9309	P121 (8th Sept. 1992)	1-63
au9391	P121 (8th Sept. 1992)	1-64
au9407	P123 (10th June 1993)	1-79
au9407	P121 (8th Sept. 1992)	80-102
au9404	P123 (10th June 1993)	1-85
au9404	P121 (8th Sept. 1992)	86-107
au9501	P126 (29th Nov. 1994)	1-208
au9604	P128 (18th July 1995)	1-25, 69-74, 110-145
au9604	P126 (29th Nov. 1994)	26-68, 75-109
au9601	P128 (18th July 1995)	1-23
au9601	P130 (21st March 1996)	24-69
me9706	P130 (21st March 1996)	2-49
cruise	salinometer serial number	station numbers
Ciuise	danifornotor dorial flambor	olation nambors
au9101	601003 (YeoKal)	1-35
	601003 (YeoKal) 601003 (YeoKal)	
au9101	601003 (YeoKal)	1-35
au9101 au9309	601003 (YeoKal) 601003 (YeoKal)	1-35 1-63
au9101 au9309 au9391	601003 (YeoKal) 601003 (YeoKal) 601003 (YeoKal)	1-35 1-63 1-64
au9101 au9309 au9391 au9407	601003 (YeoKal) 601003 (YeoKal) 601003 (YeoKal) 601855 (YeoKal) 601003 (YeoKal) 601855 (YeoKal)	1-35 1-63 1-64 1-86
au9101 au9309 au9391 au9407 au9407	601003 (YeoKal) 601003 (YeoKal) 601003 (YeoKal) 601855 (YeoKal) 601003 (YeoKal)	1-35 1-63 1-64 1-86 87-102 1-107 1-208
au9101 au9309 au9391 au9407 au9407 au9404	601003 (YeoKal) 601003 (YeoKal) 601003 (YeoKal) 601855 (YeoKal) 601003 (YeoKal) 601855 (YeoKal)	1-35 1-63 1-64 1-86 87-102 1-107
au9101 au9309 au9391 au9407 au9407 au9404 au9501	601003 (YeoKal) 601003 (YeoKal) 601003 (YeoKal) 601855 (YeoKal) 601003 (YeoKal) 601855 (YeoKal) 601830 (YeoKal)	1-35 1-63 1-64 1-86 87-102 1-107 1-208
au9101 au9309 au9391 au9407 au9407 au9404 au9501 au9604	601003 (YeoKal) 601003 (YeoKal) 601003 (YeoKal) 601855 (YeoKal) 601003 (YeoKal) 601855 (YeoKal) 601830 (YeoKal) 601003 (YeoKal)	1-35 1-63 1-64 1-86 87-102 1-107 1-208 1-23, 43-47, 139-141
au9101 au9309 au9391 au9407 au9407 au9404 au9501 au9604 au9604	601003 (YeoKal) 601003 (YeoKal) 601003 (YeoKal) 601855 (YeoKal) 601855 (YeoKal) 601830 (YeoKal) 601003 (YeoKal) 601439 (YeoKal) 601440 (YeoKal)	1-35 1-63 1-64 1-86 87-102 1-107 1-208 1-23, 43-47, 139-141 24-25
au9101 au9309 au9391 au9407 au9407 au9404 au9501 au9604 au9604	601003 (YeoKal) 601003 (YeoKal) 601003 (YeoKal) 601855 (YeoKal) 601003 (YeoKal) 601855 (YeoKal) 601830 (YeoKal) 601003 (YeoKal) 601439 (YeoKal) 601855 (YeoKal)	1-35 1-63 1-64 1-86 87-102 1-107 1-208 1-23, 43-47, 139-141 24-25 26-42, 48-68, 142-145
au9101 au9309 au9391 au9407 au9407 au9404 au9501 au9604 au9604 au9604	601003 (YeoKal) 601003 (YeoKal) 601003 (YeoKal) 601855 (YeoKal) 601855 (YeoKal) 601830 (YeoKal) 601003 (YeoKal) 601439 (YeoKal) 601439 (YeoKal) 601440 (YeoKal) 62549 (Guildline)	1-35 1-63 1-64 1-86 87-102 1-107 1-208 1-23, 43-47, 139-141 24-25 26-42, 48-68, 142-145 69-138
au9101 au9309 au9391 au9407 au9407 au9404 au9501 au9604 au9604 au9604 au9604	601003 (YeoKal) 601003 (YeoKal) 601003 (YeoKal) 601855 (YeoKal) 601855 (YeoKal) 601830 (YeoKal) 601003 (YeoKal) 601439 (YeoKal) 601440 (YeoKal) 601440 (YeoKal) 62549 (Guildline)	1-35 1-63 1-64 1-86 87-102 1-107 1-208 1-23, 43-47, 139-141 24-25 26-42, 48-68, 142-145 69-138 1-69

The following approximate mean salinity differences for data along the SR3 transect at the deep salinity maximum are evident from Figures 4.1 and 4.2:

cruise comparison	approximate mean salinity difference (PSS78)
au9601-au9101	-0.005 (south of ~49.5°S)
au9601-au9309	-0.008
au9601-au9407	-0.001
au9601-au9404	-0.004
au9601-au9501	0.001
au9601-au9604	insufficient data for comparison
au9601-me9706	-0.002

These values summarise the inter-cruise compatibility of salinity data. No significant correlation is evident between ISS batch numbers used and the observed salinity differences between cruises, and the salinometers remain the most likely source of error. A further partial occupation of the SR3 transect down to 57°S was made by the RV Melville in March to April 1997 (cruise me9706, principal investigators R.Watts, S. Rintoul, J. Richman, B. Petit, D. Luther, J. Filloux, J. Church, A. Chave). Guildline salinometers were used for salinity analyses (Table 4.2), with the hope of determining whether inter-cruise compatibility improves using these more stable salinometers. Comparing the meridional variation of the deep water salinity maximum for cruises au9601 and me9706 (Figure 4.2), a mean difference au9601-me9706 of ~-0.002 is clearly observed. This difference is less variable than for other cruises (Figure 4.1), due to stable performance of the Guildlines. Nevertherless this difference is clearly significant, and indicates that 0.002 (PSS78) is at the limit of achievable salinity accuracy when comparing different cruises.

# Small scale variance of salinity signal

Close examination of vertical CTD profiles reveals a small scale structuring, at vertical scales of the order 2 dbar, which is not consistent between different cruises. To assess whether this variability is a real oceanic feature, salinity and temperature vertical profile data variance was investigated for all cruises, as follows. Vertical salinity and temperature 2 dbar-averaged profiles were smoothed by calculating a running mean of width 12 dbar (i.e. ±3 pressure bins), centered on each pressure bin. A mean "variance" V around the smoothed profiles was then calculated for each vertical salinity profile (and similarly for temperature):

$$V_s = \left[\sum_{i=1001}^{\text{bottom}} (|s_{\text{smooth}} - s|)_i\right] / n$$
 (eqn 4.1)

for  $s_{smooth}$  the smoothed salinity, the ith 2 dbar pressure bin, and n equal to the number of 2 dbar pressure bins from 2002 dbar to the bottom of the profile. Note that only data below 2000 dbar were examined, to avoid steep vertical gradients and regions of high mixing. To allow a realistic comparison between different cruises, equivalent station positions along the SR3 transect were investigated. Variances were calculated for stations lying within the two latitude ranges 45 to  $50^{\circ}$ S and 54 to  $58^{\circ}$ S - choice of these two latitude ranges excludes stations lying within the major frontal regions where greater inter-cruise variability might occur. (Note that cruise aug391 is an exception, as it lies along the P11 transect - for this cruise, significant horizontal frontal structure was observed in the 54 to  $58^{\circ}$ S latitude range, and the results are not directly comparable to SR3 data.) The results in Table 4.3 show values of  $V_s$  and  $V_t$  (for salinity and temperature respectively) averaged over the specified station groups for each cruise.

<u>Table 4.3:</u> Vertical variance of CTD salinity and temperature data below 2000 dbar, for given latitude ranges along the SR3 transect (with the exception of cruise au9391, along the P11 transect). For the CTD's, "B" and "C" indicate a MarkIIIB and MarkIIIC respectively. "c-cell" is the condition of the CTD conductivity cell.

		latitude 45°S	to 50°S			latitud	e 54°S to	58°S	
cruise	stn	CTD c-cell	mean V <sub>s</sub>	mean V <sub>t</sub>	stn	CTD	c-cell	mean V <sub>s</sub>	mean V <sub>t</sub>
	nos.	no.	(PSS78)	(°C)	nos.	no.		(PSS78)	(°C)
au9309	6-15	1197B used	0.00031	0.00089	25-33	1197B	used	0.00031	0.00082
au9391	19-28	1073B used	0.00022	0.00065	37-44	1073B	used	0.00024	0.00079
au9407	7-22	2568C used	0.00026	0.00086	34-45	2568C	used	0.00025	0.00072
au9404	92-102	1193C suspect	0.00025	0.00087	74-80	1193C	suspect	0.00038	0.00076
au9501	6-17	1103C new	0.00047	0.00078	30-37	1193C	suspect	0.00023	0.00070
au9601	46,54-64	11103C new	0.00045	0.00083	25-33	1103C	new	0.00041	0.00071
me9706	3-4,6-7,								
	40-43	1013B new	0.00024	0.00087	19-26	1013B	new	0.00028	0.00078

 $V_s$  values are unlikely to be affected by pressure noise. Firstly, if any noise is present in the raw pressure signal, this would be averaged out in the 2 dbar binning. Moreover for CTD 1103, where the highest  $V_s$  values occur, the pressure signal is significantly less noisy than for other instruments. Secondly, for casts taken in either calm conditions or in the ice, and where pressure reversals are therefore minimal, no drop in  $V_s$  values are evident.

 $V_t$  values within each latitude range are fairly consistent between cruises compared with  $V_s$  values, which show much more variation. In particular,  $V_t$  values are consistently lower in the 54-58°S region than in the 45-50°S region - this suggests that the fine structure is a real measurement, not an electronic artifact of the instrumentation.

The magnitude of V<sub>s</sub> appears to be dependent on:

- \* the magnitude of V<sub>1</sub>:
- \* the condition of the conductivity cell;
- \* the particular instrument in use.

Firstly, inspection of individual stations reveals that when  $V_s$  exceeds a certain threshold level, there is a strong dependence of  $V_s$  on the magnitude of  $V_t$  (Figure 4.3). Below this value, there is no significant dependence. This however does not account for the high inter-cruise variation of  $V_s$  evident in Table 4.3. The results for cruise au9501 (Figure 4.4) demonstrate a dependence of  $V_s$  on the condition of the conductivity cell:  $V_s$  is significantly higher for the 45-50°S latitude range where a new cell is in use, compared to the southern stations where a suspect cell was used. In addition, comparing the 54-58°S values for cruises au9501 and au9601,  $V_t$  values are comparable, whereas  $V_s$  is much lower for the suspect conductivity cell. In fact from Figure 4.3, there is a different dependency of  $V_s$  on  $V_t$  for the suspect conductivity cell. Lastly, there also appears to be a dependence of  $V_s$  on the instrument in use. The most striking difference is between  $V_s$  values for cruises me9706 and au9601, even though new conductivity cells were used in both cases (and note that  $V_t$  values for the two cruises are comparable). Apparently some instruments are more reponsive than others - this may be related to differences between MarkIIIB and MarkIIIC CTD's, or simply differences between individual instruments.

To summarise, new conductivity cells appear to be more responsive to fine structure in the water column, however the quantitative value of small scale vertical salinity variations may also depend on the CTD in use. In more extreme cases, this fine structure includes small vertical density inversions, with typical magnitudes in the range 0.001 to 0.005 kg.m<sup>-3</sup>.

## 4.2.2 Dissolved oxygen

Dissolved oxygen bottle data along the SR3 transect for cruises au9407 and onwards are compared in Figures 4.5a and b. For all these cruises, oxygen bottle samples were analysed using the automated titration system developed by Woods Hole Oceanographic Institution (Knapp et al., 1990). Data from the earlier cruises au9101, au9309 and au9391, where samples were analysed using a manual titration method (Eriksen and Terhell, in prep.), are discussed in previous data reports (Rosenberg et al., 1995a and b). Note that in Figure 4.5, axes limits do not include the entire data set, focussing rather on deep and intermediate water masses to allow easier visual comparison between cruises. Also note that for cruise au9604, data from the longitude range 128 to 150°E are plotted to provide more points for comparison.

In summary, the following dissolved oxygen data appear to be consistent:

au9407 au9404 au9501 stations 22 and onwards au9604 au9601 stations 41 and onwards The following inconsistencies are apparent:

```
au9501 stations 1-21: values smaller by \sim 6\mumol/l au9601 stations 1-40: values larger by \sim 4\mumol/l
```

Note that the above deviation values are approximate averages only - deviations for individual samples may vary slightly with the magnitude of dissolved oxygen concentration. Examination of standardisation values for the laboratory analyses reveals the source of error: for cruise au9501, a drift in standardisation values was noted up until station 21, however restandardisations were not carried out; for cruise au9601, a jump in standardisation values occurred after station 40 (see Appendix 3.1). Clearly, standardisation values for dissolved oxygen analyses must be examined more closely during future cruises.

#### 4.2.3 Nutrients

## Phosphate and nitrate+nitrite

Phosphate and nitrate+nitrite data for cruises au9404 and onwards are compared in Figure 4.6 while data for all cruises are summarised in Figure 4.7. Note that the inconsistent results for cruise au9101 (Figure 4.7), due to higher phosphate values, are discussed in Rosenberg et al. (1995a).

The nitrate+nitrite to phosphate ratio is mostly consistent for cruises au9309 and au9407 (Figure 4.7), and for cruises au9404, au9501 and au9604 (Figures 4.6a and b); however the ratio differs for cruise au9601 (Figure 4.6c). Comparison of vertical nutrient profiles at equivalent station positions for different cruises reveals that the difference is due to phosphate, rather than nitrate+nitrite data. Phosphate values for au9601 are lower than the values for other cruises by ~0.1µmol/l. As discussed in Appendix 3.1 of this report, the phosphate carryover effect is believed to have been minimised for cruise au9601 by alterations to the analysis techniques. For au9601, the autoanalyser peaks for phosphate analyses very nearly return to the baseline level from where peak integration occurs, minimising any carryover error. For previous cruises, autoanalyser peaks for phosphate analyses do not return all the way to the baseline level. This carryover error artificially increases peak height values, and could be a cause for slightly higher phosphates for previous cruises compared to au9601. Note that the offset is unlikely to be a constant - there may be a dependence on phosphate concentration, and on instrument settings. Phosphate measurements on future cruises using the same techniques as for cruise au9601 will confirm whether the observed difference of ~0.1µmol/l in Figure 4.6c does indeed represent an error in all the previous cruises.

# Near surface phosphate and nitrate+nitrite

From Figure 4.6b, the near surface nutrient data for au9604 clearly differs from the remaining data. Moreover, the lower the near surface nutrient value, the greater the deviation from the bestfit line. From inspection of all the cruises (Figure 4.7), this feature is apparent for data collected in Antarctic waters (i.e. south of the Polar Front) during the austral summer i.e. cruises au9407, au9404 and au9604. In addition, the feature can be seen in summer data collected by the Eltanin (Gordon et al., 1982) (Figure 4.7) along a meridional transect at 132°E. There are two possible explanations for the feature:

- (a) the phosphate carryover error, discussed in previous data reports (see section 6.2.1 in Rosenberg et al., 1995b), results in depressed phosphate values near the surface; this error is amplified where vertical phosphate gradients are steep, as is the case for near surface Antarctic waters during an austral summer;
- (b) alternatively, the feature is real, indicating a stronger depletion of phosphate relative to nitrate+nitrite by biological activity in Antarctic waters during the summer.

Note that for cruises au9407 and au9404, many surface phosphate samples were bad due to the phosphate carryover effect, and much of the relevant nitrate+nitrite to phosphate ratio data are missing for these cruises. Whether explanation a or b applies is inconclusive. As already discussed, the phosphate carryover error is believed to have been minimised for cruise au9601. Thus to confirm whether the near surface phosphate depletion is an error or a real feature, more summertime Antarctic zone nutrient data are needed using the analysis techniques of cruise au9601.

## Matrix correction

For analysis of nutrients, samples are initially run against nutrient standards (see Appendix 3, Rosenberg et al., 1995b). The colour reagent is then removed, and samples are run again against the nutrient standards. The peak observed when run without the colour reagent is due mainly to a "matrix effect" (i.e. a detector response due to refractive properties of the sample water), and should be corrected for. The size of the matrix effect is dependent on chemistry and detection wavelength. Ideally, the magnitude of the effect should be checked for each nutrient sample. For cruise au9601, the effect was negligible for nitrate+nitrite and silicate analyses, however a significant effect was observed for phosphates. A mean magnitude of the matrix effect for phosphates was obtained by measuring the effect for two vertical phosphate profiles, from the north and south ends of the transect. The value, equal to  $0.088~\mu mol/l$ , should be subtracted from au9601 phosphate if the matrix effect correction is desired. Note that the matrix effect was not investigated for previous cruises, so to maintain consistency of the entire data set, the correction has not been applied to cruise au9601.

## Silicate

Silicate data along the SR3 transect for cruises au9309 and onwards are compared in Figure 4.8. Note that most of the comparisons are for stations outside the strong frontal regions. Most of the silicate data for the different cruises agree to within 5  $\mu$ mol/l, and in general no consistent offset between cruises is evident.

#### 4.2.4 Pressure

Small differences in the quality of CTD pressure data between different cruises occurs according to the CTD instrument in use. The two fundamental differences in instruments are as follows:

- (i) MarkIIIB CTD's employ a stainless steel type strain gauge for measuring pressure; there is no pressure temperature correction, and separate downcast and upcast laboratory calibrations are used to compensate for hysteresis of the pressure response. The more accurate WOCE upgraded MarkIIIC CTD's use a titanium type strain gauge, and include a pressure temperature correction the hysteresis of these sensors is small compared with the stainless steel type, and a downcast laboratory calibration only is applied to all pressure data. The manufacturer quoted accuracies of pressure data from the two types of pressure sensor are ±6.5 dbar for the Mark IIIB units (used for cruises au9101, au9309 and au9391), and ±1.2 dbar for the Mark IIIC's (used for all remaining cruises).
- (ii) The level of noise in the raw pressure signal differs for the different instruments. In general, the titanium type sensors in the MarkIIIC's display a higher noise level than the stainless steel type in the MarkIIIB's (Millard et al., 1993), and a small error may be introduced into surface pressure offset values, as described in previous data reports. Of the MarkIIIC's used, CTD 1193 was noisiest and CTD 2568 a little less so; both however were significantly noisier than CTD 1103. This pressure signal noise, up to 1 dbar in amplitude for CTD 1193, can result on occasion in 2 dbar pressure bins (for the pressure monotonically increasing data files) with too few raw data points for the formation of a 2 dbar average (see CTD methodology in Rosenberg et al. 1995b for pressure calculations). For details on individual cruises, and information on which instruments were used, see the data reports for each cruise.

## 4.2.5 Temperature

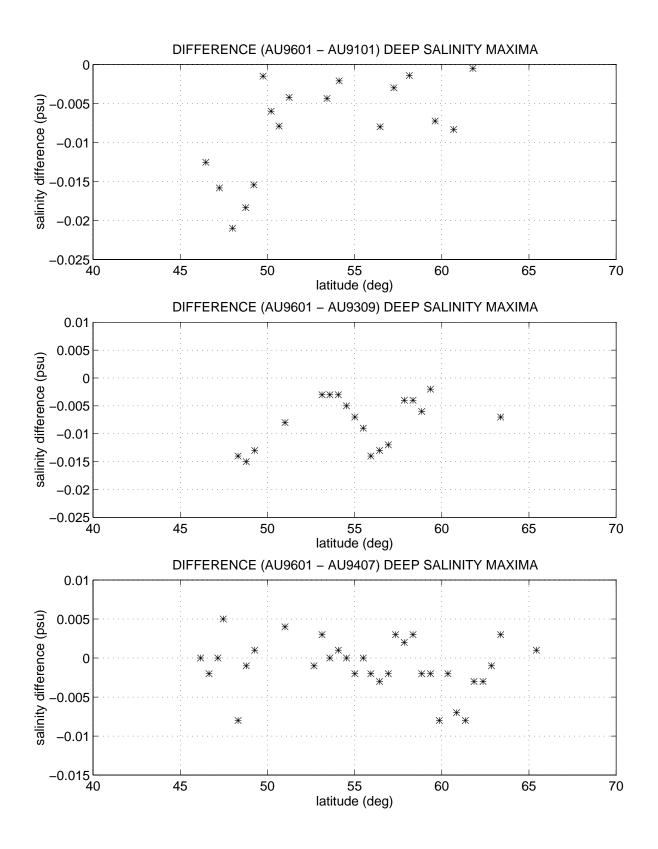
Comparison of calibrated CTD platinum temperature data  $T_{cal}$  to mercury reversing thermometer measurements  $T_{therm}$  on all the cruises allows the inter-cruise compatibility of temperatures to be assessed. Note that the same laboratory calibrations were applied to the reversing thermometers for all cruises, although a different set of thermometers was used for cruises au9309/au9391. Reversing thermometer calibrations are assumed to remain stable over the entire period. Moreover, the thermometer to CTD comparison for different cruises shows the same variation for the different thermometers used, supporting the assumption of stable thermometer calibrations. Thus any temperature errors are attributed to calibration problems for the CTD platinum temperature. For cruise au9101, insufficient thermometer measurements were made for a check of CTD temperature.

Although manufacturer quoted accuracies for the reversing thermometers are only of the order  $0.01^{\circ}\text{C}$ , thermometer resolution is usually significantly better; and given the reasonably large number of data points obtained, it is estimated that CTD temperature performance can be assessed to an accuracy of  $\sim 0.003^{\circ}\text{C}$ . Mean differences ( $T_{\text{therm}}$  -  $T_{\text{cal}}$ ) are summarised in Table 4.4. The following CTD temperature calibration problems are evident:

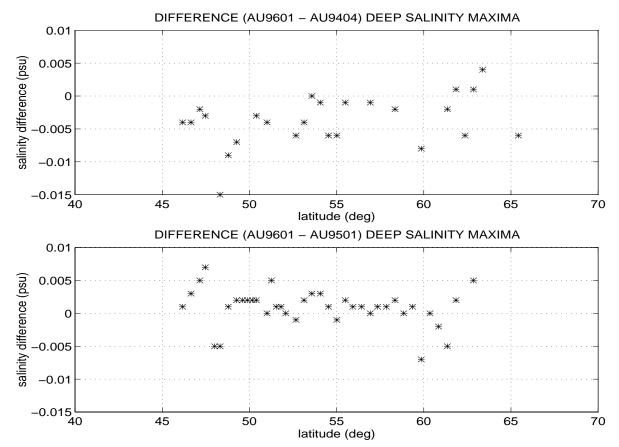
- (i) For the first half of cruise au9309, the CTD temperature is incompatible with other cruises by >0.01°C.
- (ii) For cruise au9501 where CTD 1103 was used, there is a CTD temperature calibration error of ~0.007°C (the post cruise CTD temperature calibration was used). Pre and post cruise temperature calibrations were significantly different, and a temperature error occurs when either calibration is applied (see au9501 data report).
- (iii) For cruise au9601, the difference value of ~0.005°C is large enough to be significant. In this case, a pre cruise calibration was used.
- (iv) For cruise au9407, the temperature calibration is good, except for an apparent non-linearity at lower temperatures (stations 61-82). See Rosenberg et al. (1995b) for more details.
- (v) For cruise au9404, a CTD temperature calibration error was apparent for CTD 1193 (stations 19-106). A constant correction of -0.007°C was applied to all CTD temperature data. Some error may however remain due to this assumption of a constant offset.

 $\underline{\text{Table 4.4:}}$  Mean and standard deviation of temperature residual ( $T_{\text{therm}}$  -  $T_{\text{cal}}$ ) for different cruises.

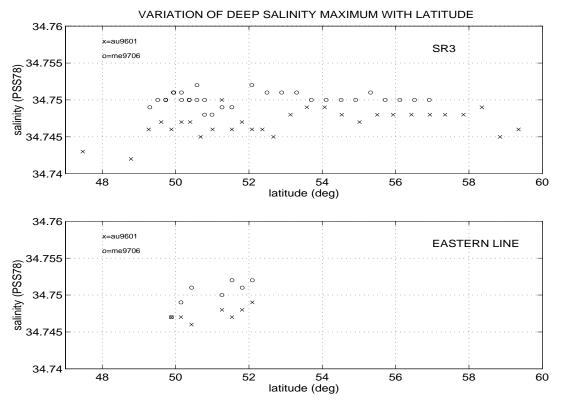
cruise (station nos.)	CTD no.	mean of (T <sub>therm</sub> - T <sub>cal</sub> ) (deg. C)	standard dev. of $(T_{therm} - T_{cal})$ (deg. C)	no. of samples
au9309 (1-35)	1197	-0.0139	0.0110	51
au9309 (36-63)/au9391 (1-63)	1073	-0.0022	0.0109	121
au9407 (1-60 and 83-102 only)	2568	0.0014	0.0131	95
au9404 (1-106)	1193/1103	0.0017	0.0090	243
au9501 (1-29,46-103,106-208)	1103	-0.0071	0.0078	155
au9501 (30-45)	1193	0.0011	0.0041	33
au9604 (1-147)	1103/1193	0.0019	0.0068	289
au9601 (1-71)	1103/1193	0.0046	0.0050	187



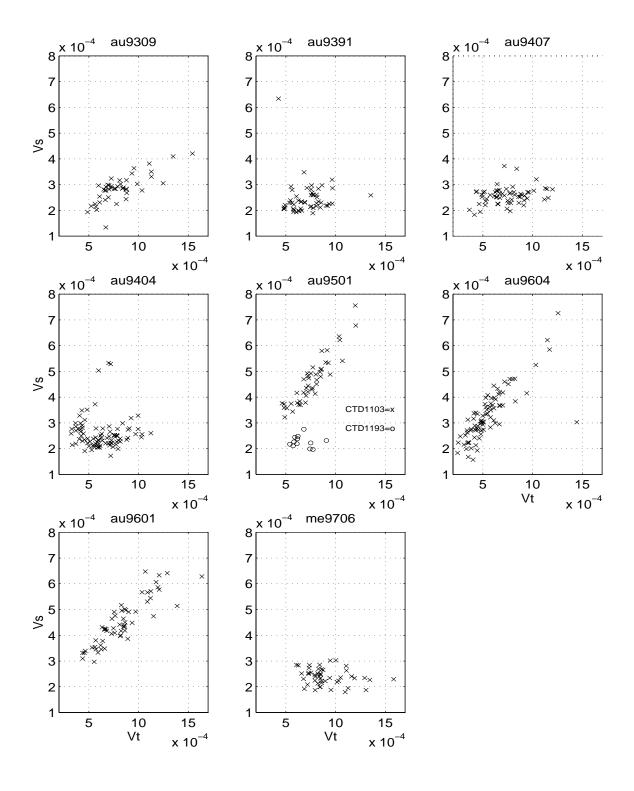
<u>Figure 4.1a:</u> Variation south along the SR3 transect of the deep salinity maximum: salinity differences between cruise au9601 and cruises au9101, au9309 and au9407. For au9101 comparison, au9601 values are linear interpolations between station positions; for cruises au9309 and au9407 comparisons, differences are only formed between station pairs separated by no more than 1.5 nautical miles of latitude.



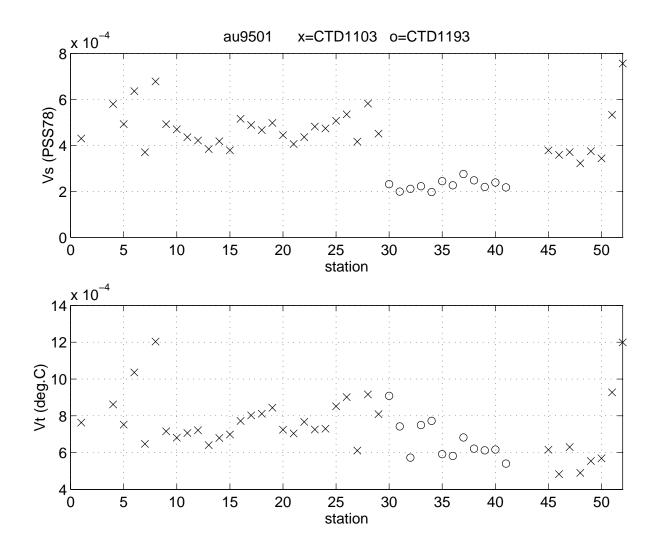
<u>Figure 4.1b:</u> Variation south along the SR3 transect of the deep salinity maximum: salinity differences between cruise au9601 and cruises au9404, au9501. Differences are only formed between station pairs separated by no more than 1.5 nautical miles of latitude.



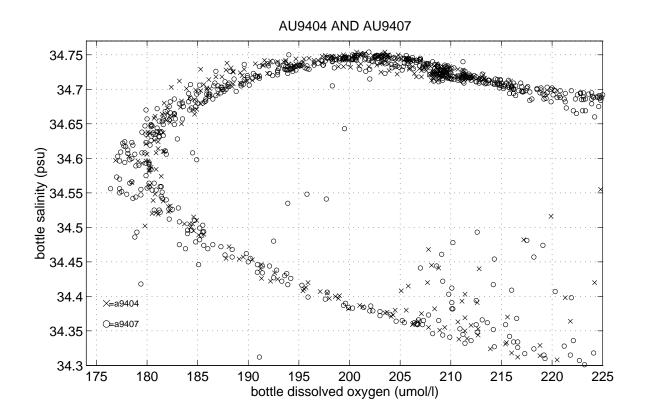
<u>Figure 4.2:</u> Variation south along the SR3 transect of the deep salinity maximum for cruises au9601 (Aurora Australis) and me9706 (Melville), both using Guildline salinometers.

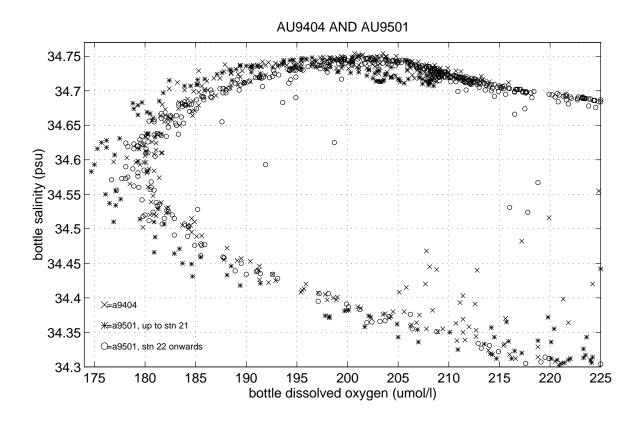


<u>Figure 4.3:</u>  $V_s$  versus  $V_t$  for all cruises along all transects. Note that all stations are plotted, except for a small number with large  $V_t$  values.

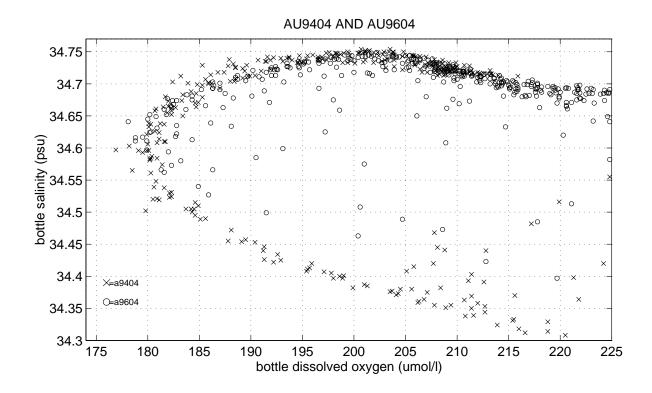


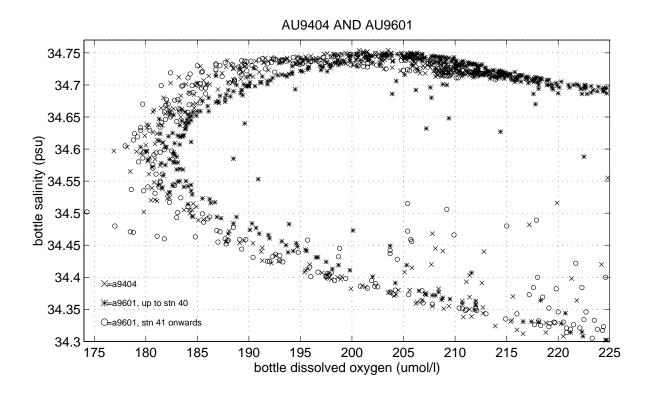
 $\underline{\text{Figure 4.4:}}\ \ \text{Variation of V}_{\text{s}}\ \text{and V}_{\text{t}}\ \text{for individual stations for cruise au9501, along the SR3 transect.}$ 



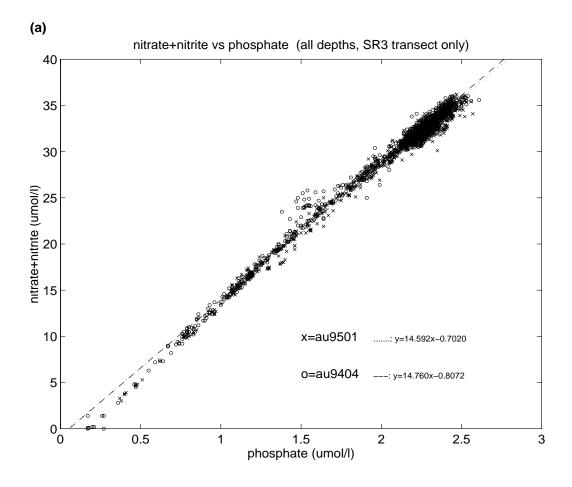


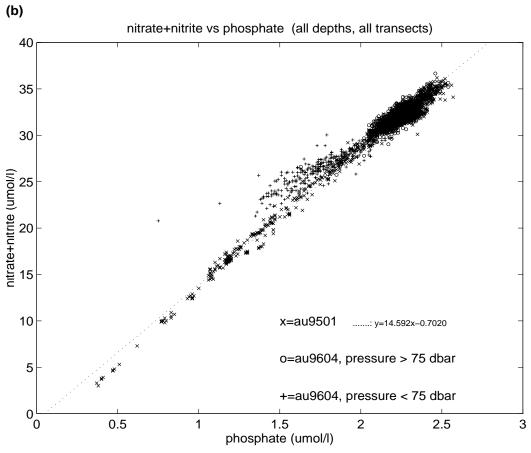
<u>Figure 4.5a:</u> Dissolved oxygen bottle data comparison for cruises au9404, au9407 and au9501, SR3 data only. Note that scale is expanded i.e. not all data are on the plot.





<u>Figure 4.5b:</u> Dissolved oxygen bottle data comparison for cruises au9404, au9604 and au9601, SR3 data only (except for au9604, where data from the longitude range 128 to 150  $^{\circ}$ E are plotted). Note that scale is expanded i.e. not all data are on the plot.





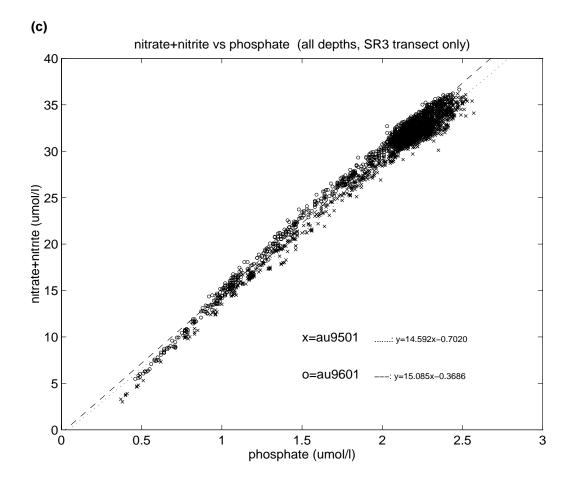
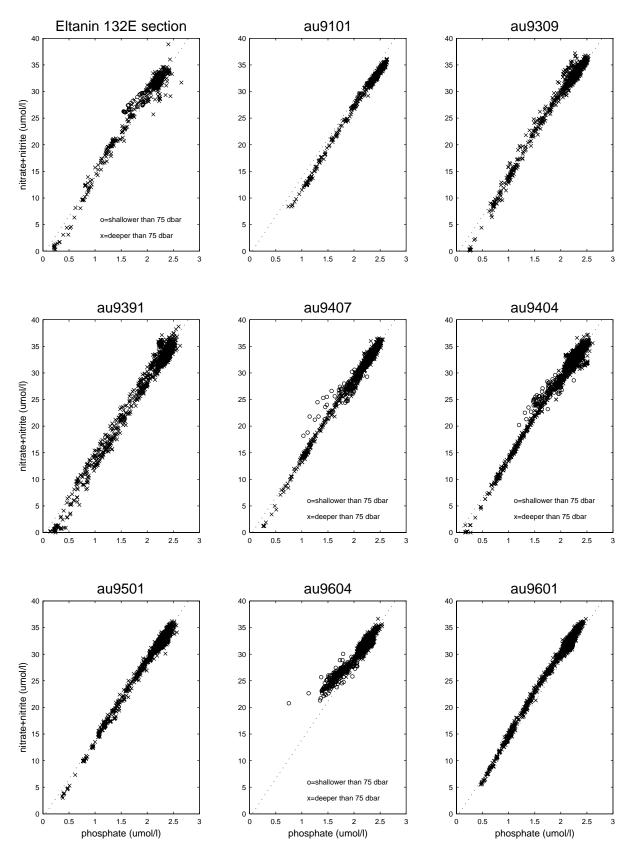
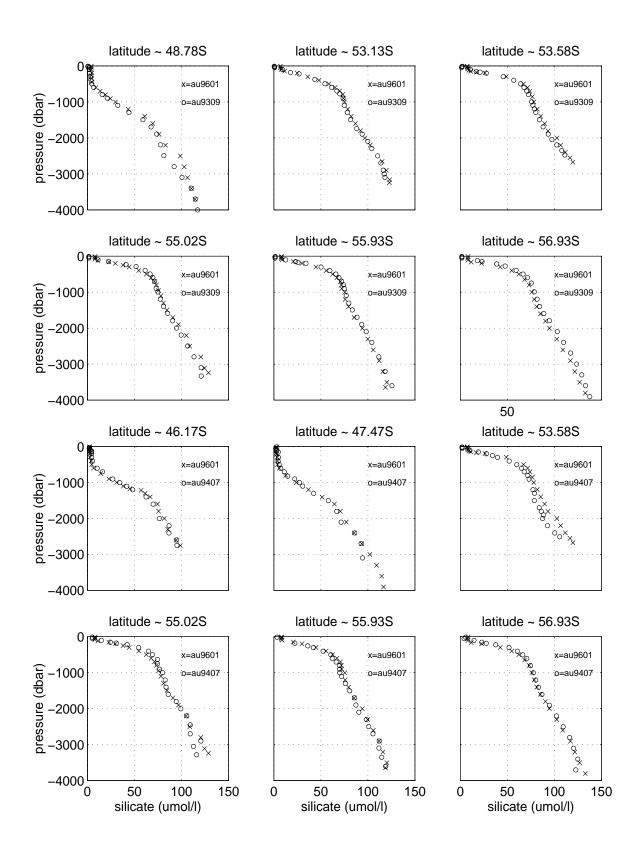


Figure 4.6 (previous page and this page): Bulk plot of nitrate+nitrite versus phosphate for: (a) all au9501 and au9404 data along the SR3 transect, together with linear best fit lines; (b) all au9501 and au9604 data along all transects, with linear best fit line for au9501; (c) all au9501 and au9601 data along the SR3 transect, together with linear best fit lines.

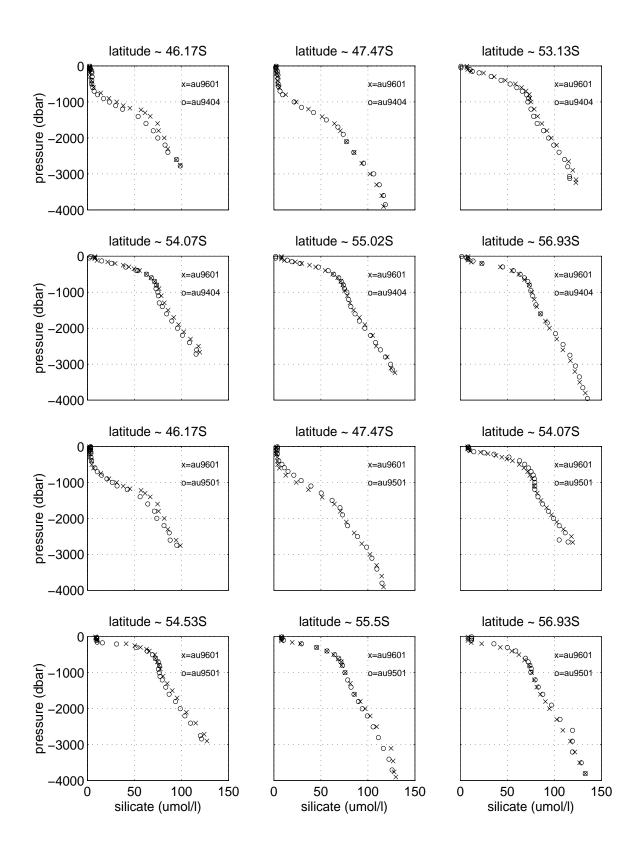
## PHOSPHATE vs NITRATE+NITRITE RATIO, WITH AU9501 BEST FIT LINE



<u>Figure 4.7:</u> Nitrate+nitrite versus phosphate for Aurora Australis oceanographic cruises, plus Eltanin data from Gordon et al. (1982). The linear best fit line for cruise au9501 is included on each plot.



<u>Figure 4.8a:</u> Comparison of vertical silicate concentration profiles between cruises au9601 and au9309, and cruises au9601 and au9407, for selected stations along the SR3 transect. Note that data below 4000 dbar are not included in the plots.



<u>Figure 4.8b:</u> Comparison of vertical silicate concentration profiles between cruises au9601 and au9404, and cruises au9601 and au9501, for selected stations along the SR3 transect. Note that data below 4000 dbar are not included in the plots.

# Part 5 Data File Types and Formats

## 5.1 UNDERWAY MEASUREMENTS

The underway measurements for the cruise, as logged automatically by the ship's data logging system, and quality controlled by human operator (Ryan, 1995), are contained in column formatted ascii files. The two file types contain 10 sec digitised data, and 15 min averaged data. In both cases, missing data or data flagged as bad are replaced by the null value -999. The files are padded out to commence on the first digitising interval of the first day in the file, and ending at the last digitising interval on the last day in the file.

## 5.1.1 10 second digitised underway measurement data

Data at the minimum digitised interval of 10 sec. are contained in files named \*.alf (Table 5.1), where the data filename prefix corresponds to the cruise acronym. A two line header is followed by the data as follows:

column 1	parameter decimal time (0.0=midnight on December 31st, therefore, for example, 1.5=midday
	on January 2nd)
2	day
3	month
4	year
5	hour
6	minute
7	second
8	latitude (decimal degrees, +ve=north, -ve=south)
9	longitude (decimal degrees, +ve=east, -ve=west)
10	depth (m)
11	sea surface temperature ( <sup>O</sup> C) (measured at the seawater inlet at 7 m depth)
12	air pressure (hPa) (included for cruises au9501, au9604 and au9601)
13	wind speed (knots) (included for cruise au9501 only)
14	wind direction (deg. true) (included for cruise au9501 only)
15	roll (included for cruise au9501 only)
16	pitch (included for cruise au9501 only)

Note that all times are UTC.

<u>Table 5.1:</u> Example 10 sec digitised underway measurement file (\*.alf file).

```
Aurora Australis data - GPS pos. (deg), depth (m), sea surface temp (deg C)
 decimaltime day mn yr hr m s
                                     lat
                                              lon
                                                       depth SST
 70.00000004 12 3 1993 0 0 0
                                   -999.0000 -999.0000
                                                        -999.0 -999.00
 70.00011578 12 3 1993 0 0 10
                                   -999.0000 -999.0000
                                                        -999.0 -999.00
 70.00023148 12 3 1993 0 0 20
                                   -44.0044 146.3534
                                                        284.6 15.20
 70.00034722 12 3 1993 0 0 30
                                   -44.0044 146.3529
                                                        -999.0
                                                               15.20
 70.00046296 12 3 1993 0 0 40
                                   -44.0044 146.3530
                                                         283.5
                                                                15.20
 70.00057870 12 3 1993 0 0 50
                                   -44.0044 146.3523
                                                         287.4
                                                                15.20
 70.00069444 12 3 1993 0 1 0
                                   -44.0043 146.3519
                                                        282.2
                                                                15.20
 70.00081019 12 3 1993 0 1 10
                                   -44.0044 146.3515
                                                        282.4 15.20
```

### 5.1.2 15 minute averaged underway measurement data

15 minute averaged data are contained in files named \*.exp (Table 5.2), where the data filename prefix corresponds to the cruise acronym. Note that wind direction and ship's heading are instantaneous values. All times represent the *centre* of the averaging interval. A two line header is followed by the data as follows:

```
column
                 parameter
        decimal time (as for 10 sec digitised files)
 1
 2
        latitude (as for 10 sec digitised files)
 3
        longitude (as for 10 sec digitised files)
 4
        air pressure (hPa)
 5
        wind speed (knots)
 6
        wind direction (deg. true)
 7
        port air temperature (OC)
 8
        starboard air temperature (OC)
 9
        port relative humidity (%)
10
        starboard relative humidity (%)
11
        quantum radiation (μmol/s/m<sup>2</sup>)
12
        ship speed (knots) (speed through the water)
13
        ship heading (deg. true)
14
        ship roll (deg.)
15
        ship pitch (deg.)
16
        sea surface salinity (parts per thousand) (from seawater inlet at 7 m depth)
        sea surface temperature (OC) (at seawater inlet, 7 m depth)
17
18
        average fluorescence (arbitrary units) (from seawater inlet at 7 m depth)
19
        seawater flow (I/min) (flow rate at seawater inlet)
```

Note that all times are UTC.

#### Table 5.2: Example 15 min averaged underway measurement file (\*.exp file).

```
Aurora Australis DLS data: dumped by EXPORT. Column units: days,deg,deg,hPa,knots,degTrue,degC,degC,%,%,umol/s/m2,knots,degTrue,deg,deg,ppt,degC, - ,l/min decimaltime lat long airP windsp windd poairT stairT pohum sthum qrad shipspd shiphdg roll pitch ssSAL ssT avfluo seaflow 70.00520833 -44.00310 146.33583 1022.2 19.6 293 14.2 14.2 93 88 -999 6.56 235.5 1.185341 0.486591 35.175 15.20 -999.000 9.95 70.01562500 -44.00076 146.31305 1022.3 22.1 290 14.2 14.3 92 87 -999 1.15 235.5 1.295333 0.346111 35.165 15.10 -999.000 9.97
                                                                                            14.0 14.0 94 89
14.1 14.0 95 90
14.1 14.1 94 89
70.02604167 -44.00056 146.31239
                                                              1022.3 20.6 305
                                                                                                                              -999 0.00 235.5
                                                                                                                                                             2 568000 0 287667 35 159
                                                                                                                                                                                                              15.10
                                                                                                                                                                                                                         -999 000
                                                                                                                                                                                                                                           9 98
                                                              1022.2 20.6 298
1022.2 20.1 298
1022.2 20.7 288
                                                                                                                              -999 0.00 235.5
-999 0.00 234.5
                      -44.00036 146.31232
70.03645833
                                                                                                                                                             1.303000 0.274444 35.165
                                                                                                                                                                                                                          -999.000
                                                                                                                                                                                                              15.10
70.04687500 -44.00000 146.31136
                                                                                                                                                             1.380111 0.433667 35.166
                                                                                                                                                                                                              15.10
                                                                                                                                                                                                                         -999,000
                                                                                                                                                             1.801667
70 06770833 -43 99918 146 31229
                                                              1022 3 18 5 29 5 13 8 14 1 96 90
                                                                                                                               170 0.00 234.5 1.619333 0.398334 35.164
```

## 5.2 2 DBAR AVERAGED CTD DATA FILES

The final format in which CTD data is distributed is as 2 dbar averaged data, contained in column formatted ascii files, named \*.all (Table 5.3) (the file name prefix is discussed in Appendix 2 of Rosenberg et al., 1995b). Averaging bins are centered on even pressure values, starting at 2 dbar. A 15 line header is followed by the data, as follows:

```
column parameter

1 pressure (dbar)

2 temperature (^{\circ}C) (ITS-90)

3 salinity (PSS78)

4 \sigma_{T} = density-1000 (kg.m<sup>-3</sup>)

5 specific volume anomaly x 10<sup>8</sup> (m<sup>3</sup>.kg<sup>-1</sup>)

6 geopotential anomaly (J.kg<sup>-1</sup>)
```

- 7 dissolved oxygen (μmol.l<sup>-1</sup>)
- 8 number of data points used in the 2 dbar averaging bin
- 9 standard deviation of temperature values in the 2 dbar bin
- standard deviation of conductivity values in the 2 dbar bin
- 11 fluorescence (mg.m<sup>-3</sup>) (uncalibrated)
- 12 photosynthetically active radiation (μmol.s<sup>-1</sup>.m<sup>2</sup>) (uncalibrated)

All files start at the 2 dbar pressure level, incrementing by 2 dbar for each new data line. Missing data are filled by blank characters (this most often applies to dissolved oxygen data).

## Table 5.3: Example 2 dbar averaged CTD data file (\*.all file).

SHIP : R.V. Aurora Australis

STATION NUMBER : 4

DATE : 02-JAN-1994 (DAY NUMBER 2)

START TIME : 1020 UTC = ZBOTTOM TIME : 1100 UTC = ZFINISH TIME : 1222 UTC = ZCRUISE : Au94/07

START POSITION : 44:07.03S 146:13.35E
BOTTOM POSITION : 44:07.14S 146:13.71E
FINISH POSITION : 44:06.61S 146:13.95E
MAXIMUM PRESSURE: 1038 DECIBARS
BOTTOM DEPTH : 1015 METRES

PRESS TEMP SAL SIGMA-T S.V.A. G.A.	D.O.		fluorescence	p.a.r.
(T-90)				
2.0 11.899 34.773 26.432 158.69 0.032	277.6	30 0.001 0.007	0.95569E+01	-0.49498E+00
4.0 11.899 34.778 26.436 158.41 0.063	280.3	30 0.001 0.001	0.10817E+02	-0.63459E+00
6.0 11.903 34.779 26.436 158.46 0.095	281.1	45 0.001 0.002	0.90911E+01	-0.60488E+00
8.0 11.903 34.778 26.435 158.55 0.127	278.0	41 0.000 0.000	0.80700E+01	-0.58265E+00
10.0 11.903 34.778 26.435 158.60 0.159	278.6	32 0.001 0.001	0.75122E+01	-0.66496E+00
12.0 11.904 34.778 26.435 158.66 0.190	280.2	32 0.001 0.001	0.72758E+01	-0.55944E+00
14.0 11.905 34.778 26.435 158.72 0.222	281.5	40 0.000 0.000	0.73697E+01	-0.62194E+00
16.0 11.907 34.779 26.435 158.76 0.254	277.5	34 0.002 0.002	0.69932E+01	-0.56719E+00
18.0 11.908 34.780 26.435 158.77 0.286	275.7	25 0.002 0.002	0.68356E+01	-0.63807E+00

## 5.3 HYDROLOGY DATA FILES

Files named \*.bot (where the filename prefix is the the cruise code e.g. a9407) are column formatted ascii files containing the hydrology data, together with CTD upcast burst data (Table 5.4). The columns contain the following values:

column	parameter
1	station number
2	CTD pressure (dbar)
3	CTD temperature ( <sup>O</sup> C)
4	reversing thermometer temperature (OC)
5	CTD conductivity (mS.cm <sup>-1</sup> )
6	CTD salinity (PSS78)
7	bottle salinity (PSS78)
8	ortho phosphate concentration (μmol.l <sup>-1</sup> )
9	nitrate + nitrite concentration (μmol.l <sup>-1</sup> )
10	reactive silicate concentration (µmol.l <sup>-1</sup> )

- 11 bottle dissolved oxygen concentration (μmol.l<sup>-1</sup>)
- 12 bottle quality flag (-1=rejected, 0=suspect, 1=good)
- 13 niskin bottle number

Missing data values are filled by a decimal point (surrounded by blank characters). Parameters 2,3,5 and 6 are mean values from the upcast CTD burst data at the time of bottle firing, where each burst contains the data 10 sec previous to the time of bottle firing. Parameters 7 to 11 are laboratory values for the hydrology analyses. Parameter 12, the bottle quality flag, is relevant to the calibration of CTD salinities - bottles flagged 1 and 0 are used for calibration, while those flagged -1 are rejected. Criteria for flagging of the bottle data are discussed elsewhere (Appendix 2 of Rosenberg et al., 1995b). Parameter 13, the niskin bottle number, is a unique identifier for each bottle. Note that the bottle number does not always correspond with rosette position.

Table 5.4: Example hydrology data file (\*.bot file).

```
8.556 15.155 15.154 43.109 35.032 35.031 0.29
                                                           8.80
                                                                  7.7
                                                                         247.10 1
                                                                                    11
2
                            43.076 35.034 35.035 0.28
                                                           0.20
                                                                  3.7
                                                                         248.50
                                                                                     9
     25.593 15.111
                                                                                 1
2
     50.992 15.105
                            43.085 35.038 35.038 0.27
                                                           0.30
                                                                  2.2
                                                                         249.10 1
                                                                                     8
                            42.227 35.068 35.077 0.48
2
     73.718 14.188
                                                           4.40
                                                                  2.8
                                                                         228.70 -1
                                                                                     7
     98.376 12.840
2
                            40.910 35.055 35.051 0.66
                                                           7.70
                                                                  2.5
                                                                         227.60 -1
                                                                                     6
2
    123.524 12.490
                            40.618 35.089 35.081 0.76
                                                           9.60
                                                                  3.0
                                                                         223.10 -1
                                                                                     5
                                                                                     4
2
    148.516 11.904
                            40.025 35.052 35.067 0.85
                                                          11.10
                                                                  3.4
                                                                         223.30 -1
2
    200.278 11.085
                            39.174 34.963 34.965 0.90
                                                          13.30
                                                                  4.0
                                                                         226.40 -1
                                                                                     3
2
    247.807 10.678 10.691 38.758 34.914 34.914 1.02
                                                          13.90
                                                                  4.1
                                                                         230.40 0
                                                                                     2
2
    289.188
             9.625
                            37.640 34.769 34.794 1.13
                                                          15.80
                                                                  4.8
                                                                         232.40 -1
                                                                                     1
3
       8.609 15.984 15.958 44.199 35.274 35.275
                                                           0.20
                                                                         270.80
                                                                  1.6
                                                                                    16
3
     21.504 15.975
                            44.198 35.276 35.275 0.25
                                                           0.20
                                                                  1.5
                                                                         266.60
                                                                                 1
                                                                                    15
3
     48.210 15.935
                            44.171 35.277 35.276 0.25
                                                           0.40
                                                                  0.7
                                                                         264.60
                                                                                1
                                                                                    14
3
     73.795 15.897
                            44.140 35.273 35.270 0.27
                                                           0.80
                                                                  1.6
                                                                         238.30 -1
                                                                                    13
                                                           7.50
3
     98.905 14.011
                            42.238 35.229 35.236 0.63
                                                                  2.3
                                                                                    12
                                                                                -1
                                                                         216.00 0
                                                                                    11
3
    148.674 12.557
                            40.763 35.155 35.155 0.81
                                                          10.90
                                                                  4.1
                                                                         227.30
3
    197.813 11.432
                            39.575 35.033 35.033 0.92
                                                          12.80
                                                                                    10
                                                                  3.9
                                                                                 1
3
                                                                         230.70
    298.658 10.110
                            38.158 34.828 34.831 1.10
                                                          15.40
                                                                  4.6
                                                                                 1
                                                                                     9
3
    396.295
              9.214
                            37.238 34.702 34.703 1.28
                                                          18.70
                                                                  6.0
                                                                         226.20 -1
                                                                                     8
3
    496.675
              8.371
                            36.405 34.604 34.603 1.52
                                                          22.50
                                                                  9.3
                                                                         210.60
                                                                                1
                                                                                     7
3
    597.207
              7.385
                            35.469 34.524 34.524 1.71
                                                          25.90
                                                                 14.6
                                                                         199.30
                                                                                 1
                                                                                     6
3
    697.115
              6.587
                            34.751 34.487 34.486 1.90
                                                          28.30
                                                                 20.6
                                                                         195.30
                                                                                1
                                                                                     5
3
    778.707
              5.739
                            33.995 34.458 34.458 2.05
                                                          30.50
                                                                 27.8
                                                                                     4
                                                                                 1
3
    900.509
              4.315
                            32.710 34.381 34.382 2.20
                                                          32.70
                                                                 33.6
                                                                         198.50
                                                                                1
                                                                                     3
3
   1000.091
             4.027
                     4.029 32.574 34.471 34.471 2.34
                                                          34.30
                                                                 49.6
                                                                         171.00 1
                                                                                   302
3
   1113.395
             3.403
                            32.110 34.517 34.522 2.42
                                                          35.40
                                                                 61.3
                                                                         169.90 -1
                                                                                     1
4
     23.926 15.341
                            43.397 35.121 35.120 0.26
                                                           0.10
                                                                  0.6
                                                                         230.60 1
                                                                                    23
4
     49.736 15.198
                            43.231 35.088 35.087 0.26
                                                           0.30
                                                                  0.6
                                                                         229.10 1
                                                                                   22
4
     99.651 13.388
                            41.599 35.202 35.200 0.77
                                                           9.00
                                                                  2.6
                                                                         200.60 1
    148.952 12.164
                            40.341 35.114 35.122 0.86
                                                          12.90
                                                                         221.80 -1 20
                                                                  3.8
                            39,222 34,985 34,980 0.95
                                                          11.40
                                                                         233.30 -1 119
    196.847 11.114
                                                                  3.6
    298.033
              9.997
                            38.028 34.804 34.803 1.02
                                                          13.80
                                                                         254.10 -1 118
              9.235
                            37.228 34.676 34.677
                                                                         256.20 -1 17
    384.198
                            36.455 34.578 34.577 1.43
    495.853 8.452
                                                          20.70
                                                                  8.1
                                                                         232.70 -1
                                                                                    16
```

## 5.4 STATION INFORMATION FILES

Station information files, named \*.sta (Table 5.5) (where the filename prefix is the cruise code), contain position, time, bottom depth and maximum pressure of cast for CTD stations. The CTD instrument number is specified in the file header. Position and time (UTC) are specified at the start, bottom and end of the cast, while the bottom depth is for the start of the cast. Note that small inconsistencies may exist between bottom depth and maximum pressure, due to drift of the vessel between the start and bottom of the cast. In addition, a single value is used for the sound velocity in seawater for echo sounder calculations (1498 m.s<sup>-1</sup>), which may cause small errors in water depth values.

Table 5.5: Example CTD station information file (\*.sta file).

RSV Aurora Australis		Cruise : Au93/09		CTD station list		(CTD unit 4)					
		sta		bottom	max P	I	bottom	1		er	nd
time	date	latitude	longitude	depth(m)	(dbar)	time	latitude	longitude	time	latitude	longitude
2022	11 MAD 02	44:06 726	146:14 255	1000			44.06.276	146:14 255		44.06.406	146.14.605
2032	11-WAK-93	44.06.735	140.14.35E	1000	956	2110	44:06.373	140:14.33E	2154	44.06.195	140.14.00
0027	12-MAR-93	44:00.06S	146:18.61E	300	289	0042	44:00.03S	146:18.77E	0115	43:59.97S	146:18.64E
0513	12-MAR-93	44:07.51S	146:14.89E	1100	1115	0549	44:07.48S	146:15.06E	0632	44:07.39S	146:15.23E
0854	12-MAR-93	44:27.89S	146:07.94E	2340	2335	0938	44:27.52S	146:07.30E	1028	44:27.32S	146:07.51E
1437	12-MAR-93	44:56.71S	145:56.67E	3380	3465	11606	44:56.10S	145:56.52E	1727	44:55.56S	145:56.36E
1	time 2032 0027 0513	time date  2032 11-MAR-93  0027 12-MAR-93  0513 12-MAR-93  0854 12-MAR-93	time date latitude  2032 11-MAR-93 44:06.73S  0027 12-MAR-93 44:00.06S  0513 12-MAR-93 44:07.51S  0854 12-MAR-93 44:27.89S	start longitude  2032 11-MAR-93 44:06.73\$ 146:14.35E  0027 12-MAR-93 44:07.51\$ 146:14.89E  0854 12-MAR-93 44:27.89\$ 146:07.94E	time date latitude longitude bottom depth(m)  2032 11-MAR-93 44:06.73S 146:14.35E 1000  0027 12-MAR-93 44:00.06S 146:18.61E 300  0513 12-MAR-93 44:07.51S 146:14.89E 1100  0854 12-MAR-93 44:27.89S 146:07.94E 2340	start time         date         latitude         longitude         bottom depth(m)           max P (ldbar)           2032         11-MAR-93         44:06.73S         146:14.35E         1000           956           0027         12-MAR-93         44:00.06S         146:18.61E         300           289           0513         12-MAR-93         44:07.51S         146:14.89E         1100           1115           0854         12-MAR-93         44:27.89S         146:07.94E         2340           2335	start time         bottom depth(m)         max P   (dbar)   time           2032         11-MAR-93         44:06.73S         146:14.35E         1000         956         2118           0027         12-MAR-93         44:00.06S         146:18.61E         300         289         0042           0513         12-MAR-93         44:07.51S         146:14.89E         1100         1115         0549           0854         12-MAR-93         44:27.89S         146:07.94E         2340         2335         0938	start time         bottom depth(m)         max P   bottom depth(m)         bottom l(dbar)         bottom latitude           2032         11-MAR-93         44:06.73S         146:14.35E         1000         956         2118         44:06.37S           0027         12-MAR-93         44:00.06S         146:18.61E         300         289         0042         44:00.03S           0513         12-MAR-93         44:07.51S         146:14.89E         1100         1115         0549         44:07.48S           0854         12-MAR-93         44:27.89S         146:07.94E         2340         2335         0938         44:27.52S	time date latitude longitude depth(m)   max P   bottom   latitude longitude   longitude	time date latitude longitude depth(m)   max P   bottom   latitude longitude   time   bottom   latitude   longitude   time   latitude   longitude   lon	time date latitude longitude depth(m)   max P   bottom   latitude longitude   time latitude   latit

## 5.5 WOCE DATA FORMAT

This section is relevant only to data submitted to the WHP Office. For WOCE format data, file format descriptions as detailed above should be ignored. Data files submitted to the WHP Office are in the standard WOCE format as specified in Joyce and Corry (1994).

## 5.5.1 CTD 2 dbar-averaged data files

- \* CTD 2 dbar-averaged file format is as per Table 4.7 of Joyce and Corry (1994), except that measurements are centered on even pressure bins (with first value at 2 dbar).
- \* CTD temperature and salinity are reported to the third decimal place only.
- \* Files are named as in the CTD methodology, except that for WOCE format data the suffix ".all" is replaced with ".ctd".
- \* The quality flags for CTD data are defined in Table 5.6. Data quality information is detailed in earlier sections of this report.

### 5.5.2 Hydrology data files

- \* Hydrology data file format is as per Table 4.5 of Joyce and Corry (1994), with quality flags defined in Tables 5.7 and 5.8.
- \* Files are named as in the CTD methodology, except that for WOCE format data the suffix ".bot" is replaced by ".sea".
- \* The total value of nitrate+nitrite only is listed.

- \* Silicate and nitrate+nitrite are reported to the first decimal place only.
- \* CTD temperature (including theta), CTD salinity and bottle salinity are all reported to the third decimal place only.
- \* CTD temperature (including theta), CTD pressure and CTD salinity are all derived from upcast CTD burst data; CTD dissolved oxygen is derived from downcast 2 dbar-averaged data.
- \* Raw CTD pressure values are not reported.
- \* SAMPNO is equal to the rosette position of the Niskin bottle.
- \* Salinity samples rejected for conductivity calibration, as per eqn A2.20 in Rosenberg et al. (1995b), are not flagged in the .sea file.
- \* Dissolved oxygen samples rejected for CTD dissolved oxygen calibration, as per Tables 1.18, 2.19 and 3.18 in Parts 1, 2 and 3 respectively of this report, are not flagged in the .sea file.

### 5.5.3 Conversion of units for dissolved oxygen and nutrients

## 5.5.3.1 Dissolved oxygen

Niskin bottle data

For the WOCE format files, all Niskin bottle dissolved oxygen concentration values have been converted from volumetric units  $\mu$ mol/l to gravimetric units  $\mu$ mol/kg, as follows. Concentration  $C_k$  in  $\mu$ mol/kg is given by

$$C_k = 1000 C_1 / \rho(\theta, s, 0)$$
 (eqn 5.1)

where  $C_l$  is the concentration in  $\mu$ mol/l, 1000 is a conversion factor, and  $\rho(\theta,s,0)$  is the potential density at zero pressure and at the potential temperature  $\theta$ , where potential temperature is given by

$$\theta = \theta(\mathsf{T},\mathsf{s},\mathsf{p}) \tag{eqn 5.2}$$

for the *in situ* temperature T, salinity s and pressure p values at which the Niskin bottle was fired. Note that T, s and p are upcast CTD burst data averages.

CTD data

In the WOCE format files, CTD dissolved oxygen data are converted to  $\mu$ mol/kg by the same method as above, except that T, s and p in eqns 5.1 and 5.2 are CTD 2 dbar-averaged data.

#### 5.5.3.2 Nutrients

For the WOCE format files, all Niskin bottle nutrient concentration values have been converted from volumetric units µmol/l to gravimetric units µmol/kg using

$$C_k = 1000 C_1 / \rho(T_1, s, 0)$$
 (eqn 5.3)

where 1000 is a conversion factor, and  $\rho(T_I,s,0)$  is the water density in the hydrology laboratory at the laboratory temperature  $T_I$  and at zero pressure. Note that the following values were used for  $T_I$ :

cruise au9501, T<sub>I</sub>=18.0°C cruise au9604, T<sub>I</sub>=19.6°C cruise au9601, T<sub>I</sub>=20.0°C

Upcast CTD burst data averages are used for s.

<u>Table 5.6:</u> Definition of quality flags for CTD data (after Table 4.10 in Joyce and Corry, 1994). These flags apply both to CTD data in the 2 dbar-averaged \*.ctd files, and to upcast CTD burst data in the \*.sea files.

definition
not calibrated with water samples
acceptable measurement
questionable measurement
bad measurement
measurement not reported
interpolated over >2 dbar interval
despiked
this flag not used
parameter not sampled

<u>Table 5.7:</u> Definition of quality flags for Niskin bottles (i.e. parameter BTLNBR in \*.sea files) (after Table 4.8 in Joyce and Corry, 1994).

flag	definition
1	this flag is not used
2	no problems noted
3	bottle leaking
4	bottle did not trip correctly
5	not reported
6,7,8	these flags are not used
9	samples not drawn from this bottle

<u>Table 5.8:</u> Definition of quality flags for water samples in \*.sea files (after Table 4.9 in Joyce and Corry, 1994).

flag	definition
1	this flag is not used
2	acceptable measurement
3	questionable measurement
4	bad measurement
5	measurement not reported
6	mean of replicate measurements
7	manual autoanalyser peak measurement
8	this flag not used
9	parameter not sampled

## 5.5.4 Station information files

<sup>\*</sup> File format is as per section 3.3 of Joyce and Corry (1994), and files are named as in the CTD methodology, except that for WOCE format data the suffix ".sta" is replaced by ".sum".

<sup>\*</sup> All depths are calculated using a uniform speed of sound through the water column of 1498 ms<sup>-1</sup>. Reported depths are as measured from the water surface. Missing depths are due to interference of the ship's bow thrusters with the echo sounder signal.

- $^{\star}$  An altimeter attached to the base of the rosette frame (approximately at the same vertical position as the CTD sensors) measures the elevation (or height above the bottom) in metres. The elevation value at each station is recorded manually from the CTD data stream display at the bottom of each CTD downcast. Motion of the ship due to waves can cause an error in these manually recorded values of up to  $\pm 3$  m.
- \* Lineout (i.e. meter wheel readings of the CTD winch) were unavailable.

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